

Dual-Layered MIMO Transmission for Increased Bandwidth Efficiency

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Abstract—A dual-layered downlink transmission scheme is proposed for intrinsically amalgamating multiple-input-multiple-output (MIMO) spatial multiplexing (SMX) with spatial modulation (SM). The proposed scheme employs a classic SMX transmission that is known to offer superior bandwidth efficiency (BE) compared with SM. We exploit receive-antenna-based SM (RSM) on top of this transmission as an enhancement of the BE. The RSM here is applied to the combined spatial and power-level domain not by activating and deactivating the RAs but rather by choosing between two power levels $\{P_1, P_2\}$ for the received symbols in these antennas. In other words, the combination of symbols received at a power level P_1 carries information in the spatial domain in the same manner as the combination of nonzero elements in the receive symbol vector carries information in the RSM transmission. This allows for the coexistence of RSM with SMX, and the results show increased BE for the proposed scheme compared with both SMX and SM. To characterize the proposed scheme, we carry out a mathematical analysis of its performance, and we use this to optimize the ratio between P_1 and P_2 for attaining the minimum error rates. Our analytical and simulation results demonstrate significant BE gains for the proposed scheme compared with conventional SMX and SM.

Index Terms—Multiple-input-multiple-output systems, spatial modulation (SM), spatial multiplexing (SMX), transmit precoding (TPC).

I. INTRODUCTION

MULTIANTENNA-aided transceivers have been shown to improve the capacity of the wireless channel by means of spatial multiplexing (SMX) [1]. For the multiuser downlink (DL), transmit precoding (TPC) schemes have been shown to improve both the attainable power efficiency (PE) and the cost of mobile terminals by shifting the signal processing complexity to the base stations (BSs). Numerous TPC solutions

exist, ranging from highly complex capacity achieving nonlinear dirty paper coding techniques [2] and their low-complexity suboptimal counterparts in the form of Tomlinson–Harashima precoding [3]–[6] to linear TPC schemes based on channel inversion [7]–[12] that offers the lowest complexity, albeit at an inferior performance. The performance–complexity tradeoffs between the above TPC have been thoroughly studied in the literature. More recently, it has been shown that the family of linear techniques exhibits a close-to-optimal performance in the large-scale multiple-input-multiple-output (MIMO) region [13]–[15]. Accordingly, we focus on the class of low-complexity closed-form linear TPC [7]–[12] due to their favorable performance–complexity tradeoff and practical relevance.

More recently, spatial modulation (SM) has been conceived for implicitly encoding information in the index of the specific antenna activated for the transmission of the modulated symbols, offering a low-complexity design alternative [16]. Its central benefits include the absence of interantenna interference (IAI) and the fact that it only requires a subset (down to one) of radio-frequency (RF) chains compared with SMX. Accordingly, the interantenna synchronization is also relaxed. Early work has focused on the design of receiver algorithms for minimizing the bit error ratio (BER) of SM at low complexity [16]–[21]. The work spans from matched filtering as a low-complexity technique for detecting the antenna index used for SM [16] to the maximum likelihood (ML) [20] with a significantly reduced complexity compared with classic SMX ML detectors, including compressive sensing approaches [18] and performance analyses [19]. Reduced-space sphere detection has also been proposed for SM in [21] for further complexity reduction where a generalized SM transmission was also explored [22]. In addition to receive processing, recent work has also proposed constellation shaping for SM [23]–[33]. Specifically, the work on this topic has focused on three main directions: shaping and optimization of the spatial constellation, i.e., the legitimate sets of activated transmit antennas (TAs) [23], modulation constellation shaping [24]–[28] for the SM and space shift keying transmission, where the constellation of the modulated bits is optimized, and joint spatial and modulation constellation shaping, in the form of optimizing the received constellation [29]–[33].

Closely related work has focused on applying the concept of SM to the receive antennas (RAs) of the communication link, as opposed to the TAs as per the above approaches, forming the RA-based spatial modulation (RSM) concept [36]–[39]. By means of TPC, this technique targets a specific subset of RAs, which receive information symbols, whereas the rest of the RAs

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85 receive only noise. This may be achieved by using zero-forcing
86 (ZF) TPC and transmitting a combination of information sym-
87 bols and zeros to the RAs, depending on the spatial symbols
88 to convey. As opposed to conventional SM where a subset of
89 RF chains is deployed, here, all TAs and RAs are active and
90 therefore there are no RF chain reductions. Still, the computa-
91 tional complexity of the receivers is drastically reduced, where
92 simply the indexes of the targeted RAs have to be detected,
93 and the classic symbols received at the activated RAs are then
94 demodulated.

95 Inspired by the above RSM philosophy, here, we propose
96 a dual-layered transmission (DLT) scheme, which intrinsically
97 amalgamates a full spatial multiplexing (SMX) with SM. First,
98 we note that since, for RSM, all TAs and RAs are active, there
99 are no RF chain reductions, and this motivates the full SMX
100 approach. To accommodate the SMX, we apply an SM to the
101 combined spatial and receive-power domain, where instead of
102 sending a combination of information symbols and zero power
103 to the RAs, we apply two different power levels for distinguish-
104 ing between the “active” and “inactive” RAs. In this manner, the
105 spatial symbols are formed based on the power levels detected.
106 We demonstrate that this improves the bandwidth efficiency
107 (BE) with respect to SMX and SM. Against this state of the
108 art, we list the main contributions of this paper.

- 110 • We propose a new DLT scheme based on linear TPC that
111 improves the BE by jointly exploiting the benefits of SMX
112 and RSM.
- 113 • We provide the performance analysis of the proposed
114 technique based on the pairwise error probability (PEP)
115 between different constellation points in the supersymbol
116 constellation formed by the combination of the spatial
117 constellation of RSM and the classic modulation constel-
118 lation of SMX.
- 119 • We use the above results for analytically deriving the
120 optimum power ratio between the two sets of antennas
121 that carry the spatial symbol for the proposed scheme for
122 minimizing the probability of detection errors.
- 123 • We calculate and compare analytically the complexity of
124 the conventional and proposed techniques, and quantify
125 the performance–complexity tradeoff of conventional and
126 proposed schemes, by introducing a PE metric that com-
127 bines the BE, transmit power, and complexity, to prove
128 the enhanced tradeoff for the proposed scheme.

129 *Remark 1:* It should be noted that, while this paper focuses
130 on a single-link scenario, the proposed technique can be readily
131 extended to a multiuser DL scenario, where the DLT and the
132 related RSM take place on a per-user basis, as facilitated by the
133 ZF-TPC employed at the BS.

134 *Remark 2:* The proposed scheme does not consist of a power
135 allocation scheme in the sense of allocating power according
136 to the quality-of-service (QoS) requirements of the user. This
137 power allocation may be applied in addition to the proposed
138 scheme in the multiuser scenario, where different users with
139 different QoS requirements employ different sets of power
140 levels $\{P_1, P_2\}$ accordingly.

141 *Remark 3:* To facilitate the proposed power-level modula-
142 tion, this paper focuses on phase shift keying (PSK) in terms

of the classical symbol modulation. Its adaptation to quadrature
143 amplitude modulation (QAM) is not trivial since the variability
144 of the power levels for the classically modulated symbols
145 would hinder the detection of the power levels of the spatially
146 modulated symbols. Nevertheless, even for PSK modulation,
147 our results illustrate a wide range of achievable BEs for the
148 proposed scheme and an improved performance compared with
149 classical SMX associated with both PSK and QAM for the
150 same BE.

The remainder of this paper is organized as follows. Section II
152 presents the MIMO system model and introduces the RSM
153 transmission philosophy. Section III details the proposed DLT
154 scheme, whereas in Section IV, we present our analytical study
155 of the performance attained and the analytical optimization
156 of the power ratio for the proposed scheme. Section V detail
157 the complexity calculation and the study of the attainable PE.
158 Finally, Section VI presents our numerical results, whereas our
159 conclusions are offered in Section VII.

II. SYSTEM MODEL AND RECEIVE-ANTENNA-BASED SPATIAL MODULATION

A. System Model

Consider a MIMO system, where the transmitter and receiver
164 are equipped with N_t and N_r antennas, respectively. For sim-
165 plicity, unless stated otherwise, in this paper, we assume that the
166 transmit power budget is limited as $P = 1$. For the case of
167 the closed-form TPCs of [7]–[12], it is required that $N_t \geq N_r$.
168 The given channel is modeled as follows:

$$\mathbf{y} = \mathbf{H}\mathbf{t} + \mathbf{w} \quad (1)$$

where \mathbf{y} is the vector of received symbols in all RAs, and \mathbf{H} is
170 the MIMO channel vector with elements $h_{m,n}$ representing the
171 complex channel coefficient between the n th TA and the m th
172 RA. Furthermore, \mathbf{t} is the vector of precoded transmit symbols
173 that will be discussed in the following, and $\mathbf{w} \sim \mathcal{CN}(0, \sigma^2 \mathbf{I})$
174 is the additive white Gaussian noise (AWGN) component at
175 the receiver, with $\mathcal{CN}(\mu, \sigma^2)$ denoting the circularly symmet-
176 ric complex Gaussian distribution with a mean of μ and a
177 variance of σ^2 .

B. Receive-Antenna-Based Spatial Modulation

The block diagram of RSM as proposed in [36] is shown
180 in Fig. 1(a). RSM targets a subset of the RAs by sending
181 information symbols to these RAs and zero power to the rest
182 of the RAs. While for RSM all RAs have to be on to detect
183 the arrival of information symbols, for coherence with the
184 SM literature, we shall refer to the antennas as “active” and
185 “inactive,” depending on whether they do or do not receive
186 information symbols, respectively. The specific combination of
187 RAs that do receive symbols implicitly conveys the symbol
188 transmitted in the spatial domain. The above RA subset trans-
189 mission is achieved by forming a supersymbol vector in the
190 form $\mathbf{s}_m^k = \mathbf{e}_k b_m = [0, \dots, b_{m_1}, \dots, 0, \dots, b_{m_2}, \dots, 0]^T$ with
191 N_a nonzero elements, where \mathbf{e}_k is a diagonal matrix of size 192

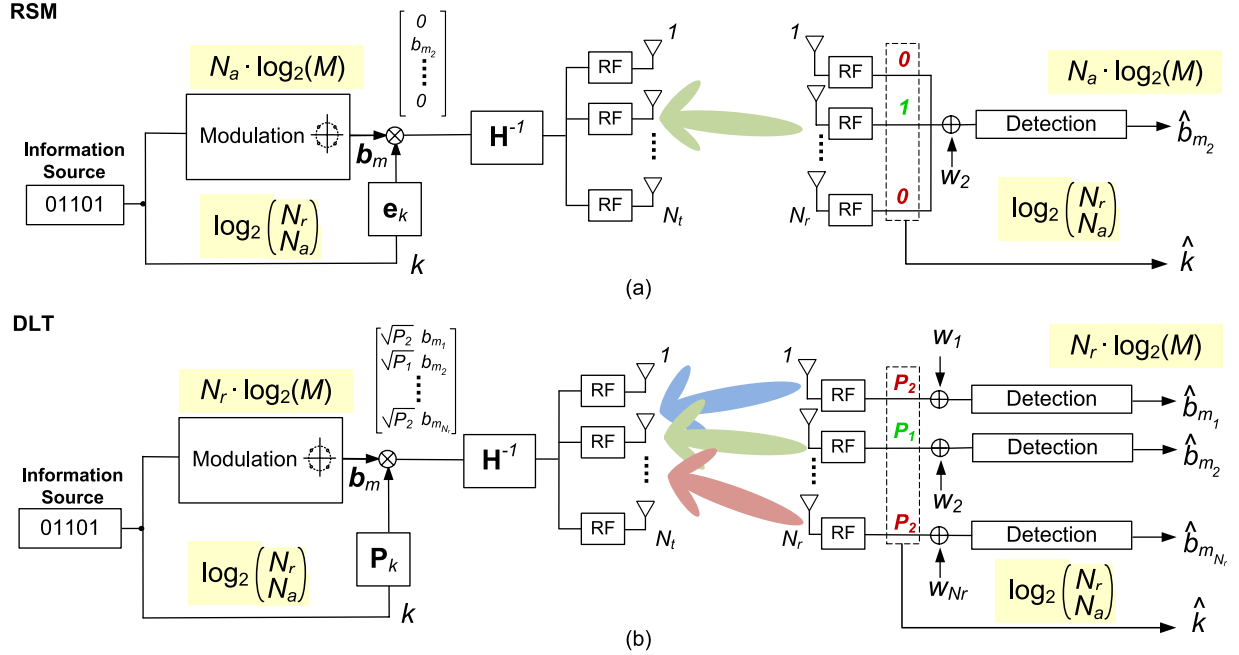


Fig. 1. Block diagram of (a) RSM and (b) DLT transmission.

193 N_r with elements taken from the set $\{1, 0\}$ on its diagonal, 194 which represents the RAs that are activated. The notation $[\cdot]^T$ 195 denotes the transpose operator. Here, $b_{m_i}, m_i \in \{1, \dots, M\}$ 196 is a symbol taken from an M -order modulation alphabet that 197 represents the transmitted waveform in the baseband domain 198 conveying $\log_2(M)$ bits and k represents the index of the 199 N_a activated RAs (the index of the nonzero elements in \mathbf{s}_m^k) 200 conveying $\log_2(N_r/N_a)$ bits in the spatial domain. Accordingly, 201 the total number of bits conveyed per supersymbol for RSM is

$$\beta = N_a \log_2(M) + \log_2\left(\frac{N_r}{N_a}\right). \quad (2)$$

202 The transmitter then sends

$$\mathbf{t} = f \mathbf{T} \mathbf{s}_m^k \quad (3)$$

203 where $\mathbf{T} = \mathbf{H}^H (\mathbf{H} \mathbf{H}^H)^{-1}$ is the ZF-TPC [7] that preserves 204 the form of \mathbf{s}_m^k at the receiver. The factor $f = \sqrt{1/\text{tr}(\mathbf{T} \mathbf{T}^H)}$, 205 where $\text{tr}(\cdot)$ denotes the trace operator and normalizes the 206 average transmit power to $P = 1$. The received symbol vector 207 can be written as

$$\mathbf{y} = f \mathbf{H} \mathbf{T} \mathbf{s}_m^k + \mathbf{w} = f \mathbf{s}_m^k + \mathbf{w} \quad (4)$$

208 where, clearly, all IAI is removed. At the receiver, a joint ML 209 detection of both the RA index and the transmit symbol is 210 obtained by the following minimization:

$$\begin{aligned} [\hat{s}_m, \hat{k}] &= \arg \min_i \|\mathbf{y} - \hat{\mathbf{y}}_i\| \\ &= \arg \min_{m_i, k_i} \|\mathbf{y} - f \mathbf{H} \mathbf{T} \mathbf{s}_{m_i}^{k_i}\| \end{aligned} \quad (5)$$

211 where $\|\mathbf{x}\|$ denotes the norm of vector \mathbf{x} , and $\hat{\mathbf{y}}_i$ is the i th 212 constellation point in the received SM constellation. A low-

complexity decoupled approach is also proposed in [36], where 213 the first active antenna indexes are detected in the form of 214

$$\hat{k} = \arg \max_{j \in \mathcal{J}} \sum_{i=1}^{N_a} |y_{j,i}|^2 \quad (6)$$

where \mathcal{J} denotes the set of symbols in the spatial domain, and 215 then, the classic modulated symbols are detected by 216

$$\hat{b}_{m_i} = \arg \min_{n_i \in \mathcal{Q}} |y_{\hat{k},i}/f - b_{n_i}|^2 \quad (7)$$

where \mathcal{Q} denotes the modulation constellation, and b_{n_i} are 217 the symbols in the modulated symbol alphabet. For reasons of 218 computational complexity, we shall focus on the latter detector 219 in this paper. 220

III. PROPOSED DUAL-LAYERED TRANSMISSION 221

From the above system description, it can be seen that for 222 the particular case of RSM, while the detection complexity 223 is clearly reduced with respect to SMX, there are no savings 224 in RF complexity since all N_r RAs have to be activated and 225 receiving for the detection in (6) and (7). Still, by forming a 226 subset of beams towards the receiver, as shown in Fig. 1(a), 227 the BE, i.e., the number of bits per channel use, is generally 228 lower for RSM than for SMX. Motivated by this, we propose 229 a dual-layered approach combining SMX with RSM, where 230 the BE of conventional SMX MIMO transmission is strictly 231 enhanced by encoding spatial bits in the RSM fashion in the 232 received power domain, by selecting two distinct, nonzero 233 power levels for the transmitted supersymbols instead of the 234 “on-off” RSM transmission in the $\{1, 0\}$ manner. This allows 235 for nonzero elements throughout the supersymbol vector \mathbf{s}_m^k , 236

hence supporting a full SMX transmission in the modulated signal domain. The block diagram of the proposed DLT is shown in Fig. 1(b).

1) *Transmitter*: Here, we employ a full data vector in the form of $\mathbf{b}_m = [b_{m_1}, b_{m_2}, \dots, b_{m_{N_r}}]^T$, with all elements being nonzero, and the encoding of the spatial bits is achieved by allocating different power levels to the received symbols according to the spatial symbol k , by applying the power allocation matrix \mathbf{P}_k , i.e.,

$$\mathbf{s}_m^k = \mathbf{P}_k \mathbf{b}_m = [s_{m_1}, s_{m_2}, \dots, s_{m_{N_r}}]^T \quad (8)$$

with

$$\mathbf{P}_k = \begin{bmatrix} \sqrt{p_1} & 0 & \dots & 0 \\ 0 & \sqrt{p_2} & \dots & 0 \\ \vdots & \vdots & \ddots & \vdots \\ 0 & 0 & \dots & \sqrt{p_{N_r}} \end{bmatrix} \quad (9)$$

where $p_i, i \in [1, N_r]$ are taken from the set $\{P_1, P_2\}$ according to the spatial symbol k . Note that classic QoS-based power allocation can be applied in addition to this process by employing an additional power allocation matrix on top of (9). The receiver can then remove this additional matrix by simple inversion, in order to detect the spatial symbol. For notational simplicity and to keep the focus of the discussion on the proposed concept, we neglect QoS-based power allocation.

2) *Receiver*: At the receiver side, the explicit knowledge of the power levels $\{P_1, P_2\}$ is not required, as long as the detector can distinguish between the two power levels. The received signal of (4) can be decomposed as

$$y_p = f\sqrt{P_1}b_{m_p} + w_p, p \in \mathcal{A} \quad (10)$$

$$y_q = f\sqrt{P_2}b_{m_q} + w_q, q \in \mathcal{I} \quad (11)$$

where \mathcal{A} and \mathcal{I} denote the sets of “active” and “inactive” antennas, respectively. Hence, the receive processing is similar to the conceived one for RSM, with the difference that the classic modulated symbols of all RAs have to be detected, as opposed to those of N_a antennas only for RSM. Accordingly, the receiver first detects the set of antennas with the highest received power levels and then detects the classic modulated symbols at all RAs according to

$$\hat{k} = \arg \max_{j \in \mathcal{J}} \sum_{i=1}^{N_a} |y_{j,i}|^2 \quad (12)$$

where \mathcal{J} denotes the set of symbols in the spatial domain, and

$$\hat{\mathbf{b}}_m = \arg \min_{n \in \mathcal{Q}} |\mathbf{y}/f - \mathbf{b}_n|^2 \quad (13)$$

where \mathcal{Q} denotes the classic modulation constellation, and b_n are the symbols in the modulated symbol alphabet.

TABLE I
BE IN BITS PER CHANNEL USE FOR SMX, RSM, AND DLT

	Bandwidth Efficiency (BE)
SMX	$\beta = N_r \log_2(M)$
RSM	$\beta = N_a \log_2(M) + \log_2 \binom{N_r}{N_a}$
DLT	$\beta = N_r \log_2(M) + \log_2 \binom{N_r}{N_a}$

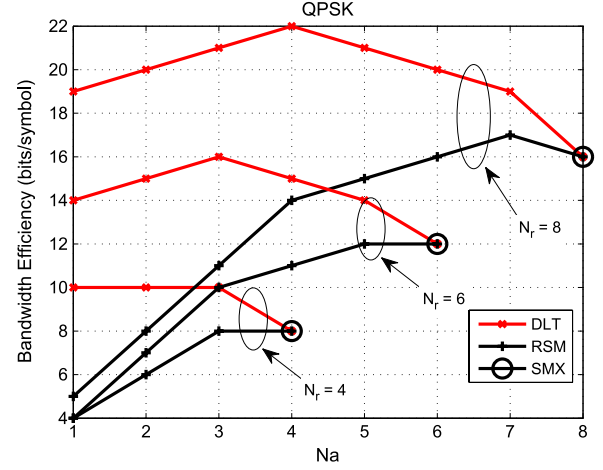


Fig. 2. BE versus N_a for SMX, RSM, and DLT using the expressions of Table I.

A. Bandwidth Efficiency

Clearly, the encoding process in (8) and (9) encodes $N_r \log_2(M)$ bits in the modulated symbol domain and an additional $\log_2 \binom{N_r}{N_a}$ bits in the spatial domain. This results in a total of

$$\beta = N_r \log_2(M) + \log_2 \binom{N_r}{N_a} \quad (14)$$

bits per transmitted supersymbol for DLT, which is strictly greater than that for SMX and RSM. Here, the notation N_a denotes the number of antennas receiving symbols at the power level P_1 . We should emphasize that, although all RAs are active for both RSM and the proposed DLT, for coherence with the literature, we shall adhere to the terms “active” and “inactive” to indicate the antennas receiving $\{1, 0\}$ and $\{P_1, P_2\}$ for RSM and DLT, respectively. A comparison of the BEs of SMX, RSM, and DLT is shown in Table I, where it can be seen that the proposed DLT approach has an improved BE compared with the conventional approaches. This is quantified in Fig. 2, where the BE is expressed in terms of bits per channel use is shown with increasing numbers of “active” antennas N_a for MIMO links with $N_r = 4$, $N_r = 6$, and $N_r = 8$, where the clear benefits of the proposed approach can be seen. It can be observed that the additional BE of DLT compared with SMX can be maximized by appropriately selecting the number of activated antennas according to

$$\tilde{N}_a = \arg \max_{N_a} \log_2 \binom{N_r}{N_a} = N_r/2 \quad (15)$$

which is demonstrated in the figure.

294 B. Symbol Power Levels

295 With regard to the resulting BER performance, the set of
296 spatial power levels $\{P_1, P_2\}$ must be carefully selected so that
297 they satisfy a combination of two constraints.
298

- 299 1) There is sufficient separation between the two power lev-
300 els P_1, P_2 for correct detection of the “active” antennas
301 and hence the spatial symbol k in the presence of noise.
- 302 2) The symbols received with $P_2 < P_1$ that dominate the
303 BER of the modulated symbol detection must experience
304 a sufficiently high signal-to-noise ratio (SNR) that is
305 adequate for reliable demodulation.

306 Let us therefore define the power ratio

$$\alpha = \frac{P_2}{P_1} \quad (16)$$

307 as the ratio between the two power levels transmitted, which
308 is optimized in the following results. Since N_a symbols are
309 transmitted with power P_1 and the remaining $N_r - N_a$ symbols
310 have power of P_2 , given a total power budget of $P = 1$, we have

$$P_1 = \frac{1}{(N_r - N_a)\alpha + N_a} \quad (17)$$

$$P_2 = \frac{\alpha}{(N_r - N_a)\alpha + N_a}. \quad (18)$$

311 Clearly, since the power levels P_1, P_2 influence the reliability
312 of detection for the modulated symbols and since the ratio α
313 determines the detection reliability of the spatial symbols, α
314 can be optimized for best BER performance. In the following,
315 we derive a closed-form expression for the optimum α value
316 for an M -order PSK modulation, where it can be seen that this
317 optimum value is independent of both N_r and of N_a .

318 *Remark:* Regarding the effect of the above on the transmit
319 power distribution, we note that the power imbalance discussed
320 refers to the information symbols s_m^k and does not translate
321 to a power imbalance for the transmit symbols \mathbf{t} . Indeed, the
322 ZF-precoded transmit symbols have the same average transmit
323 power, constrained by the scaling factor f as shown above,
324 which is valid for both the proposed DLT and for the conven-
325 tional SMX, and these transmit symbols exhibit the same power
326 distribution for both techniques. In other words, the proposed
327 scheme does not impact the design of the power amplifiers used
328 at the transmitter.

329 To verify the above, Fig. 3 shows the probability density
330 function (pdf) of the normalized transmit power per antenna
331 for both SMX and DLT in a (8×4) element MIMO system. It
332 can be seen that, as expected, both techniques show the same
333 distribution of transmit power.

334 IV. DUAL-LAYERED TRANSMISSION PERFORMANCE

335 ANALYSIS AND OPTIMUM POWER RATIO α

336 A. Probability of Error

337 Here, we carry out a performance analysis for the proposed
338 DLT scheme by deriving the PEP between the pair of symbols

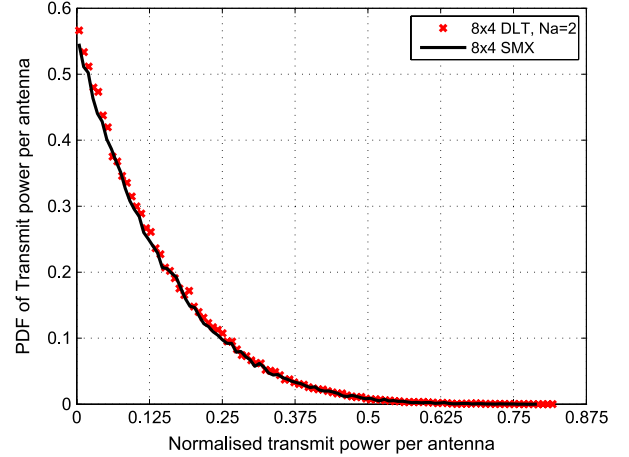


Fig. 3. PDF of transmit power per antenna for a (8×4) MIMO with SMX and DLT and QPSK with Rayleigh fading.

s_m^k and s_n^l in the superimposed spatial and classic modulation 339 constellations, following the analysis in [36]. Accordingly, we 340 define the PEP as $\mathcal{P}(s_m^k \rightarrow s_n^l)$ and use the union bound for the 341 average bit error probability P_e , which is expressed as 342

$$P_e \leq \frac{1}{\beta} E \left\{ \sum_{s_m^k \in \mathcal{B}} \sum_{s_n^l \in \mathcal{B} \setminus s_m^k} d(s_m^k, s_n^l) \mathcal{P}(s_m^k \rightarrow s_n^l) \right\} \quad (19)$$

where $d(s_m^k, s_n^l)$ is the Hamming distance between the bit 343 representations of symbols s_m^k, s_n^l and $\mathcal{B} = \mathcal{J} \cup \mathcal{Q}$ is the super- 344 symbol constellation defined as the union of the spatial domain 345 constellation and the classic modulation constellation. We have 346 used the operator \cup to define the union of sets. For the PEP, we 347 have the following theorem. 348

Theorem 1: The PEP $\mathcal{P}(s_m^k \rightarrow s_n^l)$ for DLT can be expressed as 349

$$\mathcal{P}(s_m^k \rightarrow s_n^l) = Q \left(\frac{f}{\sqrt{N_0}} \left(1 - \sum_{i=1}^{N_r} \sqrt{p_{k_i} p_{l_i}} \mathcal{R}\{b_{m_i}^* b_{n_i}\} \right) \right) \quad (20)$$

where $Q(\cdot)$ denotes the Gaussian q -function [42], $\mathcal{R}\{\cdot\}$ denotes 350 the real part of a number, $(\cdot)^*$ denotes the complex conjugate 351 operation, and $N_0 = 2\sigma^2$ is the noise power spectral density. 352

Proof: Let us first define $\mathbf{r} = \mathbf{y}/f$ and $\mathbf{v} = \mathbf{w}/f$ for 353 use in the following expressions. The PEP of the supersymbol 354 constellation can be expressed as 355

$$\begin{aligned} \mathcal{P}(s_m^k \rightarrow s_n^l) &= \mathcal{P}(\|\mathbf{r} - s_m^k\|^2 > \|\mathbf{r} - s_n^l\|^2) \\ &= \mathcal{P} \left(\sum_{i=1}^{N_r} p_{k_i} |b_{m_i}|^2 - 2\mathcal{R}\{r_i^* \sqrt{p_{k_i}} b_{m_i}\} \right. \\ &\quad \left. > \sum_{i=1}^{N_r} p_{l_i} |b_{n_i}|^2 - 2\mathcal{R}\{r_i^* \sqrt{p_{l_i}} b_{n_i}\} \right). \end{aligned} \quad (21)$$

Since, for PSK signals, we have $|b_{m_i}| = 1$, by rearranging 356 the terms in the probability expression, (21) can be further 357

358 simplified as

$$\mathcal{P}(s_m^k \rightarrow s_n^l) = \mathcal{P}\left(\sum_{i=1}^{N_r} \mathcal{R}\{r_i^* \sqrt{p_{l_i}} b_{n_i}\} - \mathcal{R}\{r_i^* \sqrt{p_{k_i}} b_{m_i}\} \right. \\ \left. > \frac{\sum_{i=1}^{N_r} p_{l_i} - \sum_{i=1}^{N_r} p_{k_i}}{2}\right). \quad (22)$$

359 Since $\sum_{i=1}^{N_r} p_{l_i} = \sum_{i=1}^{N_r} p_{k_i} = 1$ and $r_i = \sqrt{p_{k_i}} b_{m_i} + v_i$, we
360 have

$$\mathcal{P}(s_m^k \rightarrow s_n^l) = \mathcal{P}\left(\sum_{i=1}^{N_r} \mathcal{R}\{\sqrt{p_{k_i}} b_{m_i}^* \sqrt{p_{l_i}} b_{n_i}\} + \mathcal{R}\{v_i^* \sqrt{p_{l_i}} b_{n_i}\} \right. \\ \left. > \sum_{i=1}^{N_r} p_{k_i} |b_{m_i}|^2 + \mathcal{R}\{v_i^* \sqrt{p_{k_i}} b_{m_i}\}\right) \\ = \mathcal{P}\left(\sum_{i=1}^{N_r} \mathcal{R}\{v_i^* (\sqrt{p_{l_i}} b_{n_i} - \sqrt{p_{k_i}} b_{m_i})\} \right. \\ \left. > 1 - \sum_{i=1}^{N_r} \sqrt{p_{k_i} p_{l_i}} \mathcal{R}\{b_{m_i}^* b_{n_i}\}\right). \quad (23)$$

361 Let us define the random variable $\chi \triangleq \sum_{i=1}^{N_r} \mathcal{R}\{v_i^* (\sqrt{p_{l_i}} b_{n_i} -$
362 $\sqrt{p_{k_i}} b_{m_i})\}$ for which we have $\chi \in \mathcal{N}(0, AN_0/f^2)$ with

$$A = \frac{\sum_{i=1}^{N_r} p_{l_i} |b_{n_i}|^2 + p_{k_i} |b_{m_i}|^2}{2} = \frac{1}{2} \sum_{i=1}^{N_r} p_{l_i} + p_{k_i}. \quad (24)$$

363 For the unity transmit power assumed in this paper, it can be
364 seen from (24) that $A = 1$. Accordingly, for the PEP, we have

$$\mathcal{P}(s_m^k \rightarrow s_n^l) = \mathcal{P}\left(\chi > 1 - \sum_{i=1}^{N_r} \sqrt{p_{k_i} p_{l_i}} \mathcal{R}\{b_{m_i}^* b_{n_i}\}\right) \quad (25)$$

365 which, for $\chi \in \mathcal{N}(0, N_0/f^2)$, leads to (20). ■

366 B. Optimum Power Ratio α

367 As mentioned earlier, the power ratio α determines the
368 reliability of detection for the spatial symbol, whereas the lower
369 power level P_2 dominates the BER performance of the classic
370 modulated symbols' detection. As the probability of error in
371 (19) is dominated by the maximum PEP, the optimum power
372 ratio should be selected as

$$\alpha_{\text{opt}} = \arg \min_{\alpha} \max_{s_m^k, s_n^l} \{\mathcal{P}(s_m^k \rightarrow s_n^l)\}. \quad (26)$$

373 To simplify the analysis, we shall treat the errors in the spatial
374 and classic modulated symbols separately. Accordingly, for the
375 maximum PEP $\mathcal{P}_m(s_{m_i}^k \rightarrow s_{m_i}^l)$ in the spatial domain only, we
376 have the following theorem.

Theorem 2: The maximum PEP $\mathcal{P}_m(s_{m_i}^k \rightarrow s_{m_i}^l)$ for the 377
spatial symbols in DLT can be expressed as 378

$$\mathcal{P}_m(s_{m_i}^k \rightarrow s_{m_i}^l) = Q\left(\frac{f}{\sqrt{N_0}} \cdot \frac{\sqrt{P_2} - \sqrt{P_1}}{2}\right). \quad (27)$$

Proof: The maximum PEP in the spatial domain involves 379
the adjacent symbols of different power levels in the supersym- 380
bol constellation and can be expressed as 381

$$\mathcal{P}_m(s_{m_i}^k \rightarrow s_{m_i}^l) \\ = \mathcal{P}\left(\|r_i - s_{m_i}^k\|^2 > \|r_i - s_{m_i}^l\|^2\right) \\ = \mathcal{P}\left(P_1 - 2\mathcal{R}\{r_i^* \sqrt{P_1} b_{m_i}\} > P_2 - 2\mathcal{R}\{r_i^* \sqrt{P_2} b_{m_i}\}\right) \quad (28)$$

where, using $r_i = \sqrt{p_{k_i}} b_{m_i} + v_i$, we get 382

$$\mathcal{P}_m(s_{m_i}^k \rightarrow s_{m_i}^l) \\ = \mathcal{P}\left(P_1 - 2P_1 |b_{m_i}|^2 - 2\mathcal{R}\{u_i^* \sqrt{P_1} b_{m_i}\} \right. \\ \left. > P_2 - 2\sqrt{P_1 P_2} |b_{m_i}|^2 - 2\mathcal{R}\{u_i^* \sqrt{P_2} b_{m_i}\}\right) \\ = \mathcal{P}\left(2(\sqrt{P_2} - \sqrt{P_1}) \mathcal{R}\{u_i^* b_{m_i}\} > P_1 + P_2 - 2\sqrt{P_1 P_2}\right) \\ = \mathcal{P}\left(-\mathcal{R}\{u_i^* b_{m_i}\} > \frac{\sqrt{P_1} - \sqrt{P_2}}{2}\right). \quad (29)$$

Similarly to the given proof, we have used the fact 383
that $|b_{m_i}|^2 = 1$, and it can be seen that $\psi \triangleq -\mathcal{R}\{u_i^* b_{m_i}\} \in$ 384
 $\mathcal{N}(0, N_0/f^2)$. Accordingly, for the minimum PEP in the spatial 385
constellation, we have 386

$$\mathcal{P}_m(s_{m_i}^k \rightarrow s_{m_i}^l) = \mathcal{P}\left(\psi > \frac{\sqrt{P_2} - \sqrt{P_1}}{2}\right) \quad (30)$$

which leads to (27). ■ 387

This indicates that the separation between $\{P_1, P_2\}$ should 388
be maximized for minimizing the errors in the spatial bits, 389
which are dominated by the distance between the pairs of adja- 390
cent symbols having different power levels $d_s = \sqrt{P_1} - \sqrt{P_2}$. 391
We therefore define the spatial function $f_S(\alpha)$ that accounts for 392
the dependence of the spatial errors on α as 393

$$f_S(\alpha) \triangleq \sqrt{P_1} - \sqrt{P_2} = \frac{1 - \sqrt{\alpha}}{\sqrt{(N_r - N_a)\alpha + N_a}}. \quad (31)$$

As regards to the classic modulated symbol errors, it is 394
known that the PSK error probability is given as [41] 395

$$\mathcal{P}(s_{m_i}^k \rightarrow s_{n_i}^k) = \mathcal{P}\left(\|r_i - s_{m_i}^k\|^2 > \|r_i - s_{n_i}^l\|^2\right) \\ = Q\left(f \sqrt{\frac{P_2}{N_0} \log_2(M) \sin \frac{\pi}{M}}\right). \quad (32)$$

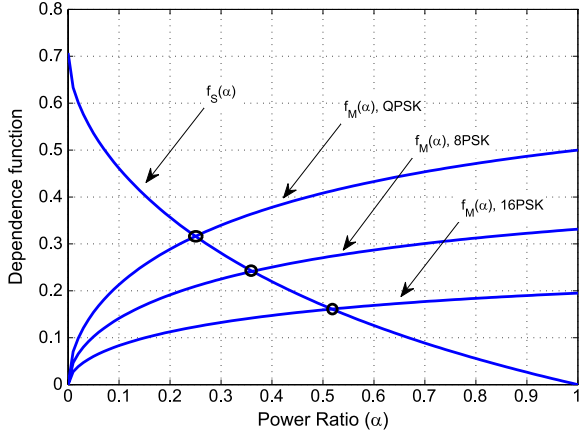


Fig. 4. Theoretical optimization of α for DLT for a (8×4) MIMO with $N_a = 2$, using (36).

Accordingly, we define the function $f_M(\alpha)$ for the dependence of the modulated symbol error on α as

$$\begin{aligned} f_M(\alpha) &\triangleq \sqrt{P_2 \log_2(M) \sin \frac{\pi}{M}} \\ &= \sqrt{\log_2(M) \sin \frac{\pi}{M} \cdot \frac{\alpha}{(N_r - N_a)\alpha + N_a}}. \end{aligned} \quad (33)$$

The optimization (26) is equivalent to the maximization of the minimum of these functions:

$$\alpha_{\text{opt}} = \arg \max_{\alpha} \{ \min \{ f_S(\alpha), f_M(\alpha) \} \}. \quad (34)$$

The optimum power scaling ratio is, therefore, given as

$$\alpha_{\text{opt}} = \arg \max_{\alpha} \left\{ \frac{1 - \sqrt{\alpha}}{\sqrt{(N_r - N_a)\alpha + N_a}}, \sqrt{\log_2(M) \sin \frac{\pi}{M} \cdot \frac{\alpha}{(N_r - N_a)\alpha + N_a}} \right\} \quad (35)$$

which is equivalent to selecting the factor α so that the two terms in the minimization become equal, which gives

$$\alpha_{\text{opt}} = \frac{1}{(1 + \sqrt{\log_2(M) \sin \frac{\pi}{M}})^2}. \quad (36)$$

We examine this optimization in Fig. 4, which shows the functions $f_S(\alpha)$, $f_M(\alpha)$ when increasing the values of α for the example of a (8×4) -element DLT system with $N_a = 2$, for $M = 4, 8, 16$, i.e., quadrature phase-shift keying (QPSK), 8PSK, and 16PSK modulation. The intersections of the lines determine the optimum values of α . It will be shown in the following that the theoretically obtained optimal values of α closely match the optimal values obtained by simulation.

V. COMPLEXITY AND POWER EFFICIENCY

A. Complexity

Here, we compare the computational complexity of SMX, RSM, and DLT and use this to carry out a comparison of the resulting PE of the techniques. First, Table II summarizes the

TABLE II
COMPLEXITY FOR SMX, RSM, AND THE PROPOSED DLT SCHEME.
 $N_X = N_a$ FOR RSM, $N_X = N_r$ FOR DLT

	Operations
<i>Transmitter:</i>	
ZF processing	$N_r^3 + 2N_t N_r$
<i>Receiver:</i>	
Spatial detection	$2N_a \binom{N_r}{N_a}$
Demodulation	$N_X M$
SMX Total	$C_{SMX} = N_r^3 + N_r(2N_t + M)$
RSM Total	$C_{RSM} = N_r^3 + 2N_t N_r + N_a \left(2 \binom{N_r}{N_a} + M \right)$
DLT Total	$C_{DLT} = N_r^3 + N_r(2N_t + M) + 2N_a \binom{N_r}{N_a}$

computational complexity of each of the techniques, taking into account the dominant operations at the transmitter and receiver. We follow the typical assumption that multiplications and additions require an equal number of floating point operations. For all three schemes, the ZF-TPC employed at the transmitter involves the inversion of the channel matrix that requires $N_r^3 + N_t N_r$ operations and the multiplication with the supersymbol vector involving an additional $N_t N_r$ operations. At the receiver, all techniques require a demodulation stage that involves M comparisons for and M -order modulation, for each antenna receiving information, i.e., $N_r M$ for both SMX and DLT, and $N_a M$ for RSM. The RSM and DLT require an additional stage for the detection of the spatial symbol which, from (6) involves N_a complex multiplications and N_a complex additions for each antenna combination out of the $\binom{N_r}{N_a}$ combinations in total.

B. Power Efficiency

As the ultimate metric for evaluating the performance-complexity tradeoff and the overall usefulness of the proposed technique, we consider the PE of DLT compared with SMX and RSM. Following the modeling of [43]–[46], we define the PE of the communication link as the bit rate per total transmit power dissipated, i.e., the ratio of the goodput achieved over the power consumed:

$$\mathcal{E} = \frac{T}{P_{\text{PA}} + N_t \cdot P_t^{\text{RF}} + N_r \cdot P_r^{\text{RF}} + p_c \cdot C} \quad (37)$$

where $P_{\text{PA}} = ((\xi/\eta) - 1)P$ in Watts is the power dissipated by the power amplifier to produce the total transmit signal power P , with η being the power amplifier's efficiency and ξ being the modulation-dependent peak-to-average power ratio (PAPR). Furthermore, $P_t^{\text{RF}} = P_{\text{mix}} + P_{\text{filt}} + P_{\text{DAC}}$ and $P_r^{\text{RF}} = P_{\text{mix}} + P_{\text{filt}} + P_{\text{ADC}}$ represent the RF powers related to the mixers, to the transmit filters, to the digital-to-analog converter (DAC) at the transmitter and to the analog-to-digital converter (ADC) at the receiver, which are assumed to be constant for the purposes of this paper. We use practical values of these from [44] as $\eta = 0.35$ and $P_{\text{mix}} = 30.3$ mW, $P_{\text{filt}} = 2.5$ mW, $P_{\text{DAC}} = 1.6$ mW, and $P_{\text{ADC}} = 1.3$ mW, yielding $P_t^{\text{RF}} = 34.4$ mW, and $P_r^{\text{RF}} = 34.1$ mW. In (37), p_c in Watts/KOps is the power per 10^3 elementary

453 operations (KOps) of the digital signal processor, and C is the
 454 number of operations involved, taken from Table II, where
 455 it is assumed that the operations shown dominate the digital
 456 signal processing complexity of the link. This term is used
 457 for introducing the complexity as a factor related to the power
 458 dissipation in the PE metric. Typical values of p_c include $p_c =$
 459 22.88 mW/KOps for the Virtex-4 and $p_c = 5.76$ mW/KOps for
 460 the Virtex-5 FPGA family from Xilinx [47]. Finally

$$T = \beta B(1 - P_B) = \beta B(1 - P_e)^B \quad (38)$$

461 represents the achieved goodput, where P_B is the block error
 462 rate with a block of size B symbols, and β is the BE of SM
 463 in bits per symbol, taken from Table I. For reference, we have
 464 assumed an LTE Type-2 TDD frame structure [48]. This has
 465 a 10 ms duration that consists of 10 subframes, out of which
 466 five subframes, containing 14 symbol time slots each, are used
 467 for DL transmission yielding a block size of $B = 70$ for the
 468 DL, whereas the remainder are used for both uplink (UL) and
 469 control information transmission. A slow fading channel is
 470 assumed where the channel remains constant for the duration
 471 of the frame.

472 The expression in (37) provides an amalgamated metric that
 473 combines goodput, complexity, and transmit signal power, all
 474 in a unified metric. High values of \mathcal{E} indicate that high bit
 475 rates are achievable for a given power consumption and thus
 476 denote high energy efficiency. The following results show that
 477 DLT provides an increased energy efficiency compared with
 478 SMX and RSM in numerous scenarios using different transmit
 479 power levels P .

480

VI. NUMERICAL RESULTS

481 To evaluate the benefits of the proposed technique, this
 482 section presents numerical results based on Monte Carlo sim-
 483 ulations of SMX, RSM, and the proposed DLT. The channel
 484 impulse response is assumed perfectly known at the transmitter.
 485 Without loss of generality, unless stated otherwise, we assume
 486 that the transmit power is restricted to $P = 1$. MIMO systems
 487 with up to eight TAs employing QPSK and 8PSK modulation
 488 are explored, albeit it is plausible that the benefits of the
 489 proposed technique extend to larger scale systems and higher
 490 order modulation.

491 *Remark:* It should be noted that the BE improvement shown
 492 in the following could also be obtained by SMX with the aid
 493 of an increased classical modulation order. Accordingly, in the
 494 following, we compare the proposed DLT to: (a) SMX using the
 495 same classical modulation order to illustrate the improved BE
 496 of DLT; and (b) SMX relying on a higher modulation order to
 497 highlight the improved performance of DLT for an identical BE.
 498 In Fig. 5, we show the BER as a function of the power
 499 ratio for DLT for the (8×4) MIMO system, where the values
 500 of α in the area of 0.25 can be seen to provide the best
 501 performance. This matches well with the theoretically derived
 502 result of Section IV-A and Fig. 4. Similarly, Fig. 6 shows the
 503 BER versus α performance for higher order modulation 8PSK
 504 and 16PSK. Again, a close match can be seen with the theo-
 505 retically derived values for α_{opt} . In Fig. 7, we show the BER
 506 with increasing SNR for the proposed DLT, where the black

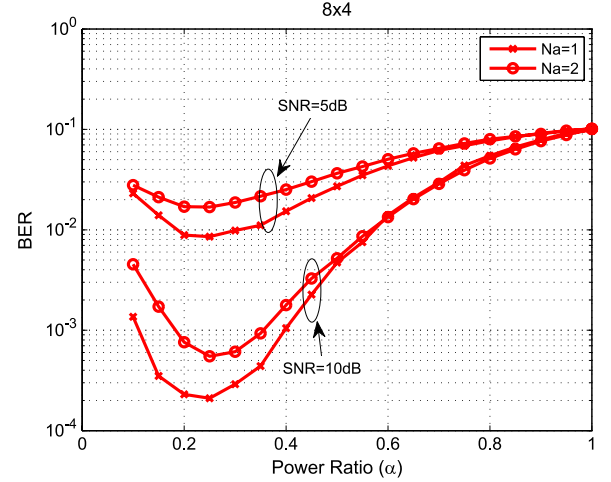


Fig. 5. BER versus α for an (8×4) MIMO with SMX and DLT, as well as QPSK with Rayleigh fading.

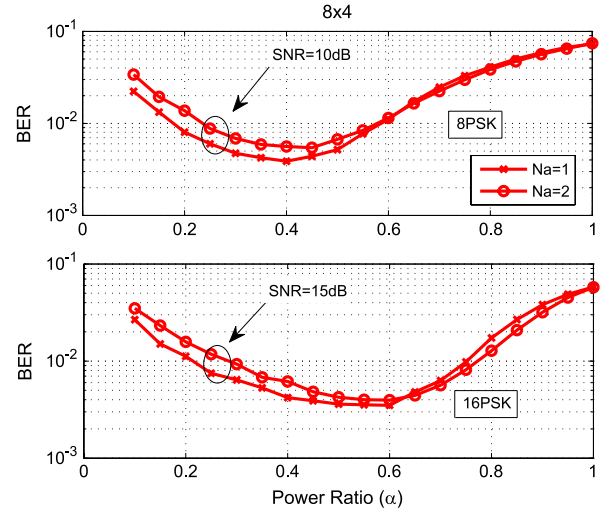


Fig. 6. BER versus α for a (8×4) MIMO with DLT, as well as 8PSK and 16PSK with Rayleigh fading.

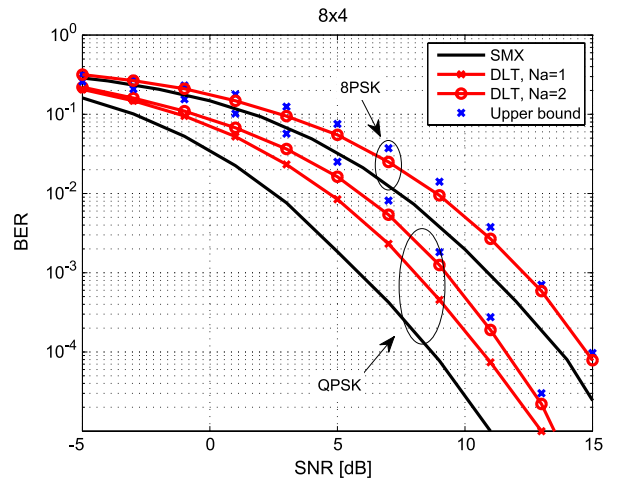


Fig. 7. BER versus SNR for a (8×4) MIMO with SMX and DLT, as well as QPSK and 8PSK with Rayleigh fading.

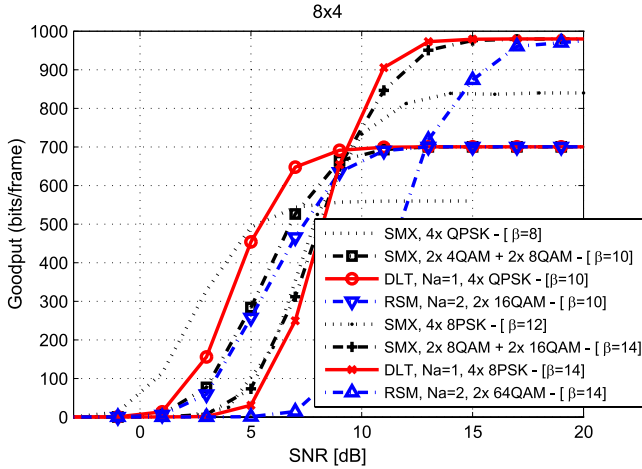


Fig. 8. Goodput versus SNR for a (8×4) MIMO with SMX and DLT, as well as Rayleigh fading.

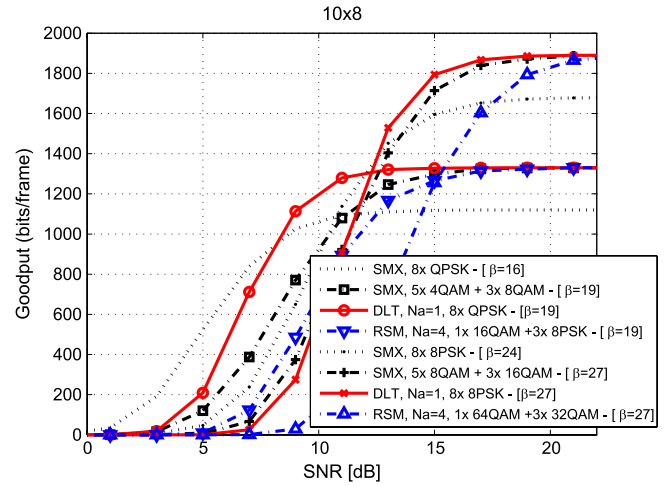


Fig. 10. Goodput versus SNR for a (10×8) MIMO with SMX and DLT, as well as Rayleigh fading.

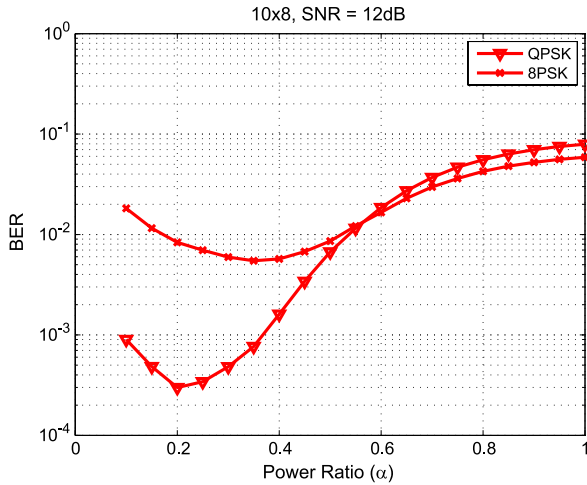


Fig. 9. BER versus α for a (10×8) MIMO with DLT, QPSK, and 8PSK with Rayleigh fading.

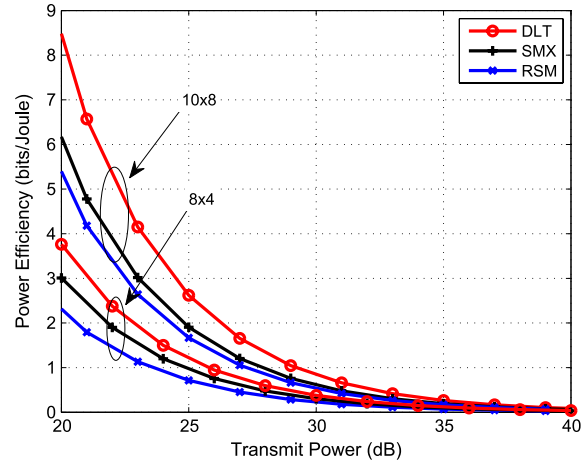


Fig. 11. PE versus transmit power for (10×8) and (8×4) MIMO systems with SMX and DLT, as well as QPSK with Rayleigh fading.

507 lines for $N_a = 4$ represent SMX transmission. The curves show
 508 results for both QPSK and 8PSK. The theoretical upper bound
 509 using (19) is also depicted for both cases, and it can be observed
 510 that it offers a tight bound. Clearly, the DLT scheme has inferior
 511 BER performance compared with SMX due to the additional
 512 spatial streams but at the benefit of improved BE. The improved
 513 BE of DLT is demonstrated in Fig. 8 where the goodput
 514 with increasing SNR is depicted for the same (8×4) MIMO
 515 scenario. Clearly, DLT provides higher goodput than SMX for
 516 sufficiently high SNR values. To complete our comparisons, for
 517 both scenarios in the figure, we also show the cases where the
 518 symbol modulation order used for SMX and RSM is increased
 519 for some of the spatial streams in order to achieve the same
 520 BE values of $\beta = 10$ and $\beta = 14$ with the proposed DLT, for
 521 QPSK and 8PSK, respectively. Clearly, this has an impact on
 522 the SNR requirement of SMX, where it can be seen that the
 523 proposed DLT scheme obtains the maximum goodput at lower
 524 SNR values.

525 The performance comparison is extended to the (10×8)
 526 MIMO system in Figs. 9 and 10. In Fig. 9, we show the

BER as a function of the power ratio for DLT, where the best
 527 performance is provided for α in the range of 0.2 for QPSK and
 528 0.4 for 8PSK. Fig. 10 shows the goodput with increasing SNR,
 529 where again it can be observed that the DLT provides better
 530 goodput than SMX at higher SNR values. As above, for both
 531 scenarios characterized in the figure, we also include the cases
 532 where the symbol modulation order used for SMX and RSM is
 533 increased for some of the spatial streams in order to achieve the
 534 same BE values of $\beta = 19$ and $\beta = 27$ with the proposed DLT,
 535 for QPSK and 8PSK, respectively. Again, it can be seen that the
 536 proposed DLT scheme obtains the maximum goodput at lower
 537 SNR values.

Finally, Figs. 11 and 12 show the PE of the SMX, RSM
 539 and DLT techniques. Fig. 11 shows the PE for increasing
 540 transmit power, within the region of power values used in
 541 the communication standards for (10×8) and (8×4) MIMO
 542 systems. It is assumed here that the noise variance is $\sigma^2 = 1$ to
 543 indirectly account for the path loss (and, hence, the useful signal
 544 power loss) experienced in real transmission. It can be seen that
 545 the proposed DLT scheme outperforms SMX and RSM in terms of

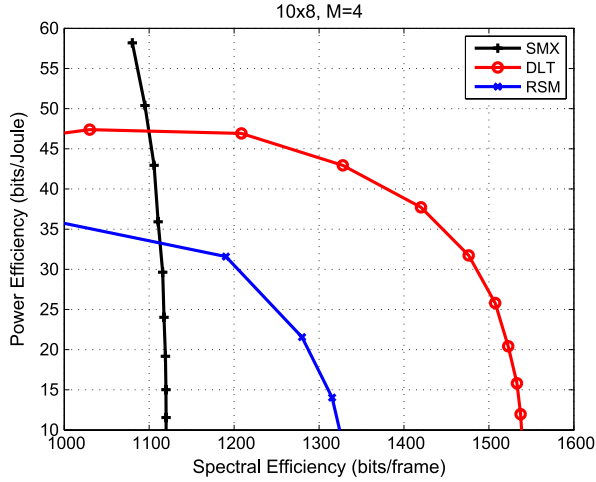


Fig. 12. Power efficiency versus spectral efficiency for a (10×8) MIMO with SMX and DLT, as well as QPSK with Rayleigh fading.

of PE for all transmit power values in both (10×8) and (8×4) MIMO systems. The tradeoff between PE and BE is shown in Fig. 12. It can be seen that DLT offers a more scalable tradeoff with a wider range of BEs for the PE range, while it is more power efficient than SMX and RSM in the region of high BEs.

VII. CONCLUSION

A dual-layered DL transmission scheme was proposed, which combines traditional MIMO SMX with RSM. As opposed to traditional SM where a subset of antennas carry a spatial stream, here, we allow all antennas to carry information by applying SM on the symbol power-level domain. This provides scope for the analytical optimization of the ratio between the power levels used in the proposed scheme. Both our simulations and performance analysis show that, by allowing all antennas to form spatial streams, the proposed scheme improves the system's BE and power efficiency compared to both SMX and SM.

Further work can involve exploring more advanced TPC schemes for the proposed transmission scheme and exploring the adaptations of the proposed scheme for QAM and enhancing its robustness to channel state information errors.

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AUTHOR PLEASE ANSWER ALL QUERIES

AQ1 = Please provide publication update in Ref. [18].

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Dual-Layered MIMO Transmission for Increased Bandwidth Efficiency

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Abstract—A dual-layered downlink transmission scheme is proposed for intrinsically amalgamating multiple-input-multiple-output (MIMO) spatial multiplexing (SMX) with spatial modulation (SM). The proposed scheme employs a classic SMX transmission that is known to offer superior bandwidth efficiency (BE) compared with SM. We exploit receive-antenna-based SM (RSM) on top of this transmission as an enhancement of the BE. The RSM here is applied to the combined spatial and power-level domain not by activating and deactivating the RAs but rather by choosing between two power levels $\{P_1, P_2\}$ for the received symbols in these antennas. In other words, the combination of symbols received at a power level P_1 carries information in the spatial domain in the same manner as the combination of nonzero elements in the receive symbol vector carries information in the RSM transmission. This allows for the coexistence of RSM with SMX, and the results show increased BE for the proposed scheme compared with both SMX and SM. To characterize the proposed scheme, we carry out a mathematical analysis of its performance, and we use this to optimize the ratio between P_1 and P_2 for attaining the minimum error rates. Our analytical and simulation results demonstrate significant BE gains for the proposed scheme compared with conventional SMX and SM.

Index Terms—Multiple-input-multiple-output systems, spatial modulation (SM), spatial multiplexing (SMX), transmit precoding (TPC).

I. INTRODUCTION

MULTIANTENNA-aided transceivers have been shown to improve the capacity of the wireless channel by means of spatial multiplexing (SMX) [1]. For the multiuser downlink (DL), transmit precoding (TPC) schemes have been shown to improve both the attainable power efficiency (PE) and the cost of mobile terminals by shifting the signal processing complexity to the base stations (BSs). Numerous TPC solutions

exist, ranging from highly complex capacity achieving nonlinear dirty paper coding techniques [2] and their low-complexity suboptimal counterparts in the form of Tomlinson–Harashima precoding [3]–[6] to linear TPC schemes based on channel inversion [7]–[12] that offers the lowest complexity, albeit at an inferior performance. The performance–complexity tradeoffs between the above TPC have been thoroughly studied in the literature. More recently, it has been shown that the family of linear techniques exhibits a close-to-optimal performance in the large-scale multiple-input-multiple-output (MIMO) region [13]–[15]. Accordingly, we focus on the class of low-complexity closed-form linear TPC [7]–[12] due to their favorable performance–complexity tradeoff and practical relevance.

More recently, spatial modulation (SM) has been conceived for implicitly encoding information in the index of the specific antenna activated for the transmission of the modulated symbols, offering a low-complexity design alternative [16]. Its central benefits include the absence of interantenna interference (IAI) and the fact that it only requires a subset (down to one) of radio-frequency (RF) chains compared with SMX. Accordingly, the interantenna synchronization is also relaxed. Early work has focused on the design of receiver algorithms for minimizing the bit error ratio (BER) of SM at low complexity [16]–[21]. The work spans from matched filtering as a low-complexity technique for detecting the antenna index used for SM [16] to the maximum likelihood (ML) [20] with a significantly reduced complexity compared with classic SMX ML detectors, including compressive sensing approaches [18] and performance analyses [19]. Reduced-space sphere detection has also been proposed for SM in [21] for further complexity reduction where a generalized SM transmission was also explored [22]. In addition to receive processing, recent work has also proposed constellation shaping for SM [23]–[33]. Specifically, the work on this topic has focused on three main directions: shaping and optimization of the spatial constellation, i.e., the legitimate sets of activated transmit antennas (TAs) [23], modulation constellation shaping [24]–[28] for the SM and space shift keying transmission, where the constellation of the modulated bits is optimized, and joint spatial and modulation constellation shaping, in the form of optimizing the received constellation [29]–[33].

Closely related work has focused on applying the concept of SM to the receive antennas (RAs) of the communication link, as opposed to the TAs as per the above approaches, forming the RA-based spatial modulation (RSM) concept [36]–[39]. By means of TPC, this technique targets a specific subset of RAs, which receive information symbols, whereas the rest of the RAs

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85 receive only noise. This may be achieved by using zero-forcing
86 (ZF) TPC and transmitting a combination of information sym-
87 bols and zeros to the RAs, depending on the spatial symbols
88 to convey. As opposed to conventional SM where a subset of
89 RF chains is deployed, here, all TAs and RAs are active and
90 therefore there are no RF chain reductions. Still, the computa-
91 tional complexity of the receivers is drastically reduced, where
92 simply the indexes of the targeted RAs have to be detected,
93 and the classic symbols received at the activated RAs are then
94 demodulated.

95 Inspired by the above RSM philosophy, here, we propose
96 a dual-layered transmission (DLT) scheme, which intrinsically
97 amalgamates a full spatial multiplexing (SMX) with SM. First,
98 we note that since, for RSM, all TAs and RAs are active, there
99 are no RF chain reductions, and this motivates the full SMX
100 approach. To accommodate the SMX, we apply an SM to the
101 combined spatial and receive-power domain, where instead of
102 sending a combination of information symbols and zero power
103 to the RAs, we apply two different power levels for distinguish-
104 ing between the “active” and “inactive” RAs. In this manner, the
105 spatial symbols are formed based on the power levels detected.
106 We demonstrate that this improves the bandwidth efficiency
107 (BE) with respect to SMX and SM. Against this state of the
108 art, we list the main contributions of this paper.

- 109 • We propose a new DLT scheme based on linear TPC that
110 improves the BE by jointly exploiting the benefits of SMX
111 and RSM.
- 112 • We provide the performance analysis of the proposed
113 technique based on the pairwise error probability (PEP)
114 between different constellation points in the supersymbol
115 constellation formed by the combination of the spatial
116 constellation of RSM and the classic modulation constel-
117 lation of SMX.
- 118 • We use the above results for analytically deriving the
119 optimum power ratio between the two sets of antennas
120 that carry the spatial symbol for the proposed scheme for
121 minimizing the probability of detection errors.
- 122 • We calculate and compare analytically the complexity of
123 the conventional and proposed techniques, and quantify
124 the performance–complexity tradeoff of conventional and
125 proposed schemes, by introducing a PE metric that com-
126 bines the BE, transmit power, and complexity, to prove
127 the enhanced tradeoff for the proposed scheme.

129 *Remark 1:* It should be noted that, while this paper focuses
130 on a single-link scenario, the proposed technique can be readily
131 extended to a multiuser DL scenario, where the DLT and the
132 related RSM take place on a per-user basis, as facilitated by the
133 ZF-TPC employed at the BS.

134 *Remark 2:* The proposed scheme does not consist of a power
135 allocation scheme in the sense of allocating power according
136 to the quality-of-service (QoS) requirements of the user. This
137 power allocation may be applied in addition to the proposed
138 scheme in the multiuser scenario, where different users with
139 different QoS requirements employ different sets of power
140 levels $\{P_1, P_2\}$ accordingly.

141 *Remark 3:* To facilitate the proposed power-level modula-
142 tion, this paper focuses on phase shift keying (PSK) in terms

of the classical symbol modulation. Its adaptation to quadrature
143 amplitude modulation (QAM) is not trivial since the variability
144 of the power levels for the classically modulated symbols
145 would hinder the detection of the power levels of the spatially
146 modulated symbols. Nevertheless, even for PSK modulation,
147 our results illustrate a wide range of achievable BEs for the
148 proposed scheme and an improved performance compared with
149 classical SMX associated with both PSK and QAM for the
150 same BE.

The remainder of this paper is organized as follows. Section II
152 presents the MIMO system model and introduces the RSM
153 transmission philosophy. Section III details the proposed DLT
154 scheme, whereas in Section IV, we present our analytical study
155 of the performance attained and the analytical optimization
156 of the power ratio for the proposed scheme. Section V detail
157 the complexity calculation and the study of the attainable PE.
158 Finally, Section VI presents our numerical results, whereas our
159 conclusions are offered in Section VII.

II. SYSTEM MODEL AND RECEIVE-ANTENNA-BASED SPATIAL MODULATION

A. System Model

Consider a MIMO system, where the transmitter and receiver
164 are equipped with N_t and N_r antennas, respectively. For sim-
165 plicity, unless stated otherwise, in this paper, we assume that the
166 transmit power budget is limited as $P = 1$. For the case of
167 the closed-form TPCs of [7]–[12], it is required that $N_t \geq N_r$.
168 The given channel is modeled as follows:

$$\mathbf{y} = \mathbf{H}\mathbf{t} + \mathbf{w} \quad (1)$$

where \mathbf{y} is the vector of received symbols in all RAs, and \mathbf{H} is
170 the MIMO channel vector with elements $h_{m,n}$ representing the
171 complex channel coefficient between the n th TA and the m th
172 RA. Furthermore, \mathbf{t} is the vector of precoded transmit symbols
173 that will be discussed in the following, and $\mathbf{w} \sim \mathcal{CN}(0, \sigma^2 \mathbf{I})$
174 is the additive white Gaussian noise (AWGN) component at
175 the receiver, with $\mathcal{CN}(\mu, \sigma^2)$ denoting the circularly symmet-
176 ric complex Gaussian distribution with a mean of μ and a
177 variance of σ^2 .

B. Receive-Antenna-Based Spatial Modulation

The block diagram of RSM as proposed in [36] is shown
180 in Fig. 1(a). RSM targets a subset of the RAs by sending
181 information symbols to these RAs and zero power to the rest
182 of the RAs. While for RSM all RAs have to be on to detect
183 the arrival of information symbols, for coherence with the
184 SM literature, we shall refer to the antennas as “active” and
185 “inactive,” depending on whether they do or do not receive
186 information symbols, respectively. The specific combination of
187 RAs that do receive symbols implicitly conveys the symbol
188 transmitted in the spatial domain. The above RA subset trans-
189 mission is achieved by forming a supersymbol vector in the
190 form $\mathbf{s}_m^k = \mathbf{e}_k b_m = [0, \dots, b_{m_1}, \dots, 0, \dots, b_{m_2}, \dots, 0]^T$ with
191 N_a nonzero elements, where \mathbf{e}_k is a diagonal matrix of size 192

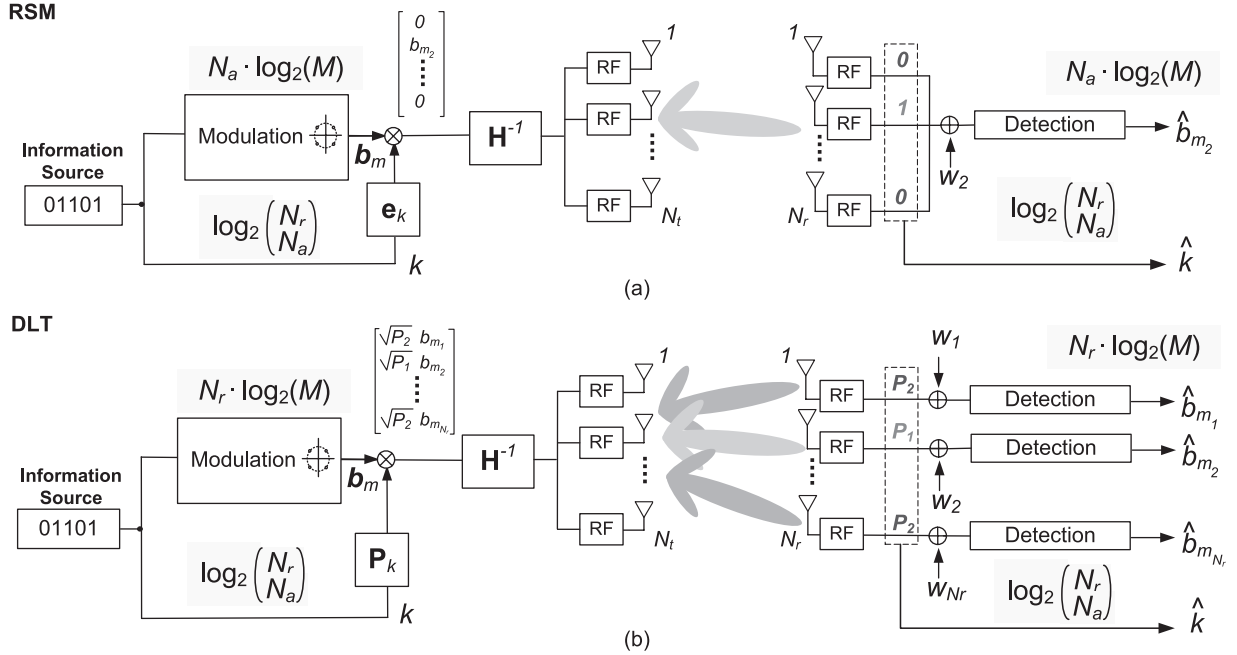


Fig. 1. Block diagram of (a) RSM and (b) DLT transmission.

193 N_r with elements taken from the set $\{1, 0\}$ on its diagonal, 194 which represents the RAs that are activated. The notation $[\cdot]^T$ 195 denotes the transpose operator. Here, $b_{m_i}, m_i \in \{1, \dots, M\}$ 196 is a symbol taken from an M -order modulation alphabet that 197 represents the transmitted waveform in the baseband domain 198 conveying $\log_2(M)$ bits and k represents the index of the 199 N_a activated RAs (the index of the nonzero elements in \mathbf{s}_m^k) 200 conveying $\log_2(N_r)$ bits in the spatial domain. Accordingly, 201 the total number of bits conveyed per supersymbol for RSM is

$$\beta = N_a \log_2(M) + \log_2 \left(\frac{N_r}{N_a} \right). \quad (2)$$

202 The transmitter then sends

$$\mathbf{t} = f \mathbf{T} \mathbf{s}_m^k \quad (3)$$

203 where $\mathbf{T} = \mathbf{H}^H (\mathbf{H} \mathbf{H}^H)^{-1}$ is the ZF-TPC [7] that preserves 204 the form of \mathbf{s}_m^k at the receiver. The factor $f = \sqrt{1/\text{tr}(\mathbf{T} \mathbf{T}^H)}$, 205 where $\text{tr}(\cdot)$ denotes the trace operator and normalizes the 206 average transmit power to $P = 1$. The received symbol vector 207 can be written as

$$\mathbf{y} = f \mathbf{H} \mathbf{T} \mathbf{s}_m^k + \mathbf{w} = f \mathbf{s}_m^k + \mathbf{w} \quad (4)$$

208 where, clearly, all IAI is removed. At the receiver, a joint ML 209 detection of both the RA index and the transmit symbol is 210 obtained by the following minimization:

$$\begin{aligned} [\hat{s}_m, \hat{k}] &= \arg \min_i \|\mathbf{y} - \hat{\mathbf{y}}_i\| \\ &= \arg \min_{m_i, k_i} \|\mathbf{y} - f \mathbf{H} \mathbf{T} \mathbf{s}_{m_i}^{k_i}\| \end{aligned} \quad (5)$$

211 where $\|\mathbf{x}\|$ denotes the norm of vector \mathbf{x} , and $\hat{\mathbf{y}}_i$ is the i th 212 constellation point in the received SM constellation. A low-

complexity decoupled approach is also proposed in [36], where 213 the first active antenna indexes are detected in the form of 214

$$\hat{k} = \arg \max_{j \in \mathcal{J}} \sum_{i=1}^{N_a} |y_{j,i}|^2 \quad (6)$$

where \mathcal{J} denotes the set of symbols in the spatial domain, and 215 then, the classic modulated symbols are detected by 216

$$\hat{b}_{m_i} = \arg \min_{n_i \in \mathcal{Q}} |y_{\hat{k},i}/f - b_{n_i}|^2 \quad (7)$$

where \mathcal{Q} denotes the modulation constellation, and b_{n_i} are 217 the symbols in the modulated symbol alphabet. For reasons of 218 computational complexity, we shall focus on the latter detector 219 in this paper. 220

III. PROPOSED DUAL-LAYERED TRANSMISSION 221

From the above system description, it can be seen that for 222 the particular case of RSM, while the detection complexity 223 is clearly reduced with respect to SMX, there are no savings 224 in RF complexity since all N_r RAs have to be activated and 225 receiving for the detection in (6) and (7). Still, by forming a 226 subset of beams towards the receiver, as shown in Fig. 1(a), 227 the BE, i.e., the number of bits per channel use, is generally 228 lower for RSM than for SMX. Motivated by this, we propose 229 a dual-layered approach combining SMX with RSM, where 230 the BE of conventional SMX MIMO transmission is strictly 231 enhanced by encoding spatial bits in the RSM fashion in the 232 received power domain, by selecting two distinct, nonzero 233 power levels for the transmitted supersymbols instead of the 234 “on-off” RSM transmission in the $\{1, 0\}$ manner. This allows 235 for nonzero elements throughout the supersymbol vector \mathbf{s}_m^k , 236

hence supporting a full SMX transmission in the modulated signal domain. The block diagram of the proposed DLT is shown in Fig. 1(b).

1) *Transmitter*: Here, we employ a full data vector in the form of $\mathbf{b}_m = [b_{m_1}, b_{m_2}, \dots, b_{m_{N_r}}]^T$, with all elements being nonzero, and the encoding of the spatial bits is achieved by allocating different power levels to the received symbols according to the spatial symbol k , by applying the power allocation matrix \mathbf{P}_k , i.e.,

$$\mathbf{s}_m^k = \mathbf{P}_k \mathbf{b}_m = [s_{m_1}, s_{m_2}, \dots, s_{m_{N_r}}]^T \quad (8)$$

with

$$\mathbf{P}_k = \begin{bmatrix} \sqrt{p_1} & 0 & \dots & 0 \\ 0 & \sqrt{p_2} & \dots & 0 \\ \vdots & \vdots & \ddots & \vdots \\ 0 & 0 & \dots & \sqrt{p_{N_r}} \end{bmatrix} \quad (9)$$

where $p_i, i \in [1, N_r]$ are taken from the set $\{P_1, P_2\}$ according to the spatial symbol k . Note that classic QoS-based power allocation can be applied in addition to this process by employing an additional power allocation matrix on top of (9). The receiver can then remove this additional matrix by simple inversion, in order to detect the spatial symbol. For notational simplicity and to keep the focus of the discussion on the proposed concept, we neglect QoS-based power allocation.

2) *Receiver*: At the receiver side, the explicit knowledge of the power levels $\{P_1, P_2\}$ is not required, as long as the detector can distinguish between the two power levels. The received signal of (4) can be decomposed as

$$y_p = f\sqrt{P_1}b_{m_p} + w_p, p \in \mathcal{A} \quad (10)$$

$$y_q = f\sqrt{P_2}b_{m_q} + w_q, q \in \mathcal{I} \quad (11)$$

where \mathcal{A} and \mathcal{I} denote the sets of “active” and “inactive” antennas, respectively. Hence, the receive processing is similar to the conceived one for RSM, with the difference that the classic modulated symbols of all RAs have to be detected, as opposed to those of N_a antennas only for RSM. Accordingly, the receiver first detects the set of antennas with the highest received power levels and then detects the classic modulated symbols at all RAs according to

$$\hat{k} = \arg \max_{j \in \mathcal{J}} \sum_{i=1}^{N_a} |y_{j,i}|^2 \quad (12)$$

where \mathcal{J} denotes the set of symbols in the spatial domain, and

$$\hat{\mathbf{b}}_m = \arg \min_{n \in \mathcal{Q}} |\mathbf{y}/f - \mathbf{b}_n|^2 \quad (13)$$

where \mathcal{Q} denotes the classic modulation constellation, and b_n are the symbols in the modulated symbol alphabet.

TABLE I
BE IN BITS PER CHANNEL USE FOR SMX, RSM, AND DLT

	Bandwidth Efficiency (BE)
SMX	$\beta = N_r \log_2(M)$
RSM	$\beta = N_a \log_2(M) + \log_2 \binom{N_r}{N_a}$
DLT	$\beta = N_r \log_2(M) + \log_2 \binom{N_r}{N_a}$

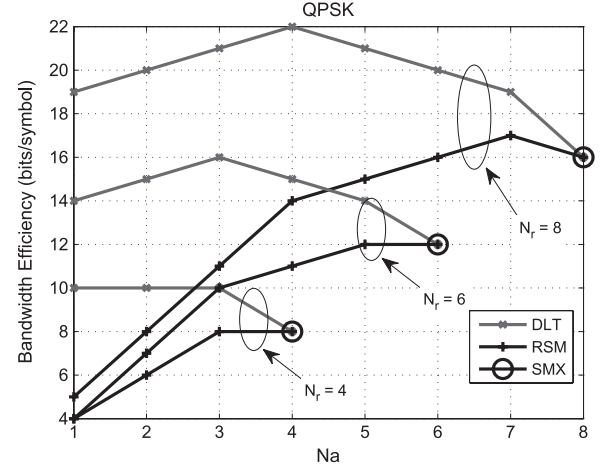


Fig. 2. BE versus N_a for SMX, RSM, and DLT using the expressions of Table I.

A. Bandwidth Efficiency

Clearly, the encoding process in (8) and (9) encodes $N_r \log_2(M)$ bits in the modulated symbol domain and an additional $\log_2 \binom{N_r}{N_a}$ bits in the spatial domain. This results in a total of

$$\beta = N_r \log_2(M) + \log_2 \binom{N_r}{N_a} \quad (14)$$

bits per transmitted supersymbol for DLT, which is strictly greater than that for SMX and RSM. Here, the notation N_a denotes the number of antennas receiving symbols at the power level P_1 . We should emphasize that, although all RAs are active for both RSM and the proposed DLT, for coherence with the literature, we shall adhere to the terms “active” and “inactive” to indicate the antennas receiving $\{1, 0\}$ and $\{P_1, P_2\}$ for RSM and DLT, respectively. A comparison of the BEs of SMX, RSM, and DLT is shown in Table I, where it can be seen that the proposed DLT approach has an improved BE compared with the conventional approaches. This is quantified in Fig. 2, where the BE is expressed in terms of bits per channel use is shown with increasing numbers of “active” antennas N_a for MIMO links with $N_r = 4$, $N_r = 6$, and $N_r = 8$, where the clear benefits of the proposed approach can be seen. It can be observed that the additional BE of DLT compared with SMX can be maximized by appropriately selecting the number of activated antennas according to

$$\tilde{N}_a = \arg \max_{N_a} \log_2 \binom{N_r}{N_a} = N_r/2 \quad (15)$$

which is demonstrated in the figure.

294 B. Symbol Power Levels

295 With regard to the resulting BER performance, the set of
296 spatial power levels $\{P_1, P_2\}$ must be carefully selected so that
297 they satisfy a combination of two constraints.
298

- 299 1) There is sufficient separation between the two power lev-
300 els P_1, P_2 for correct detection of the “active” antennas
301 and hence the spatial symbol k in the presence of noise.
- 302 2) The symbols received with $P_2 < P_1$ that dominate the
303 BER of the modulated symbol detection must experience
304 a sufficiently high signal-to-noise ratio (SNR) that is
305 adequate for reliable demodulation.

306 Let us therefore define the power ratio

$$\alpha = \frac{P_2}{P_1} \quad (16)$$

307 as the ratio between the two power levels transmitted, which
308 is optimized in the following results. Since N_a symbols are
309 transmitted with power P_1 and the remaining $N_r - N_a$ symbols
310 have power of P_2 , given a total power budget of $P = 1$, we have

$$P_1 = \frac{1}{(N_r - N_a)\alpha + N_a} \quad (17)$$

$$P_2 = \frac{\alpha}{(N_r - N_a)\alpha + N_a}. \quad (18)$$

311 Clearly, since the power levels P_1, P_2 influence the reliability
312 of detection for the modulated symbols and since the ratio α
313 determines the detection reliability of the spatial symbols, α
314 can be optimized for best BER performance. In the following,
315 we derive a closed-form expression for the optimum α value
316 for an M -order PSK modulation, where it can be seen that this
317 optimum value is independent of both N_r and of N_a .

318 *Remark:* Regarding the effect of the above on the transmit
319 power distribution, we note that the power imbalance discussed
320 refers to the information symbols s_m^k and does not translate
321 to a power imbalance for the transmit symbols \mathbf{t} . Indeed, the
322 ZF-precoded transmit symbols have the same average transmit
323 power, constrained by the scaling factor f as shown above,
324 which is valid for both the proposed DLT and for the conven-
325 tional SMX, and these transmit symbols exhibit the same power
326 distribution for both techniques. In other words, the proposed
327 scheme does not impact the design of the power amplifiers used
328 at the transmitter.

329 To verify the above, Fig. 3 shows the probability density
330 function (pdf) of the normalized transmit power per antenna
331 for both SMX and DLT in a (8×4) element MIMO system. It
332 can be seen that, as expected, both techniques show the same
333 distribution of transmit power.

334 IV. DUAL-LAYERED TRANSMISSION PERFORMANCE

335 ANALYSIS AND OPTIMUM POWER RATIO α

336 A. Probability of Error

337 Here, we carry out a performance analysis for the proposed
338 DLT scheme by deriving the PEP between the pair of symbols

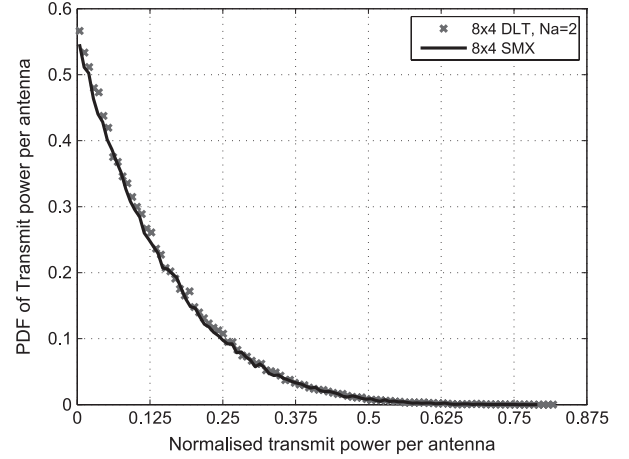


Fig. 3. PDF of transmit power per antenna for a (8×4) MIMO with SMX and DLT and QPSK with Rayleigh fading.

339 s_m^k and s_n^l in the superimposed spatial and classic modulation
340 constellations, following the analysis in [36]. Accordingly, we
341 define the PEP as $\mathcal{P}(s_m^k \rightarrow s_n^l)$ and use the union bound for the
342 average bit error probability P_e , which is expressed as

$$P_e \leq \frac{1}{\beta} E \left\{ \sum_{s_m^k \in \mathcal{B}} \sum_{s_n^l \in \mathcal{B} \setminus s_m^k} d(s_m^k, s_n^l) \mathcal{P}(s_m^k \rightarrow s_n^l) \right\} \quad (19)$$

where $d(s_m^k, s_n^l)$ is the Hamming distance between the bit
343 representations of symbols s_m^k, s_n^l and $\mathcal{B} = \mathcal{J} \cup \mathcal{Q}$ is the super-
344 symbol constellation defined as the union of the spatial domain
345 constellation and the classic modulation constellation. We have
346 used the operator \cup to define the union of sets. For the PEP, we
347 have the following theorem.
348

Theorem 1: The PEP $\mathcal{P}(s_m^k \rightarrow s_n^l)$ for DLT can be expressed as

$$\mathcal{P}(s_m^k \rightarrow s_n^l) = Q \left(\frac{f}{\sqrt{N_0}} \left(1 - \sum_{i=1}^{N_r} \sqrt{p_{k_i} p_{l_i}} \mathcal{R}\{b_{m_i}^* b_{n_i}\} \right) \right) \quad (20)$$

where $Q(\cdot)$ denotes the Gaussian q -function [42], $\mathcal{R}\{\cdot\}$ denotes
350 the real part of a number, $(\cdot)^*$ denotes the complex conjugate
351 operation, and $N_0 = 2\sigma^2$ is the noise power spectral density.
352

Proof: Let us first define $\mathbf{r} = \mathbf{y}/f$ and $\mathbf{v} = \mathbf{w}/f$ for
353 use in the following expressions. The PEP of the supersymbol
354 constellation can be expressed as
355

$$\begin{aligned} \mathcal{P}(s_m^k \rightarrow s_n^l) &= \mathcal{P}(\|\mathbf{r} - s_m^k\|^2 > \|\mathbf{r} - s_n^l\|^2) \\ &= \mathcal{P} \left(\sum_{i=1}^{N_r} p_{k_i} |b_{m_i}|^2 - 2\mathcal{R}\{r_i^* \sqrt{p_{k_i}} b_{m_i}\} \right. \\ &\quad \left. > \sum_{i=1}^{N_r} p_{l_i} |b_{n_i}|^2 - 2\mathcal{R}\{r_i^* \sqrt{p_{l_i}} b_{n_i}\} \right). \end{aligned} \quad (21)$$

Since, for PSK signals, we have $|b_{m_i}| = 1$, by rearranging
356 the terms in the probability expression, (21) can be further
357

358 simplified as

$$\mathcal{P}(s_m^k \rightarrow s_n^l) = \mathcal{P}\left(\sum_{i=1}^{N_r} \mathcal{R}\{r_i^* \sqrt{p_{l_i}} b_{n_i}\} - \mathcal{R}\{r_i^* \sqrt{p_{k_i}} b_{m_i}\} \right. \\ \left. > \frac{\sum_{i=1}^{N_r} p_{l_i} - \sum_{i=1}^{N_r} p_{k_i}}{2}\right). \quad (22)$$

359 Since $\sum_{i=1}^{N_r} p_{l_i} = \sum_{i=1}^{N_r} p_{k_i} = 1$ and $r_i = \sqrt{p_{k_i}} b_{m_i} + v_i$, we
360 have

$$\mathcal{P}(s_m^k \rightarrow s_n^l) = \mathcal{P}\left(\sum_{i=1}^{N_r} \mathcal{R}\{\sqrt{p_{k_i}} b_{m_i}^* \sqrt{p_{l_i}} b_{n_i}\} + \mathcal{R}\{v_i^* \sqrt{p_{l_i}} b_{n_i}\} \right. \\ \left. > \sum_{i=1}^{N_r} p_{k_i} |b_{m_i}|^2 + \mathcal{R}\{v_i^* \sqrt{p_{k_i}} b_{m_i}\}\right) \\ = \mathcal{P}\left(\sum_{i=1}^{N_r} \mathcal{R}\{v_i^* (\sqrt{p_{l_i}} b_{n_i} - \sqrt{p_{k_i}} b_{m_i})\} \right. \\ \left. > 1 - \sum_{i=1}^{N_r} \sqrt{p_{k_i} p_{l_i}} \mathcal{R}\{b_{m_i}^* b_{n_i}\}\right). \quad (23)$$

361 Let us define the random variable $\chi \triangleq \sum_{i=1}^{N_r} \mathcal{R}\{v_i^* (\sqrt{p_{l_i}} b_{n_i} -$
362 $\sqrt{p_{k_i}} b_{m_i})\}$ for which we have $\chi \in \mathcal{N}(0, AN_0/f^2)$ with

$$A = \frac{\sum_{i=1}^{N_r} p_{l_i} |b_{n_i}|^2 + p_{k_i} |b_{n_i}|^2}{2} = \frac{1}{2} \sum_{i=1}^{N_r} p_{l_i} + p_{k_i}. \quad (24)$$

363 For the unity transmit power assumed in this paper, it can be
364 seen from (24) that $A = 1$. Accordingly, for the PEP, we have

$$\mathcal{P}(s_m^k \rightarrow s_n^l) = \mathcal{P}\left(\chi > 1 - \sum_{i=1}^{N_r} \sqrt{p_{k_i} p_{l_i}} \mathcal{R}\{b_{m_i}^* b_{n_i}\}\right) \quad (25)$$

365 which, for $\chi \in \mathcal{N}(0, N_0/f^2)$, leads to (20). ■

366 B. Optimum Power Ratio α

367 As mentioned earlier, the power ratio α determines the
368 reliability of detection for the spatial symbol, whereas the lower
369 power level P_2 dominates the BER performance of the classic
370 modulated symbols' detection. As the probability of error in
371 (19) is dominated by the maximum PEP, the optimum power
372 ratio should be selected as

$$\alpha_{\text{opt}} = \arg \min_{\alpha} \max_{s_m^k, s_n^l} \{\mathcal{P}(s_m^k \rightarrow s_n^l)\}. \quad (26)$$

373 To simplify the analysis, we shall treat the errors in the spatial
374 and classic modulated symbols separately. Accordingly, for the
375 maximum PEP $\mathcal{P}_m(s_m^k \rightarrow s_{m_i}^l)$ in the spatial domain only, we
376 have the following theorem.

Theorem 2: The maximum PEP $\mathcal{P}_m(s_m^k \rightarrow s_{m_i}^l)$ for the 377
spatial symbols in DLT can be expressed as 378

$$\mathcal{P}_m(s_m^k \rightarrow s_{m_i}^l) = Q\left(\frac{f}{\sqrt{N_0}} \cdot \frac{\sqrt{P_2} - \sqrt{P_1}}{2}\right). \quad (27)$$

Proof: The maximum PEP in the spatial domain involves 379
the adjacent symbols of different power levels in the supersym- 380
bol constellation and can be expressed as 381

$$\mathcal{P}_m(s_m^k \rightarrow s_{m_i}^l) \\ = \mathcal{P}\left(\|r_i - s_{m_i}^k\|^2 > \|r_i - s_{m_i}^l\|^2\right) \\ = \mathcal{P}\left(P_1 - 2\mathcal{R}\{r_i^* \sqrt{P_1} b_{m_i}\} > P_2 - 2\mathcal{R}\{r_i^* \sqrt{P_2} b_{m_i}\}\right) \quad (28)$$

where, using $r_i = \sqrt{p_{k_i}} b_{m_i} + v_i$, we get 382

$$\mathcal{P}_m(s_m^k \rightarrow s_{m_i}^l) \\ = \mathcal{P}\left(P_1 - 2P_1 |b_{m_i}|^2 - 2\mathcal{R}\{u_i^* \sqrt{P_1} b_{m_i}\} \right. \\ \left. > P_2 - 2\sqrt{P_1 P_2} |b_{m_i}|^2 - 2\mathcal{R}\{u_i^* \sqrt{P_2} b_{m_i}\}\right) \\ = \mathcal{P}\left(2(\sqrt{P_2} - \sqrt{P_1}) \mathcal{R}\{u_i^* b_{m_i}\} > P_1 + P_2 - 2\sqrt{P_1 P_2}\right) \\ = \mathcal{P}\left(-\mathcal{R}\{u_i^* b_{m_i}\} > \frac{\sqrt{P_1} - \sqrt{P_2}}{2}\right). \quad (29)$$

Similarly to the given proof, we have used the fact 383
that $|b_{m_i}|^2 = 1$, and it can be seen that $\psi \triangleq -\mathcal{R}\{u_i^* b_{m_i}\} \in$ 384
 $\mathcal{N}(0, N_0/f^2)$. Accordingly, for the minimum PEP in the spatial 385
constellation, we have 386

$$\mathcal{P}_m(s_m^k \rightarrow s_{m_i}^l) = \mathcal{P}\left(\psi > \frac{\sqrt{P_2} - \sqrt{P_1}}{2}\right) \quad (30)$$

which leads to (27). ■ 387

This indicates that the separation between $\{P_1, P_2\}$ should 388
be maximized for minimizing the errors in the spatial bits, 389
which are dominated by the distance between the pairs of adja- 390
cent symbols having different power levels $d_s = \sqrt{P_1} - \sqrt{P_2}$. 391
We therefore define the spatial function $f_S(\alpha)$ that accounts for 392
the dependence of the spatial errors on α as 393

$$f_S(\alpha) \triangleq \sqrt{P_1} - \sqrt{P_2} = \frac{1 - \sqrt{\alpha}}{\sqrt{(N_r - N_a)\alpha + N_a}}. \quad (31)$$

As regards to the classic modulated symbol errors, it is 394
known that the PSK error probability is given as [41] 395

$$\mathcal{P}(s_{m_i}^k \rightarrow s_{n_i}^k) = \mathcal{P}\left(\|r_i - s_{m_i}^k\|^2 > \|r_i - s_{n_i}^l\|^2\right) \\ = Q\left(f \sqrt{\frac{P_2}{N_0}} \log_2(M) \sin \frac{\pi}{M}\right). \quad (32)$$

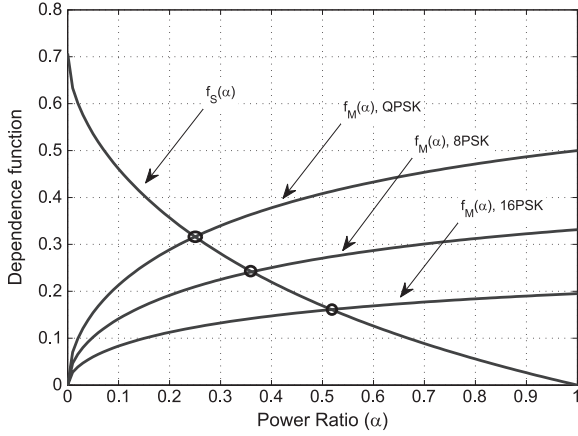


Fig. 4. Theoretical optimization of α for DLT for a (8×4) MIMO with $N_a = 2$, using (36).

Accordingly, we define the function $f_M(\alpha)$ for the dependence of the modulated symbol error on α as

$$\begin{aligned} f_M(\alpha) &\triangleq \sqrt{P_2 \log_2(M) \sin \frac{\pi}{M}} \\ &= \sqrt{\log_2(M) \sin \frac{\pi}{M} \cdot \frac{\alpha}{(N_r - N_a)\alpha + N_a}}. \end{aligned} \quad (33)$$

The optimization (26) is equivalent to the maximization of the minimum of these functions:

$$\alpha_{\text{opt}} = \arg \max_{\alpha} \{ \min \{ f_S(\alpha), f_M(\alpha) \} \}. \quad (34)$$

The optimum power scaling ratio is, therefore, given as

$$\alpha_{\text{opt}} = \arg \max_{\alpha} \left\{ \frac{1 - \sqrt{\alpha}}{\sqrt{(N_r - N_a)\alpha + N_a}}, \sqrt{\log_2(M) \sin \frac{\pi}{M} \cdot \frac{\alpha}{(N_r - N_a)\alpha + N_a}} \right\} \quad (35)$$

which is equivalent to selecting the factor α so that the two terms in the minimization become equal, which gives

$$\alpha_{\text{opt}} = \frac{1}{(1 + \sqrt{\log_2(M) \sin \frac{\pi}{M}})^2}. \quad (36)$$

We examine this optimization in Fig. 4, which shows the functions $f_S(\alpha)$, $f_M(\alpha)$ when increasing the values of α for the example of a (8×4) -element DLT system with $N_a = 2$, for $M = 4, 8, 16$, i.e., quadrature phase-shift keying (QPSK), 8PSK, and 16PSK modulation. The intersections of the lines determine the optimum values of α . It will be shown in the following that the theoretically obtained optimal values of α closely match the optimal values obtained by simulation.

V. COMPLEXITY AND POWER EFFICIENCY

A. Complexity

Here, we compare the computational complexity of SMX, RSM, and DLT and use this to carry out a comparison of the resulting PE of the techniques. First, Table II summarizes the

TABLE II
COMPLEXITY FOR SMX, RSM, AND THE PROPOSED DLT SCHEME.
 $N_X = N_a$ FOR RSM, $N_X = N_r$ FOR DLT

	Operations
<i>Transmitter:</i>	
ZF processing	$N_r^3 + 2N_t N_r$
<i>Receiver:</i>	
Spatial detection	$2N_a \binom{N_r}{N_a}$
Demodulation	$N_X M$
SMX Total	$C_{SMX} = N_r^3 + N_r(2N_t + M)$
RSM Total	$C_{RSM} = N_r^3 + 2N_t N_r + N_a \left(2 \binom{N_r}{N_a} + M \right)$
DLT Total	$C_{DLT} = N_r^3 + N_r(2N_t + M) + 2N_a \binom{N_r}{N_a}$

computational complexity of each of the techniques, taking into account the dominant operations at the transmitter and receiver. We follow the typical assumption that multiplications and additions require an equal number of floating point operations. For all three schemes, the ZF-TPC employed at the transmitter involves the inversion of the channel matrix that requires $N_r^3 + N_t N_r$ operations and the multiplication with the supersymbol vector involving an additional $N_t N_r$ operations. At the receiver, all techniques require a demodulation stage that involves M comparisons for and M -order modulation, for each antenna receiving information, i.e., $N_r M$ for both SMX and DLT, and $N_a M$ for RSM. The RSM and DLT require an additional stage for the detection of the spatial symbol which, from (6) involves N_a complex multiplications and N_a complex additions for each antenna combination out of the $\binom{N_r}{N_a}$ combinations in total.

B. Power Efficiency

As the ultimate metric for evaluating the performance-complexity tradeoff and the overall usefulness of the proposed technique, we consider the PE of DLT compared with SMX and RSM. Following the modeling of [43]–[46], we define the PE of the communication link as the bit rate per total transmit power dissipated, i.e., the ratio of the goodput achieved over the power consumed:

$$\mathcal{E} = \frac{T}{P_{\text{PA}} + N_t \cdot P_t^{\text{RF}} + N_r \cdot P_r^{\text{RF}} + p_c \cdot C} \quad (37)$$

where $P_{\text{PA}} = ((\xi/\eta) - 1)P$ in Watts is the power dissipated by the power amplifier to produce the total transmit signal power P , with η being the power amplifier's efficiency and ξ being the modulation-dependent peak-to-average power ratio (PAPR). Furthermore, $P_t^{\text{RF}} = P_{\text{mix}} + P_{\text{filt}} + P_{\text{DAC}}$ and $P_r^{\text{RF}} = P_{\text{mix}} + P_{\text{filt}} + P_{\text{ADC}}$ represent the RF powers related to the mixers, to the transmit filters, to the digital-to-analog converter (DAC) at the transmitter and to the analog-to-digital converter (ADC) at the receiver, which are assumed to be constant for the purposes of this paper. We use practical values of these from [44] as $\eta = 0.35$ and $P_{\text{mix}} = 30.3$ mW, $P_{\text{filt}} = 2.5$ mW, $P_{\text{DAC}} = 1.6$ mW, and $P_{\text{ADC}} = 1.3$ mW, yielding $P_t^{\text{RF}} = 34.4$ mW, and $P_r^{\text{RF}} = 34.1$ mW. In (37), p_c in Watts/KOps is the power per 10^3 elementary 452

453 operations (KOps) of the digital signal processor, and C is the
 454 number of operations involved, taken from Table II, where
 455 it is assumed that the operations shown dominate the digital
 456 signal processing complexity of the link. This term is used
 457 for introducing the complexity as a factor related to the power
 458 dissipation in the PE metric. Typical values of p_c include $p_c =$
 459 22.88 mW/KOps for the Virtex-4 and $p_c = 5.76$ mW/KOps for
 460 the Virtex-5 FPGA family from Xilinx [47]. Finally

$$T = \beta B(1 - P_B) = \beta B(1 - P_e)^B \quad (38)$$

461 represents the achieved goodput, where P_B is the block error
 462 rate with a block of size B symbols, and β is the BE of SM
 463 in bits per symbol, taken from Table I. For reference, we have
 464 assumed an LTE Type-2 TDD frame structure [48]. This has
 465 a 10 ms duration that consists of 10 subframes, out of which
 466 five subframes, containing 14 symbol time slots each, are used
 467 for DL transmission yielding a block size of $B = 70$ for the
 468 DL, whereas the remainder are used for both uplink (UL) and
 469 control information transmission. A slow fading channel is
 470 assumed where the channel remains constant for the duration
 471 of the frame.

472 The expression in (37) provides an amalgamated metric that
 473 combines goodput, complexity, and transmit signal power, all
 474 in a unified metric. High values of \mathcal{E} indicate that high bit
 475 rates are achievable for a given power consumption and thus
 476 denote high energy efficiency. The following results show that
 477 DLT provides an increased energy efficiency compared with
 478 SMX and RSM in numerous scenarios using different transmit
 479 power levels P .

480

VI. NUMERICAL RESULTS

481 To evaluate the benefits of the proposed technique, this
 482 section presents numerical results based on Monte Carlo sim-
 483 ulations of SMX, RSM, and the proposed DLT. The channel
 484 impulse response is assumed perfectly known at the transmitter.
 485 Without loss of generality, unless stated otherwise, we assume
 486 that the transmit power is restricted to $P = 1$. MIMO systems
 487 with up to eight TAs employing QPSK and 8PSK modulation
 488 are explored, albeit it is plausible that the benefits of the
 489 proposed technique extend to larger scale systems and higher
 490 order modulation.

491 *Remark:* It should be noted that the BE improvement shown
 492 in the following could also be obtained by SMX with the aid
 493 of an increased classical modulation order. Accordingly, in the
 494 following, we compare the proposed DLT to: (a) SMX using the
 495 same classical modulation order to illustrate the improved BE
 496 of DLT; and (b) SMX relying on a higher modulation order to
 497 highlight the improved performance of DLT for an identical BE.

498 In Fig. 5, we show the BER as a function of the power
 499 ratio for DLT for the (8×4) MIMO system, where the values
 500 of α in the area of 0.25 can be seen to provide the best
 501 performance. This matches well with the theoretically derived
 502 result of Section IV-A and Fig. 4. Similarly, Fig. 6 shows the
 503 BER versus α performance for higher order modulation 8PSK
 504 and 16PSK. Again, a close match can be seen with the theo-
 505 retically derived values for α_{opt} . In Fig. 7, we show the BER
 506 with increasing SNR for the proposed DLT, where the black

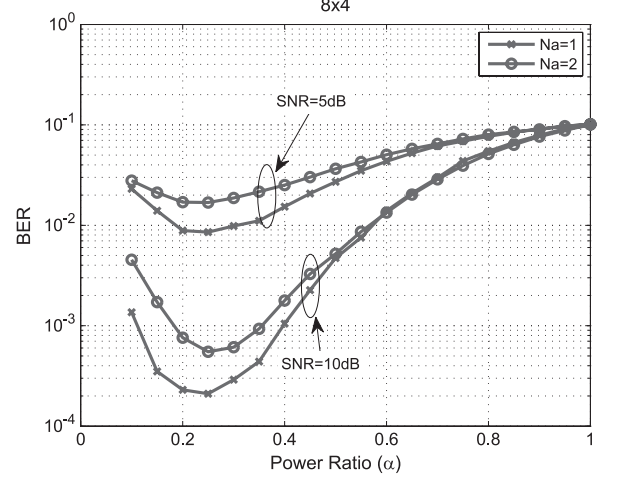


Fig. 5. BER versus α for an (8×4) MIMO with SMX and DLT, as well as QPSK with Rayleigh fading.

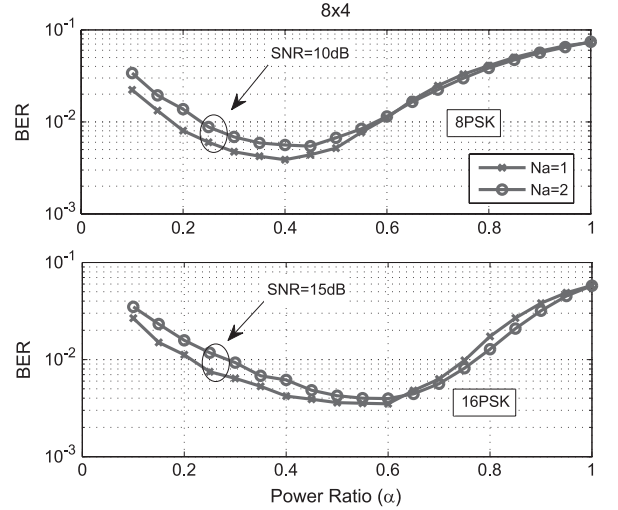


Fig. 6. BER versus α for a (8×4) MIMO with DLT, as well as 8PSK and 16PSK with Rayleigh fading.

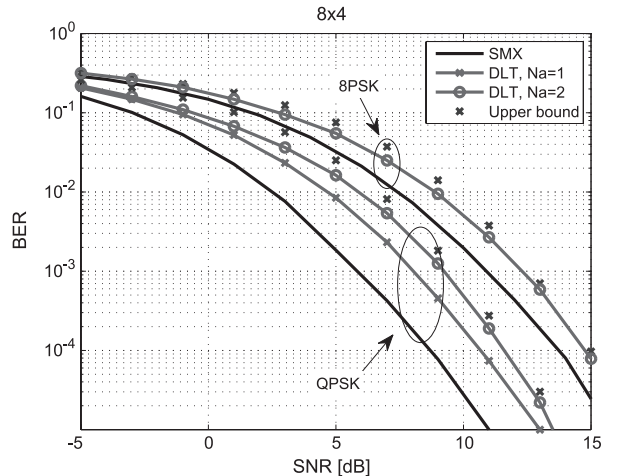


Fig. 7. BER versus SNR for a (8×4) MIMO with SMX and DLT, as well as QPSK and 8PSK with Rayleigh fading.

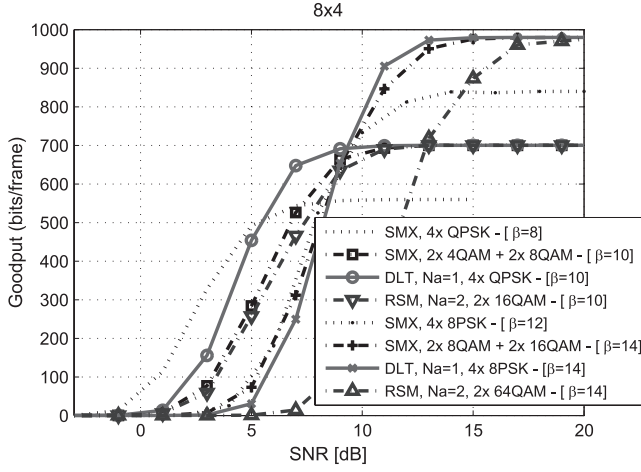


Fig. 8. Goodput versus SNR for a (8×4) MIMO with SMX and DLT, as well as Rayleigh fading.

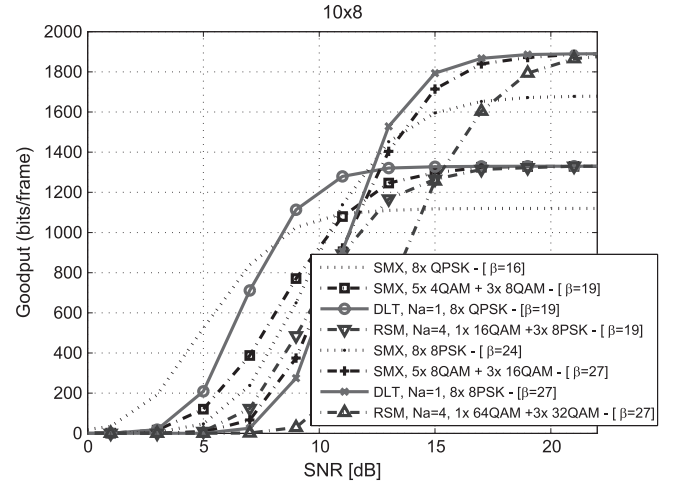


Fig. 10. Goodput versus SNR for a (10×8) MIMO with SMX and DLT, as well as Rayleigh fading.

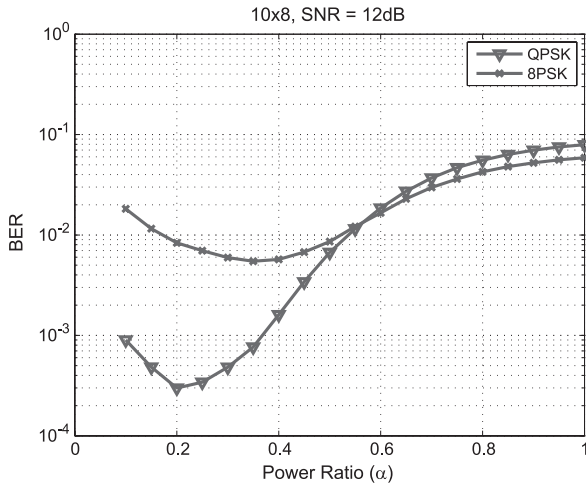


Fig. 9. BER versus α for a (10×8) MIMO with DLT, QPSK, and 8PSK with Rayleigh fading.

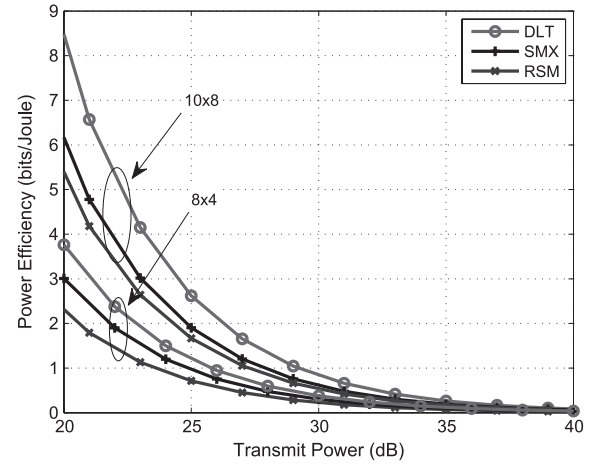


Fig. 11. PE versus transmit power for (10×8) and (8×4) MIMO systems with SMX and DLT, as well as QPSK with Rayleigh fading.

507 lines for $N_a = 4$ represent SMX transmission. The curves show
 508 results for both QPSK and 8PSK. The theoretical upper bound
 509 using (19) is also depicted for both cases, and it can be observed
 510 that it offers a tight bound. Clearly, the DLT scheme has inferior
 511 BER performance compared with SMX due to the additional
 512 spatial streams but at the benefit of improved BE. The improved
 513 BE of DLT is demonstrated in Fig. 8 where the goodput
 514 with increasing SNR is depicted for the same (8×4) MIMO
 515 scenario. Clearly, DLT provides higher goodput than SMX for
 516 sufficiently high SNR values. To complete our comparisons, for
 517 both scenarios in the figure, we also show the cases where the
 518 symbol modulation order used for SMX and RSM is increased
 519 for some of the spatial streams in order to achieve the same
 520 BE values of $\beta = 10$ and $\beta = 14$ with the proposed DLT, for
 521 QPSK and 8PSK, respectively. Clearly, this has an impact on
 522 the SNR requirement of SMX, where it can be seen that the
 523 proposed DLT scheme obtains the maximum goodput at lower
 524 SNR values.

525 The performance comparison is extended to the (10×8)
 526 MIMO system in Figs. 9 and 10. In Fig. 9, we show the

BER as a function of the power ratio for DLT, where the best
 527 performance is provided for α in the range of 0.2 for QPSK and
 528 0.4 for 8PSK. Fig. 10 shows the goodput with increasing SNR,
 529 where again it can be observed that the DLT provides better
 530 goodput than SMX at higher SNR values. As above, for both
 531 scenarios characterized in the figure, we also include the cases
 532 where the symbol modulation order used for SMX and RSM is
 533 increased for some of the spatial streams in order to achieve the
 534 same BE values of $\beta = 19$ and $\beta = 27$ with the proposed DLT,
 535 for QPSK and 8PSK, respectively. Again, it can be seen that the
 536 proposed DLT scheme obtains the maximum goodput at lower
 537 SNR values.

538 Finally, Figs. 11 and 12 show the PE of the SMX, RSM
 539 and DLT techniques. Fig. 11 shows the PE for increasing
 540 transmit power, within the region of power values used in
 541 the communication standards for (10×8) and (8×4) MIMO
 542 systems. It is assumed here that the noise variance is $\sigma^2 = 1$ to
 543 indirectly account for the path loss (and, hence, the useful signal
 544 power loss) experienced in real transmission. It can be seen that
 545 the proposed DLT scheme outperforms SMX and RSM in terms

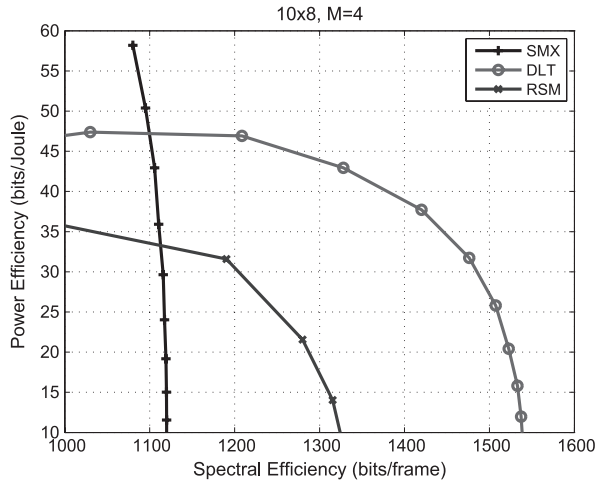


Fig. 12. Power efficiency versus spectral efficiency for a (10×8) MIMO with SMX and DLT, as well as QPSK with Rayleigh fading.

of PE for all transmit power values in both (10×8) and (8×4) MIMO systems. The tradeoff between PE and BE is shown in Fig. 12. It can be seen that DLT offers a more scalable tradeoff with a wider range of BEs for the PE range, while it is more power efficient than SMX and RSM in the region of high BEs.

VII. CONCLUSION

A dual-layered DL transmission scheme was proposed, which combines traditional MIMO SMX with RSM. As opposed to traditional SM where a subset of antennas carry a spatial stream, here, we allow all antennas to carry information by applying SM on the symbol power-level domain. This provides scope for the analytical optimization of the ratio between the power levels used in the proposed scheme. Both our simulations and performance analysis show that, by allowing all antennas to form spatial streams, the proposed scheme improves the system's BE and power efficiency compared to both SMX and SM.

Further work can involve exploring more advanced TPC schemes for the proposed transmission scheme and exploring the adaptations of the proposed scheme for QAM and enhancing its robustness to channel state information errors.

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