

An Investigation of Thermal Ratings for High Voltage Cable Crossings through the use of 3D Finite Element Analysis

Z.Y.Huang , J.A.Pilgrim and P.L.Lewin
University of Southampton, Southampton, UK

DEFINITION OF RESEARCH PROBLEM

The Importance of Cable Crossings

- Cable crossings are inevitably found in urban areas as a result of growing complexity of underground cable systems
- Dangerously high temperatures can occur at crossing points, resulting in premature aging of cable insulation and potentially cable failures
- The only existing explicit rating method is IEC60287 (analytical), but its application/accuracy is restricted by idealistic assumptions



Figure 1 - sample cable crossing in North America
(www.dstar.org/research/project-desc/UG-cable-ampacity)

QUESTION – Are there any alternative methods which can be applied to accurately rate cable crossings with more realistic environmental parameters?

Research / Economical concerns

Project interests

- Effect of ground conditions
- Mutual heat reduction / optimize thermal performance
- Accuracy of IEC 60287

Economical Factors

- Minimize risk
- Minimize ageing
- Minimize capital expenditure

Technical Factors

- Deeply buried
- Large vertical spacing between crossing circuits
- Redesign both circuits for best performance

against

Need to find a compromise between maximisation of power transfer and economical concerns

DEVELOPMENT OF 3D FEA MODEL

Example Cable Crossings

- Conductor size: 800 mm²
Copper conductor: D_c=34.7 mm
XLPE insulation: D_i=72.6 mm
Lead alloy sheath: D_s=78.5 mm
PE serving: D_e=86.8 mm
- 2 x 132 kV single-core armour-free cables crossing at 90 degrees
- 2 x 132 kV three-phase circuits crossing at 90 degrees
- Burial depths:
(upper cable) 0.5 m & 0.75 m, 1.5 m, 1.25 m (lower cable)
(upper cable) 1m & 1.25 m, 1 m, 2.25 m (lower cable)

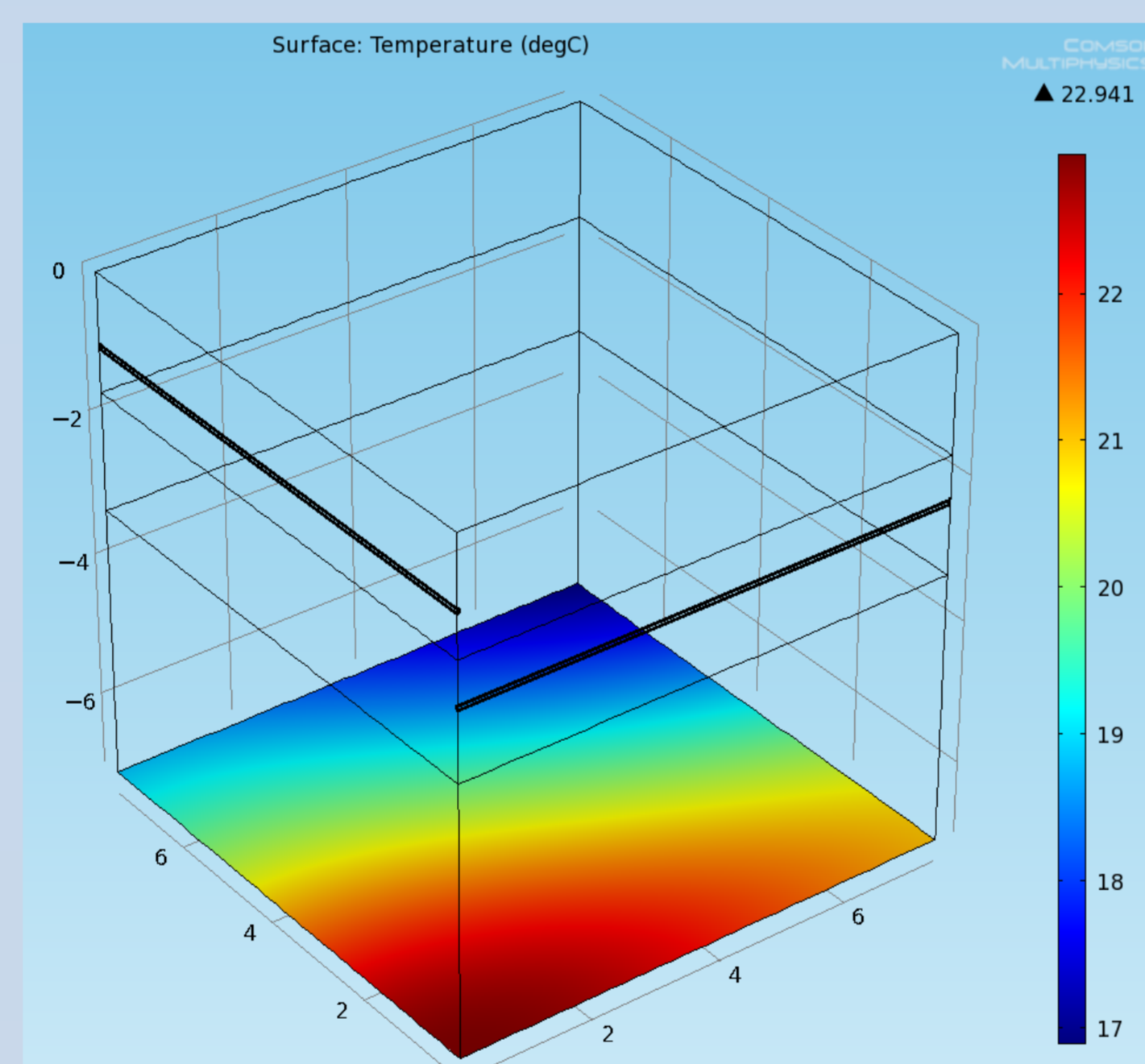


Figure 2 – example temperature plot on bottom boundary

Numerical Modelling

- Model size: 7.5 x 7.5 x 7 m (LxWxH) homogeneous soil, P_s=1.2 Km/W
- Ground surface conditions: isothermal at 12 / 15°C, still air convection, 1 m/s air convection, 10 m/s air convection
- Bottom boundary condition: locally fixed temperature(surface)

$$T(\text{local}) = T(\infty) + \frac{P_s}{2\pi} \times Wt \times \ln \frac{d'}{d}$$

P_s = soil thermal resistivity, Km/W

Wt = total losses inside the cable, W/m

d = distance between the point under consideration and actual buried cable, m

d' = distance between the point under consideration and image cable above the ground, m

- Side wall boundary condition: thermal insulation/symmetry
- Heat sources : Joule loss, dielectric loss, sheath loss

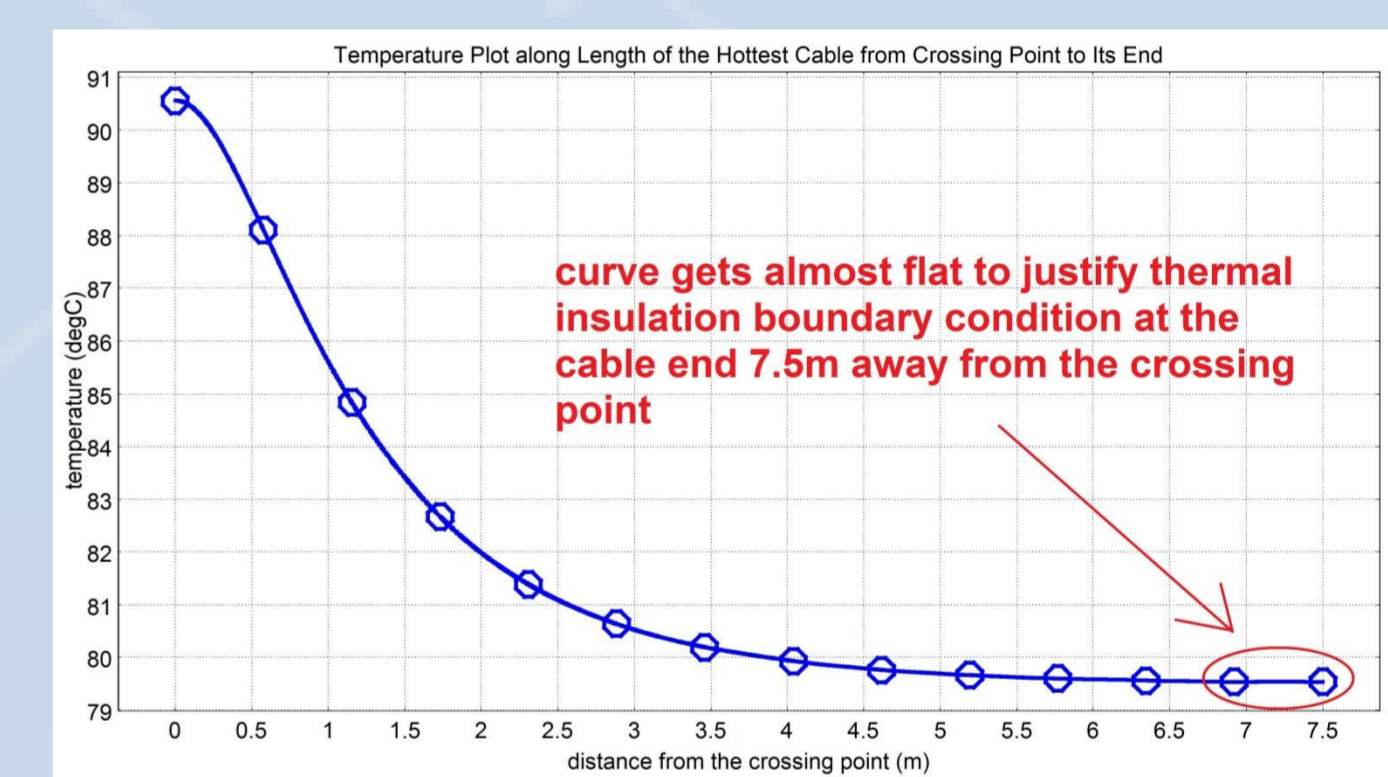


Figure 3 - temperature plot along length of the hottest cable

RESULTS AND IMPLICATIONS

Single Cable Modelling Results

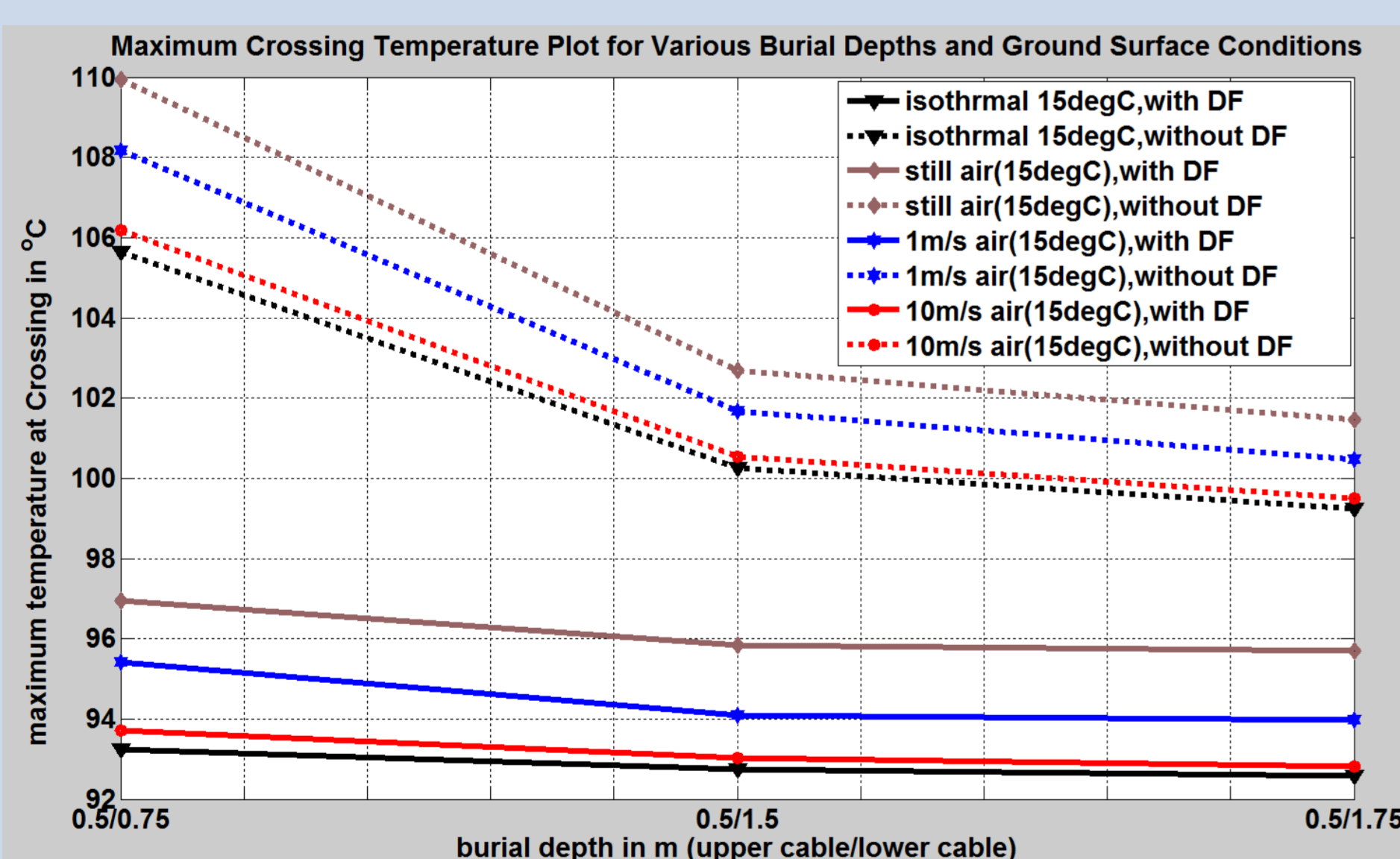


Figure 4 - crossing temperature plot for various burial and ground conditions part 1

- Applying Derating factor (DF) from IEC60287(Std) reduces temperatures, but still above 90°C
- The magnitude of the excess temperature depends on ground boundary conditions

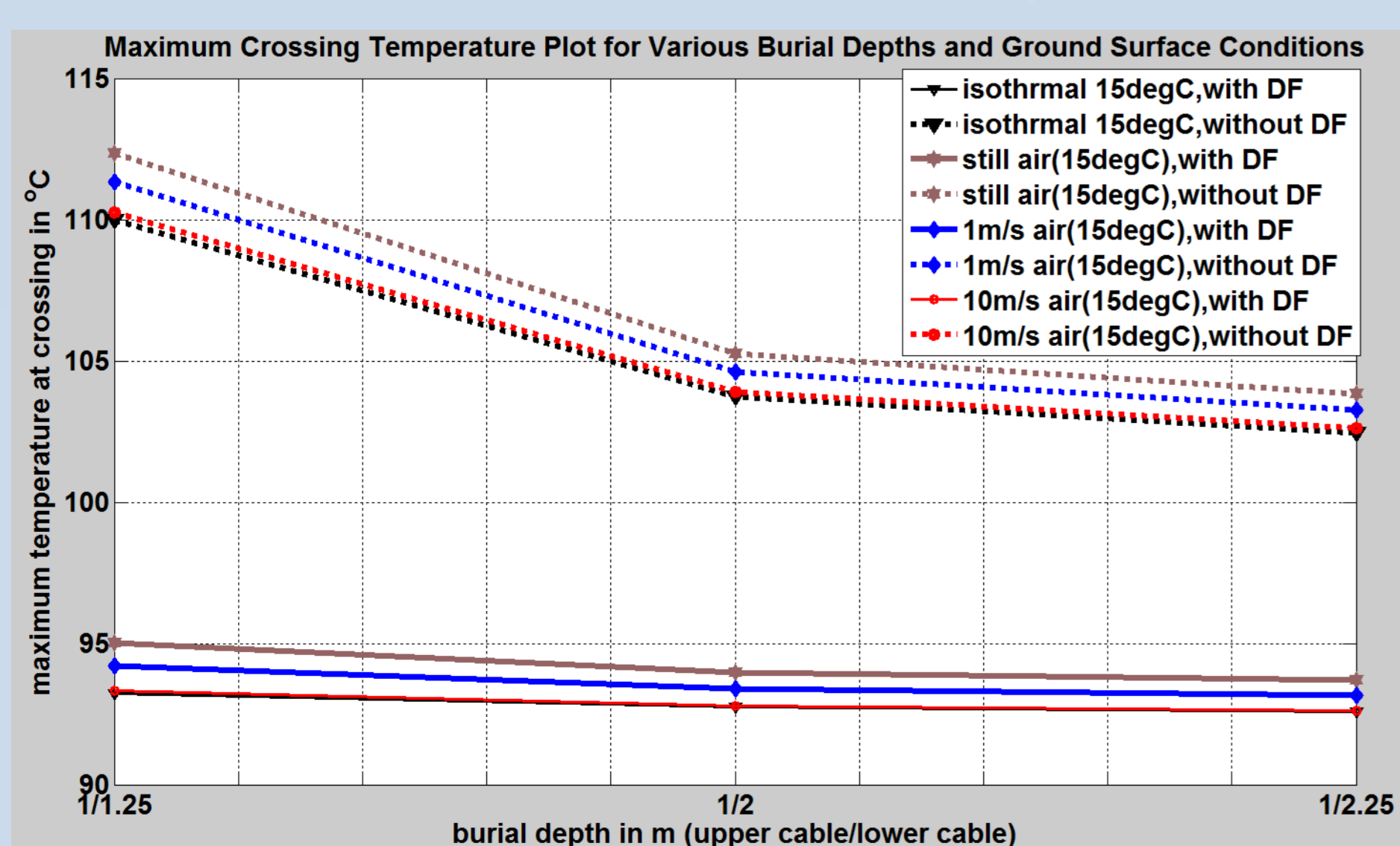


Figure 5 - crossing temperature plot for various burial and ground conditions part 2

- The match between FEA and IEC 60287 results improves with increasing burial depth and vertical spacing between two crossing circuits
- This is due to the reduced effect of the ground condition surface with increasing burial depth

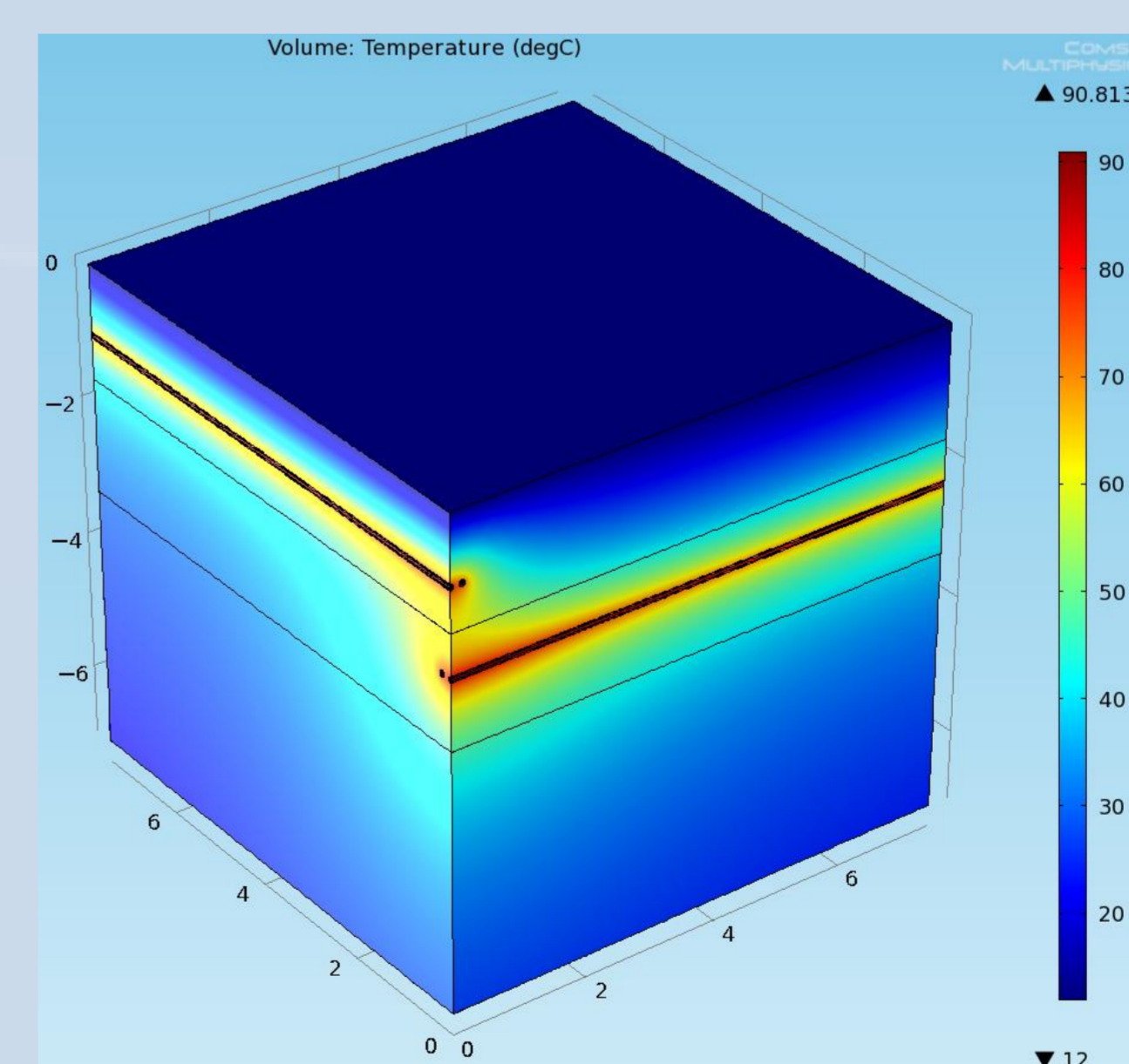


Figure 6 – volume temperature profile of two three-phase cable crossing at 90 degrees

- Extend single cable crossing model to three-phase circuits crossing
- Trends match single cable case but over-rating increases
- Because the total heat generated is increasing, ground condition imposes a stronger effect on the overall crossing thermal performance

Implication & Further research

- The isothermal ground boundary assumption in IEC60287 for crossing rating calculation is necessary for quick analytical calculation. However, it reduces the accuracy of calculations for practical applications.
- Ground surface condition has a strong effect on crossing thermal performance so that an understanding of its effect is vital for accurate rating strategy.
- Further study will focus on how good is IEC60287 can be applied in crossing rating problems quantitatively.

Contact details : zh2g09@ecs.soton.ac.uk

University of Southampton, Highfield, Southampton, SO17 1BJ, UK