Shear Lag Models for Discontinuous Composites: Fibre End Stresses and Weak Interface Layers

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Abstract

A new shear lag (SL) type model for stress transfer in a composite with cylindrical fibres is derived. It accounts for fibre end stresses in an approximate yet realistic manner, and leads to a new formula for predicting the Young's modulus of the composites. The predictions of this model were found to agree well with data for metal matrix composites (MMCs) with fibres of various aspect ratios. The accuracy and relative simplicity of the new model have been exploited in the development of an approximate analytical model for the stress transfer and macroscopic yield stress of a composite that contains a weak layer in the matrix adjacent to the reinforcement. With the aid of the latter model, the proof stress of MMCs which contain a precipitate free zone (PFZ) around the reinforcement, can be studied; experimental data obtained for aged 8090 MMCs is consistent with the model predictions.

Keywords: shear lag model, stress transfer, MMC, PFZ, interface, Al-Li

1.   Introduction

The elastic response of composite systems to externally applied stress can be predicted by Eshelby type models, which are valid for ellipsoidal inclusions [1,2,3,4], or by shear lag (SL) type models, which have been proposed for aligned cylindrical inclusions [5,6,7,8]. Even though stress fields around cylindrical inclusions are very similar to those around ellipsoidal inclusions with the same aspect ratio [9], Eshelby type model predictions differ considerably from SL type model predictions with regard to stress transfer in short fibre and particulate composites [5,8,10]. This indicates that, as a result of quite crude assumptions concerning the magnitude of the stresses at the ends of the fibres, the current SL type models severely underestimate the load transfer to the reinforcement.

Hence, Eshelby type models have tended to be favoured over SL type models. Nevertheless, SL type models offer advantages both in terms of the relative ease of the modelling and because they represent a better approximation of the often angular shapes of inclusions in various real composites.

Apart from the elastic response, also the yielding in composites can be analysed with SL and Eshelby type models. Several studies of yield strength of composites with a homogeneous matrix yield strength have been presented [11,12]. However, in the present paper, the focus is on composite systems that have a weak interfacial matrix layer around the reinforcement. These types of interfaces are for instance encountered in Al-Li and Al-Si-Mg based composites, in which a matrix layer devoid of the strengthening precipitates forms in the course of the ageing temper [13,14,15,16]. This type of layer in a precipitation strengthened metallic material is generally called a precipitate free zone (PFZ). The relative simplicity of SL type models can be exploited to modify them for specific situations. In the present paper, it is shown that an SL type model can be used to derive analytical expressions for stress transfer of a composite system that contains a weak matrix layer adjacent to the reinforcement.

Thus, the aim of the present paper is twofold. Firstly, it is shown that improving the description of the stresses at the fibre ends can enhance the accuracy of the shear lag model. Secondly, an SL type model is derived for the case of a composite system that contains a weak interface layer between matrix and reinforcement.

2.   A new shear lag model

2.1.   Formulation

According to the shear lag model (see schematic of geometry in Fig. 1), the axial stress in the cylindrical fibre is given by (see e.g. [10]):

$$\sigma_r(z) = E_r \varepsilon_c + A \sinh\left(\frac{\gamma z}{r_o}\right) + B \cosh\left(\frac{\gamma z}{r_o}\right) \tag{1}$$

where ε_c is the average macroscopic strain of the composite,

$$\gamma = \sqrt{\frac{2E_m}{E_r(1+\nu_m)\ln(1/f_r)}} \tag{2}$$

E_r and E_m are the Young's moduli of the reinforcement and the matrix, respectively, ν_m is Poisson's ratio of the matrix, f_r is the volume fraction of reinforcement and r_o is the radius of the fibre cross-section. Constants A and B are dependent on the assumed stress at the fibre ends, σ_e. Taking the origin at the middle of the fibre and accounting for the symmetry gives:

$$\sigma_r(z) = E_r \varepsilon_c - (E_r \varepsilon_c - \sigma_e) \cosh\left(\frac{\gamma z}{r_o}\right) \mathrm{sech}(\gamma s_r) \tag{3}$$

where s_r is the aspect ratio of the fibre. Hence it follows that the stress at $z = 0$ is given by:

$$\sigma_r(z = 0) = E_r \varepsilon_c - (E_r \varepsilon_c - \sigma_e)\mathrm{sech}(\gamma s_r) \tag{4}$$

In the literature several ways of determining σ_e have been proposed [8,10,17,18]. In the most simple version of the shear lag model, here denoted as the debonded shear lag (DSL) model, σ_e is simply neglected, that is, $\sigma_e = 0$. The DSL model is not reasonable for well-bonded fibres with relatively low aspect ratio, but is quite adequate for fibres with high aspect ratio. In his modification of the DSL model, Clyne [10] suggested that it is reasonable to assume σ_e as the average of the remote matrix stress and the peak fibre stress in the absence of fibre end stresses. It can be shown [10] that this leads to:

$$\sigma_e = E_m' \varepsilon_c \tag{5}$$

where

$$E_m' = \frac{E_r[1 - \mathrm{sech}(\gamma s_r)] + E_m}{2} \qquad \text{(CSL model)} \tag{6}$$

From this the average longitudinal stress σ_c can be calculated and the corresponding composite modulus according to the CSL model is obtained as [5,10]:

$$E_c = \frac{\sigma_c}{\varepsilon_c} = f_r E_r\left[1 - \frac{E_r - E_m'}{E_r}\frac{\tanh(\gamma s_r)}{\gamma s_r}\right] + (1 - f_r)E_m \tag{7}$$

The latter equation gives the average stress in the composite as the weighted average of the mean stress in the reinforcement (1st term on the right hand side of the latter equation) and the average stress in the matrix (2nd term on the right hand side of the latter equation). It has been shown that Clyne's version of the shear lag model (CSL) is an improvement over the DSL model in terms of the prediction of Young's modulus data of Al-SiC composites. However, both versions underestimate Young's modulus of such composites [10].

In the present work it is proposed that within the framework of the shear lag model, a more consistent approach would be to take σ_e as the average of the average matrix stress ($E_m\varepsilon_c$) and the peak fibre stress in the presence of fibre end stresses. Hence, it follows:

$$2\sigma_e = E_r \varepsilon_c - (E_r \varepsilon_c - \sigma_e)\mathrm{sech}(\gamma s_r) + E_m \varepsilon_c \tag{8}$$

which leads again to Eq. (5) but with E_m' redefined as

$$E'_{m} = \frac{E_{r}[1 - \mathrm{sech}(\gamma s_{r})] + E_{m}}{2 - \mathrm{sech}(\gamma s_{r})} \tag{9}$$

This version will be denoted as the SSSL model. Combining Eqs 7 and 9 gives:

$$E_{c} = f_{r}E_{r}\left[1 - \left(\frac{1 - E_{m}/E_{r}}{2 - \mathrm{sech}(\gamma s_{r})}\right)\frac{\tanh(\gamma s_{r})}{\gamma s_{r}}\right] + (1 - f_{r})E_{m} \tag{10}$$

Jiang et al. [8] have also proposed an SL type model based on an expression for σ_{e} which differs from the ones presented above. In the discussion that follows, this version will be referred to as the JSL model. It is further noted that the semi-empirical Tsai-Halpin equation [19] has also been used to describe the elastic response of composite systems.
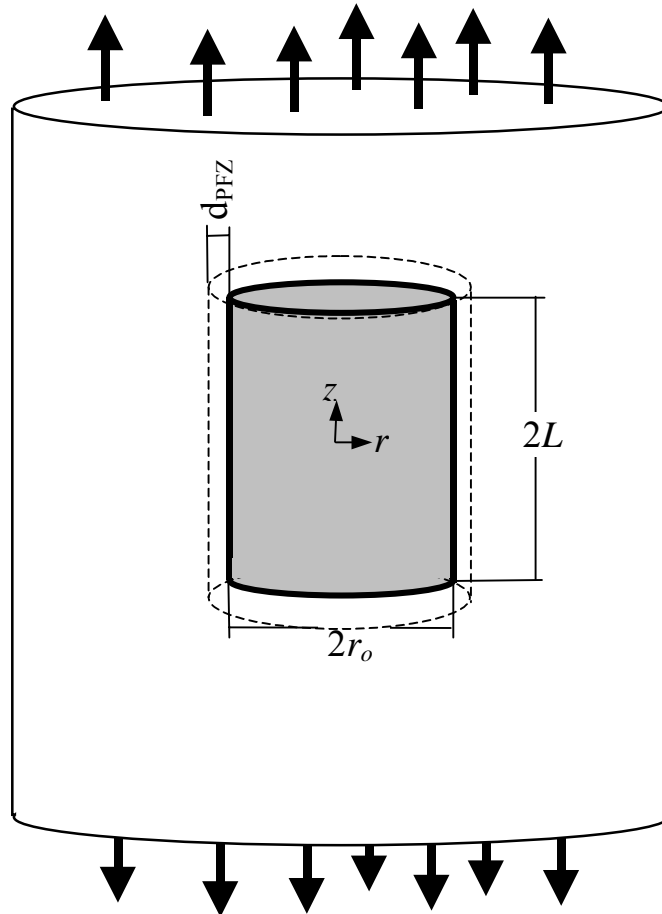

Fig. 1   Geometry of cylindrical fibre in a composite material which is subjected to external loading. The extend of the weak zone around the fibre is indicated by the dotted line.

2.2. Comparison with experimental data

In comparing the predicted E_c with measured values, it is important to select only data on alloys for which the reinforcement is approximately cylindrical (or approximately ellipsoidal) with aspect ratios that have been characterised in detail. Such data is available for SiC reinforced Al-based alloys with s_r of about 2 [20,21 *], s_r of about 3 [22] and s_r of about 4 [8,23]. The predictions from the various models are compared with these data in Fig. 2 ($s_r = 2$), Fig. 3 ($s_r = 3$), Fig. 4 ($s_r = 4$) and Fig. 5. It should be noted that E_m depends on the composition of the Al-based alloys, especially the Li content. In order to make valid comparisons for cases in which E_m varies considerably between the alloys, in some figures the ratio E_c / E_m rather than E_c is plotted. In these cases E_m is taken as the average value for the alloys considered. The plots in Figs 2-5 show that the present SSSL model fits well to the measured data, and, in comparison with the other models, it appears to provide the best overall fit.

The relative accuracy of the model predictions depends critically on the aspect ratio of the inclusions (see Fig. 5). As a consequence, the present comparison of data and model predictions should only be considered as just an indication of the SSSL model's accuracy, since, in many real MMCs, the range of aspect ratios of the inclusions is quite broad whilst the inclusions are not perfectly aligned [22]. This point is illustrated via an investigation of E_c data on so-called particulate reinforced, Al-based MMCs [24,25,26,27], which are technologically important because they possess relatively homogeneous properties and are relatively cheap to produce. Single particulate reinforced MMCs generally contain a range of angular particles. Within a single composite a broad range of reinforcement sizes and shapes can be encountered and aspect ratios vary between 1 and 4 [24,27]. Due to the thermo-mechanical processing (extrusion, rolling), the longer axis of the reinforcing particles (especially the ones with higher s_r) tend to be aligned along the axis of the main working direction and, for various MMCs, the effective s_r along this axis has been estimated at 1.4 to 1.8 [20,25,27,28]. Comparison of data on E_c along the axis of the main working direction with the predictions of the models (Fig. 6, with $s_r = 1.5$) shows that for these composites the best fit is provided by the Eshelby model (see also Refs. [13,24,25,27]). The SSSL model, whilst showing a considerable improvement over the CSL model, underpredicts this data by about 15 to 25%. In discussing this finding it is important to note that these each composite contains angular reinforcements with a broad range of shapes and aspect ratios, and, hence, the suitability of any one of the models or the adopted effective average aspect ratio may be questionable. Hence, these data do not provide a conclusive proof as to the validity of the various models, but they do indicate that at these very low aspect ratios the Eshelby model is more appropriate than the SSSL model.

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* Actually, the SiC fibres in the 6061 Al based composites studied by McDanels [21] have a wide range of aspect ratios. In correspondence to Clyne's assessment [10] we estimate the effective aspect ratio of the fibres in these composites at about 2. This older data is included in the present paper to facilitate comparison with Clyne's work.
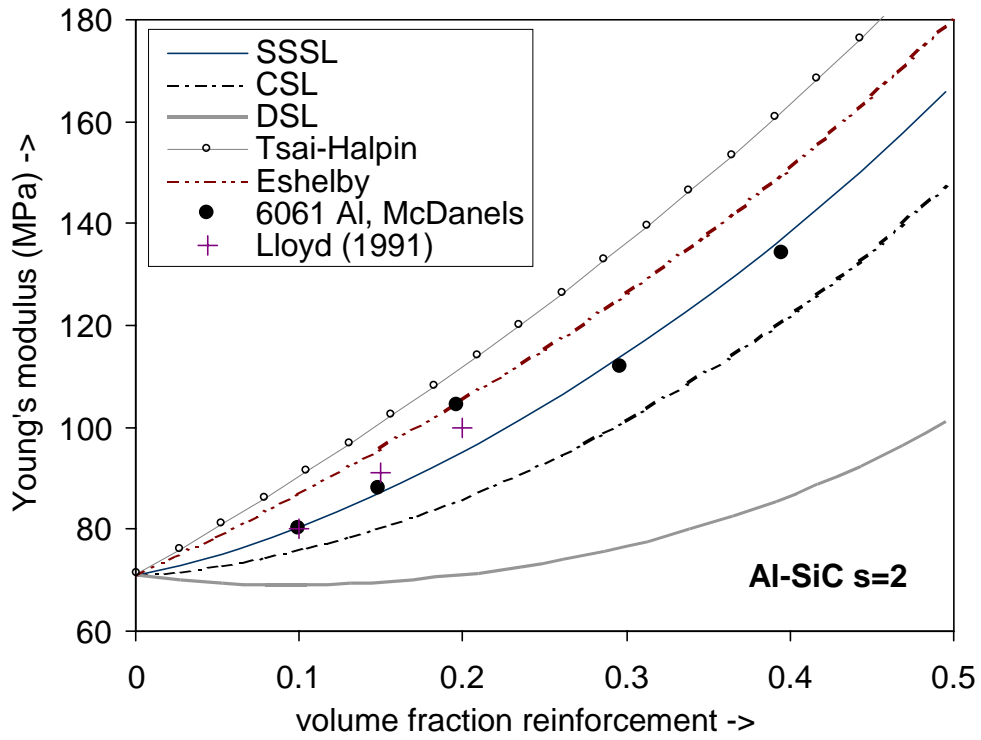
Fig. 2 Comparison of predicted and measured Young's modulus of Al-SiC composites with s_r =2. (E_{Al} = 71 GPa, E_{SiC} = 450 GPa.)
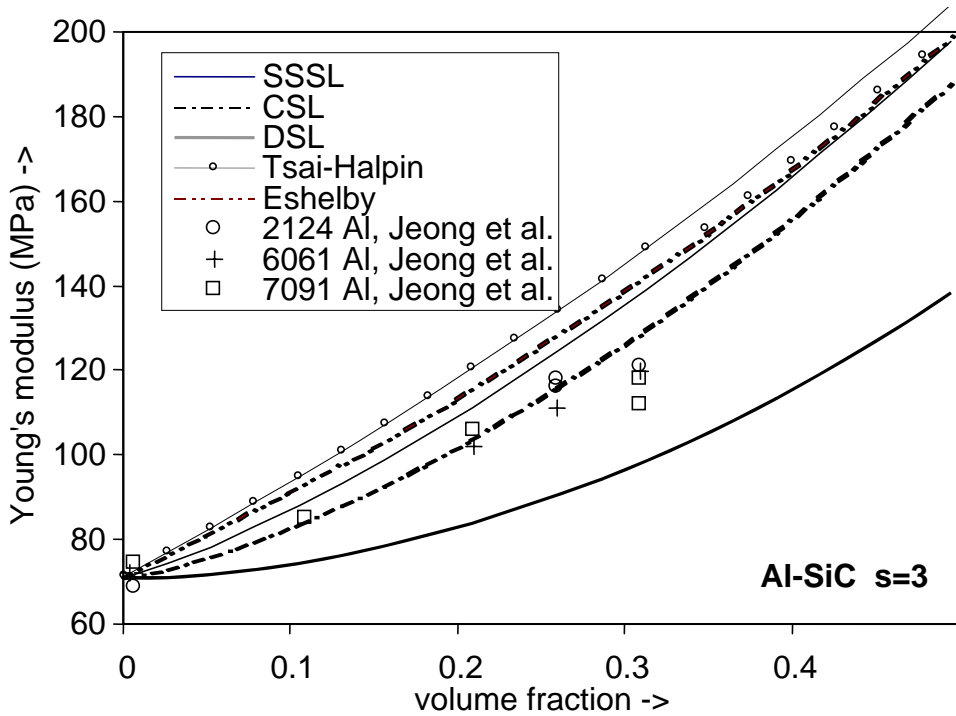

Fig. 3 Comparison of predicted and measured Young's modulus of Al-SiC composites with s_r =3. (E_{Al} = 71 GPa, E_{SiC} = 450 GPa.)
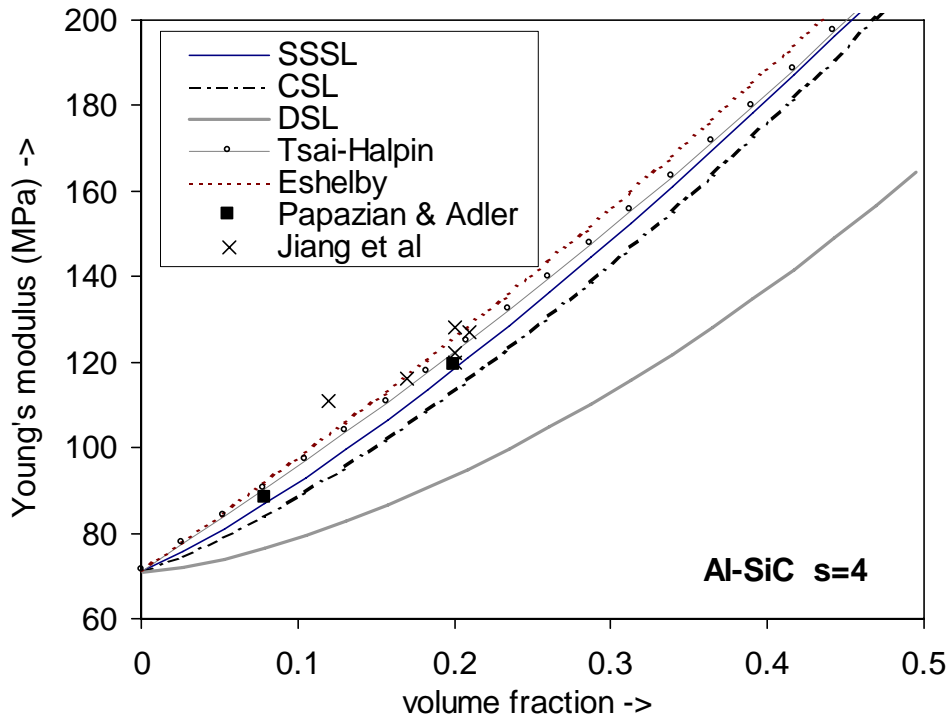
Fig. 4   Comparison of predicted and measured Young's modulus of Al-SiC composites with s_r =4. (E_{Al} = 78 GPa, E_{SiC} = 450 GPa.)

In more general terms the present comparison of the various models with the available data indicates that neither the Eshelby model nor any SL type model can fit the available data for all volume fractions and aspect ratios. This is thought to be mainly due to the approximations made in the development of these models (mean field assumptions in the Eshelby model, approximations for fibre end stresses in SL models), whilst inconsistency between assumed and actual shape of inclusions may also play a part. Nevertheless, in terms of predictive capability, the SSSL model is clearly a considerable improvement over other SL type models[†], and, on balance, this relatively simple, closed form solution appears to perform in some cases nearly as well as, and in other cases better than the Eshelby model. From a modelling perspective, it is further encouraging to note that of the four SL models considered, the SSSL model predictions are generally closest to those of the Eshelby model. Thus, the present SSSL model alleviates the problem of the large discrepancies [5,10] between previous shear lag (DSL, CSL) and Eshelby model predictions (see Fig. 5). Specifically, the SSSL model predicts $E_r \geq E_c \geq E_m$ for all s_r, resolving the physically unreasonable, for perfectly bonded fibres, CSL model predictions of $E_c < E_m, E_r$ for low s_r (that is, for $s_r < 0.9$ in Al/SiC composites).

[†]   It should also be noted that, whilst the JSL model [8] predictions for E_c appear, in general, to be less accurate than the corresponding ones by the SSSL model, the strength of the JSL model lies especially in its capability of predicting local stresses in the matrix and in assessing the effect of residual stresses on the yield behaviour of composites.
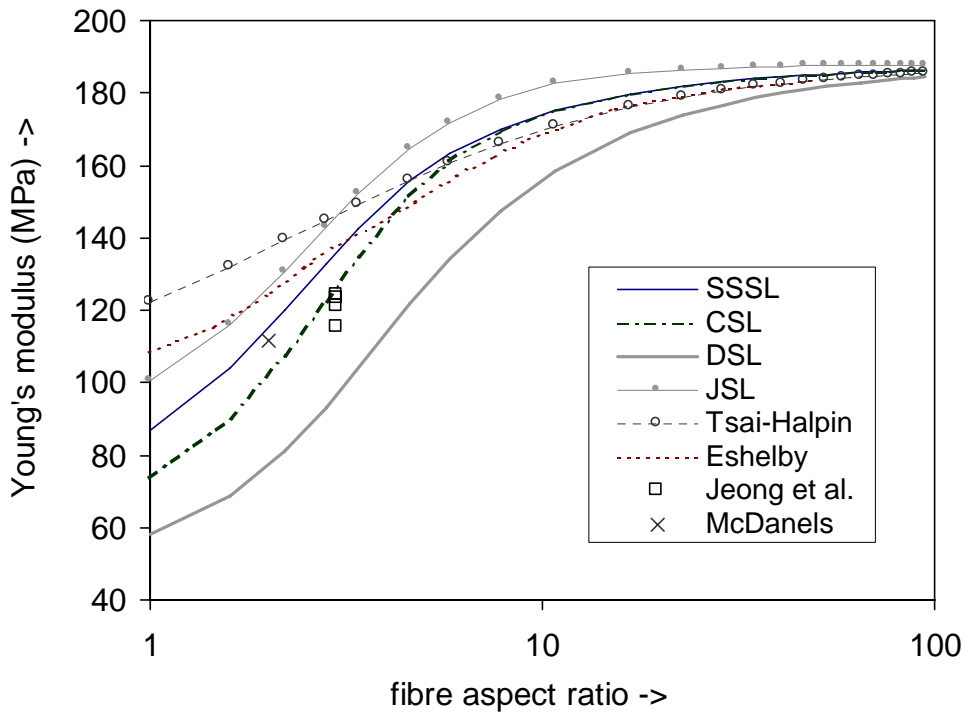
Fig. 5   Comparison of Young's modulus of Al-30vol%SiC composites as predicted by different
shear lag type models and by the Eshelby model. (E_{Al} = 71 GPa, E_{SiC} = 450 GPa.)
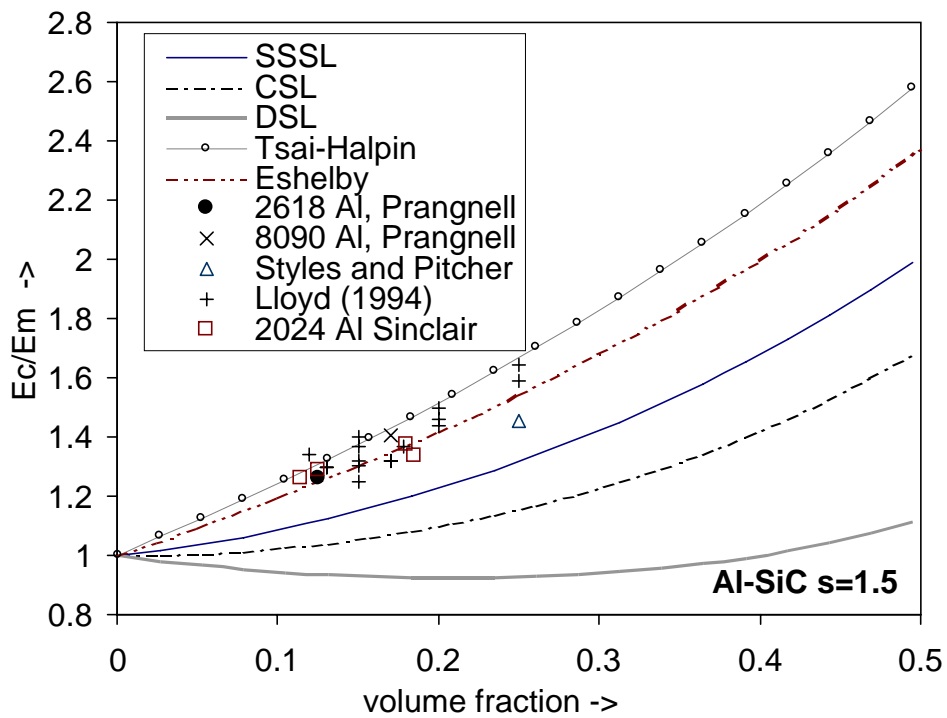

Fig. 6   Comparison of predicted and measured Young's modulus of particulate reinforced Al-SiC
composites. s_r is estimated to equal 1.5. (E_{Al} = 78 GPa, E_{SiC} = 450 GPa.)

In summarising this section, it is concluded that the present modification of the shear lag model, the SSSL model, fits well to the experimental data on fibre reinforced composites and avoids the physically unreasonable predictions made by earlier SL type models.

3.   The effect of a weak interface layer on the yield stress

3.1.   Modelling

The present analysis of the yield strength of a composite with a weak interface layer is based on the SSSL model described in the previous section. Although the model is described in a general manner, several assumptions and examples are chosen especially with metallic matrices reinforced by relatively stiff fibres in mind. Some simplifying assumptions are made with the aim of obtaining explicit, closed form solutions.

When a weak interface layer is present around the reinforcement, the stresses that can be sustained by the weak interface layer before local yielding occurs are limited and the stress transfer to the reinforcement will be reduced. In order to arrive at a mathematically tractable solution, first the strains at the fibre ends will be estimated in the simple case when the weak interface layer is very weak in comparison to the matrix ($\sigma_{\text{y}}^{\text{PFZ}} << \sigma_{\text{y}}^{\text{m}}$). The fibres are assumed much stiffer than the matrix ($E_{\text{r}} >> E_{\text{m}}$). Hence, the elastic deformation of the fibres is negligibly small and the composite deforms via deformation of matrix and weak interface layer only. Thus, the elongation of the weak interface layer at the fibre ends should be compatible with that of the matrix at some perpendicular distance from the fibre where matrix strain is approximately equal to composite strain. This condition gives:

$$(1+\varepsilon_{\text{e}})d_{\text{PFZ}} + L \approx (1+\varepsilon_{\text{c}})(L + d_{\text{PFZ}}) \tag{11a}$$

where d_{PFZ} and ε_e are, respectively, the thickness and strain of the layer, L is the half-length of the fibre (Fig. 1) and ε_c the composite strain. From (11a), it follows:

$$\varepsilon_{\text{e}} \approx \varepsilon_{\text{c}}\left[\frac{L}{d_{\text{PFZ}}} + 1\right] \tag{11b}$$

Since d_{PFZ} is much smaller than L, it is evident from Eq. 11b that the maximum stress at the fibre ends in the presence of a weak interface layer will reach the yield strength of that layer, σ_y^{PFZ}, well before significant yielding throughout the remainder of the matrix of the composite occurs. As a consequence, the stress transfer due to stresses at the fibre ends is essentially reduced by a factor σ_y^{PFZ}/σ_e, in comparison to a composite with homogeneous matrix strength.

Apart from the stresses at the fibre ends, the stresses at the sides of the fibre will also be influenced by the presence of the weak interfacial layer, and, especially for longer fibres, the shear stresses in the yielding layer adjacent to the fibre sides will be important in determining the overall stress response of the composites. An indication of this influence is provided by the SL prediction of the interfacial shear stress distribution along the fibre side. This shear reaches a maximum near the fibre ends and the composite strain initiating yield locally is found equal to

$$\varepsilon_c^* = \frac{\sigma_y^{PFZ}}{E_r}\left(1 + \frac{1}{\gamma \tanh(\gamma s_r)}\right) \tag{12}$$

Since E_r is much greater than E_m and σ_y^{PFZ} is smaller than the matrix yield stress σ_y^m, it is clear from the latter equation that, for fibres with large aspect ratio, yielding of the interface layer on the fibre side will start well before the matrix yields. In order to generate a simple mathematical model for this gradual weakening process, the assumption is here made that the average fibre stress is reduced by the factor σ_y^{PFZ}/σ_e where σ_e is the fibre end stress for non-yielding matrix at identical σ_c. This assumption leads to the following expression for the overall stress in the composite:

$$\frac{\sigma_c}{\varepsilon_c} = f_r E_r \left(1 - \frac{E_r - E_m'}{E_r}\frac{\tanh(\gamma s_r)}{\gamma s_r}\right)\frac{\sigma_y^{PFZ}}{\sigma_e} + (1 - f_r)E_m \tag{13}$$

As indicated by Eqs. 3 and 4, for fibres with a small aspect ratio, the stress transfer at the fibre ends is the dominant factor in determining the overall response. Thus, the average fibre stress is very close to σ_e, therefore the weak interface layer will only yield at the fibre end face and Eq. 13 can be applied without significant loss of accuracy. In contrast, for fibres with a large aspect ratio, there is considerable stress transfer remaining at the side of the fibre even after yielding of the weak layer has occurred at the fibre ends. The present treatment essentially approximates the weakening of this stress transfer due to the presence of the weak layer by assuming that the shear stress averaged over one half of the fibre is proportional to σ_e. The proposed approximation may, however, become less accurate with increasing aspect ratio.

As the total volume of the weak interface layer will generally be very small, the yielding in the weak interface layers will not lead to a major deviation from linearity of the stress-strain curve of the composite, that is, on a macroscopic scale, the yielding in the weak interface layers will be barely detectable. Significant deviation from linearity will occur when yielding occurs in the remainder of the matrix, that is, when the average stress in the matrix exceeds the matrix yield stress (see also [8]). Hence, it follows:

$$\sigma_y^c = \varepsilon_c f_r E_r \left(1 - \frac{E_r - E_m'}{E_r}\frac{\tanh(\gamma s_r)}{\gamma s_r}\right)\frac{\sigma_y^{PFZ}}{\sigma_e} + (1 - f_r)\sigma_y^m \tag{14}$$

The strain in the composite may be further approximated at the yield point by $\varepsilon_c \cong \sigma_y^m / E_m$ and, hence, Eq. 14 can be rearranged to give a linear relationship between the macroscopic yield strength of the composite and the yield strength of the matrix:

$$\frac{\sigma_y^c}{\sigma_y^m} \cong f_r \left(\frac{E_r}{E_m} - \frac{E_r - E_m'}{E_m} \frac{\tanh(\gamma s_r)}{\gamma s_r} \right) \frac{\sigma_y^{PFZ}}{\sigma_e} + (1 - f_r) \tag{15}$$

or, by using Eq. 5:

$$\frac{\sigma_y^c}{\sigma_y^m} \cong f_r \left(\frac{E_r}{E_m'} - \frac{E_r - E_m'}{E_m'} \frac{\tanh(\gamma s_r)}{\gamma s_r} \right) \frac{\sigma_y^{PFZ}}{\sigma_y^m} + (1 - f_r) \tag{16}$$

It is noted that when $\sigma_y^{PFZ} / \sigma_e$ equals 1, it follows from Eqs. 7 and 15 that $\sigma_y^c / \sigma_y^m = E_c / E_m$. This case however represents an unrealistic situation of no local matrix yielding over the reinforcement-matrix interface. Hence the composite behaves linearly until overall yield which coincides with matrix yield, that is, at strain $\varepsilon_c = \dfrac{\sigma_y^c}{E_c} = \dfrac{\sigma_y^m}{E_m}$. Eq. 16 shows that $\sigma_y^c / \sigma_y^m \neq E_c / E_m$ when $\sigma_y^{PFZ} / \sigma_y^m = 1$, that is, in the absence of a weak interface layer.

In most real composites, the PFZ will strain harden during plastic deformation and for this effect to be accounted for by the proposed model, the stress at the fibre ends can be calculated from a theoretical expression of strain hardening [29,30]:

$$\sigma_y^{PFZ} = \sigma_{y,0}^{PFZ} + K \sqrt{\varepsilon_e} \tag{17}$$

where $\sigma_{y,0}^{PFZ}$ is the yield strength of the weak interface layer at zero pre-strain, ε_e is the strain in the plastic zone calculated using Eq. 11 and K is a parameter which depends on the strain hardening capability of the PFZ (for 8090 K is estimated at about 150 MPa).

3.2. Verification and application

The present model of MMCs with a weak interface region adjacent to the particles should be valid for various heat treatable Al-based MMCs in which a PFZ around the reinforcement develops. An example of such a composite is the 8090 (Al-Li-Cu-Mg) alloy reinforced with SiC particles. The matrix of this composite is strengthened by GPB zones, S′ (Al$_2$CuMg) and δ′ (Al$_3$Li) precipitates [14,31,33,32], but a layer devoid of the strengthening δ′ (Al$_3$Li) precipitates forms around the SiC particles as a result of Li depletion of the zone caused by the formation of Li containing precipitates on the SiC/matrix interface [14]. The SiC particles are angular, and, although they are clearly not cylindrical, SL type models with cylindrical inclusions should provide a better approximation of the stress transfer as compared to the Eshelby type model with ellipsoidal inclusions. In a recent study [33] of the proof strengths of various Al-Li-Cu-Mg based composites and monolithic alloys, a

comprehensive model for the strength of the matrices of these alloys and composites based on a detailed assessment of the microstructures is presented and validated. The values of σ_y^m and σ_y^{PFZ} obtained in that study are used to validate the model presented in this section of the present work. It should be noted that obtaining σ_y^m and σ_y^{PFZ} for heat treatable, PFZ-containing MMCs is not a straightforward matter, because both these strengths vary with ageing time and cannot be measured directly.

Account should also be taken of the fact that, due to the high load transfer to the reinforcement resulting from plastic deformation, MMCs have a high work hardening rate, and consequently the (0.2%) proof stress can be considerably higher than the yield stress. In order to account for this "plastic stress transfer", the corresponding strength increment, $\Delta\sigma_{pst}$, as predicted by the Eshelby-type model presented in Ref. [34], is used. The latter work shows that $\Delta\sigma_{pst}$ depends on f_r, s_r, elasticity constants and the plastic strain of the composite ε_e^p, and is estimated at about 20 MPa for the material data of the tested MMCs considered here (Table 1). For the composites with a weak interface layer, the "plastic stress transfer" is taken account of by assuming that, similarly to the elastic stress transfer, the effect is proportional to σ_y^{PFZ}. Thus, Eq. 16 is modified to:

$$\sigma_{0.2}^c \cong \left[f_r \left(\frac{E_r}{E_m'} - \frac{E_r - E_m'}{E_m'} \frac{\tanh(\gamma s_r)}{\gamma s_r} \right) \sigma_y^m + \Delta\sigma_{pst} \right] \frac{\sigma_y^{PFZ}}{\sigma_y^m} + (1 - f_r)\sigma_y^m \qquad (18)$$

The results of the assessment of the 0.2% proof stress, presented in Table 1, show that the proposed model predicts the proof stresses of the 8090 MMC samples quite well. In particular, it accurately predicts that, for this composite, the potential strengthening effect due the SiC is reduced to zero as a result of the presence of the PFZ.

Table 1 Yield strengths of 8090/17vol%SiC composites after ageing for several times at 170ºC. σ_y^m and σ_y^{PFZ} are obtained from a quantitative analysis microstructure in combination with a comprehensive model of the strengthening of Al-Li-Cu-Mg alloys [33] ($s_r = 1.5$).

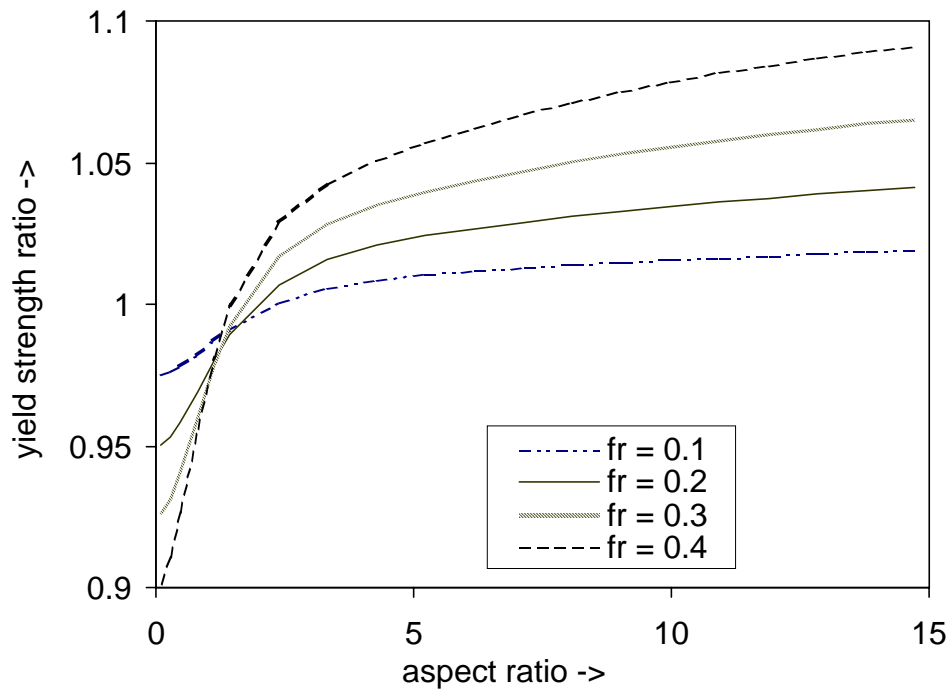| t (h)	d_{PFZ} (μm)	σ_y^m (MPa)	σ_y^{PFZ} (MPa)	$\sigma_y^m : \sigma_y^c$ (predicted) (MPa)	$\sigma_{0.2}^c$ (predicted) (MPa)	$\sigma_{0.2}^c$ (measured) (MPa)
0	0	136	-	1.18	185	220
0.17	0.02	294	161	0.95	297	306
7	0.06	353	186	0.94	352	368
168	0.12	399	243	0.96	402	418

Fig. 7   The ratio of the yield strength of Al-SiC composites to the yield strength of the matrix for $\sigma_y^{PFZ} / \sigma_y^m = 0.75$, vs. the aspect ratio of the cylindrical SiC reinforcement. ($E_{Al} = 71$ GPa, $E_{SiC} = 450$ GPa.)
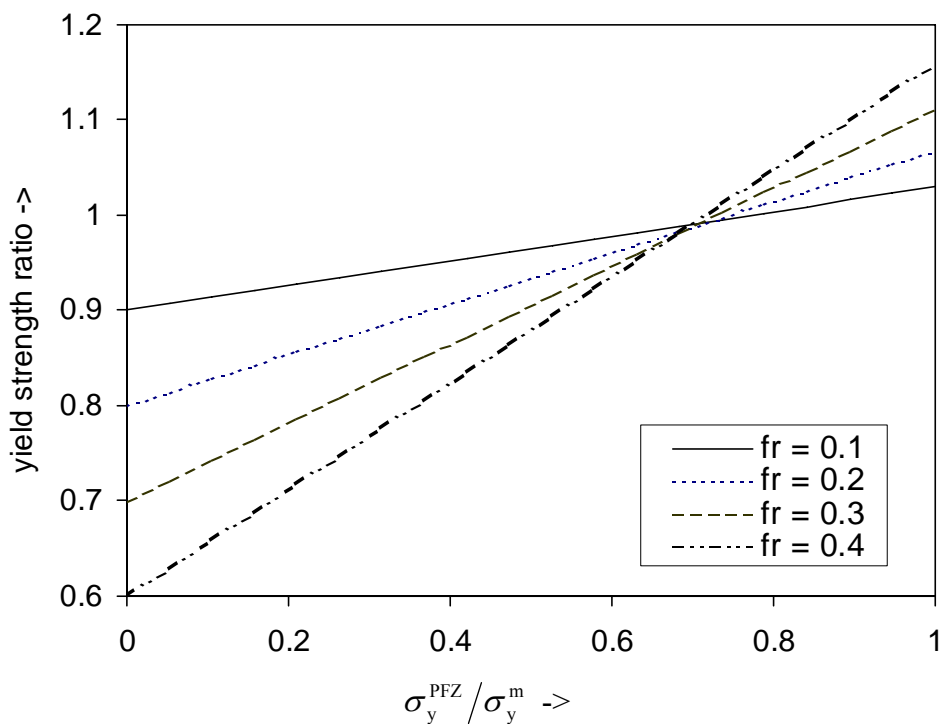

Fig. 8   The ratio of the yield strength of Al-SiC composites to the yield strength of the matrix vs. $\sigma_y^{PFZ} / \sigma_y^m$. The aspect ratio of cylindrical SiC inclusions is 2. ($E_{Al} = 71$ GPa, $E_{SiC} = 450$ GPa.)

The above analytical expressions can be readily evaluated for any composite and selected results for the case of Al-SiC composites are presented in Fig. 7 and Fig. 8. For the sake of clarity of presentation the strain hardening of the PFZ has been neglected, that is, a perfectly plastic matrix is considered. The present simplified model predicts that for a perfectly plastic matrix, the thickness of the PFZ, d_{PFZ}, does not influence the yield strength of the composite.

Fig. 7 shows that even for a relatively limited softening of the interface layer ($\sigma_y^{\mathrm{PFZ}} / \sigma_y^{\mathrm{m}} = 0.75$) the strengthening of the material as a result of the addition of fibres is predicted to be significantly reduced. This effect is especially marked for low aspect ratios of "reinforcement". Fig. 8 further illustrates the effect of a combination of a weak interface layer and low fibre aspect ratio. This figure shows that for composites with inclusions of fixed aspect ratio ($s_r = 2$), strengthening due to the SiC is only achieved if $\sigma_y^{\mathrm{PFZ}} / \sigma_y^{\mathrm{m}}$ is larger than a critical value (for $s_r = 2$ this critical value is 0.7).

Having successfully applied the present model for a composite with a weak interface layer to data on one specific MMC, it is clear that more work on these type of systems is needed to obtain a full assessment of the accuracy of the model. Especially data on the effect of variation of the aspect ratio of the fibres would enhance understanding of the stress transfer in these composites with a weak interface layer. This kind of understanding can be achieved by finite element modelling, which, in addition, will lead to a detailed examination of the localised microscopic yield behaviour of the weak interface.

Summary

A new version of the shear lag (SL) model for bonded fibres has been derived. This new version (SSSL) accounts for fibre end stresses in an approximate yet realistic manner. It is shown that the SSSL model agrees well with experimental data and resolves some of the discrepancies between Eshelby type models and previous SL type models.

The accuracy and relative simplicity of the SSSL model have been exploited to derive an analytical model for the stress transfer in a composite that contains a weak layer in the matrix adjacent to the reinforcement. Evaluation of the equations for the example of an Al-SiC metal matrix composite shows that a relatively small strength differential of the weak layer with the rest of the matrix can significantly reduce the apparent macroscopic yield strength of the composite. The model predictions are consistent with yield strength measurements of aged 8090 (Al-Li-Cu-Mg) MMC samples.

Acknowledgements

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