

Phase and Amplitude Regeneration through Sequential PSA and FWM Saturation in HNLF

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Abstract *All-optical phase and amplitude regeneration of a QPSK signal using only two nonlinear stages is achieved by combining a PSA with a saturated pump-degenerate FWM based amplitude squeezer. EVM, phase noise and magnitude noise are all reduced by 50%.*

Introduction

Although phase regeneration alone may extend the reach of telecommunications signals, particularly phase shift keying (PSK) formats, it cannot be recursively applied to a signal ad infinitum; eventually the uncorrected amplitude noise will limit the signal to noise ratio of the transmission. Indeed, given that many phase sensitive amplifier (PSA) based phase regenerators result in an increase in amplitude noise, relatively few consecutive phase squeezing stages may be applied before they are no longer beneficial. Ultimately, to correct for non-deterministic noise, both the signal's phase **and** amplitude must be regenerated.

The few publications reporting PSA-based phase regeneration with simultaneous amplitude regeneration either make use of four wave mixing (FWM) saturation¹, or operate the PSA within a nonlinear amplifying loop mirror (NALM)². Despite successfully regenerating both phase and amplitude (and sometimes also offering multi-level functionality²), these schemes are often complicated in their optimisation and are limited in their regenerative ability either due to intrinsic noise processes, or as a result of a compromise between the underlying regenerative operations.

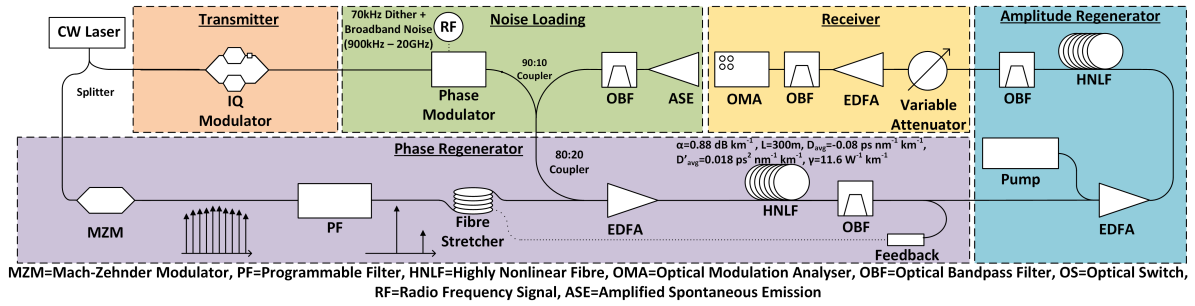
Instead of combining the two regenerative processes in one nonlinear stage, they may be applied sequentially in two independent processes³, allowing for easier optimisation but possibly requiring many stages of nonlinearity. In the investigation presented here, we combine two recent demonstrations of ours, the first, a compact, highly tunable scheme for phase regeneration of a quaternary PSK (QPSK) signal⁴ and the second, a saturated pump-degenerate FWM based amplitude squeezer, which makes use of a high pump to signal power ratio to reduce amplitude noise to phase noise conversion⁵. This enables the duties of phase and amplitude regeneration to be separated, greatly simplifying optimisation,

all the while making use of only two nonlinear stages. As the phase regenerator is conjugating, self phase modulation (SPM) accrued by the signal in the phase regenerator is undone as it propagates through the amplitude regenerator. We analyse the regenerator in terms of its effect on the signal's noise statistics, its constellation plots as well as providing BER measurements, for various combinations of broadband phase noise and amplified spontaneous emission (ASE).

Concept

The scheme consists of two simple nonlinear processing stages. The first is a wavelength converting, idler-free PSA which squeezes the signal phase by simultaneously producing the signal's 3rd phase harmonic using a cascaded signal-degenerate FWM process and coherently adding to it the signal's phase conjugate using a co-propagating dual-pumped FWM process. This scheme is notable not only for achieving phase squeezing using a single nonlinear stage, but also its ease of tunability and flexible operating power, advantages paid for through its wavelength converting nature - the regenerated signal is produced at the location of the signal's 3rd harmonic and is conjugated⁴.

The role of the second nonlinear stage is four-fold: 1) conversion of the signal back to its original wavelength; 2) restoration of the signal to its unconjugated state; 3) regeneration of the signal's amplitude; 4) compensation of the SPM induced by the first nonlinear stage. All of these goals can be readily achieved by employing a pump-degenerate parametric amplifier operated in saturation and selecting the conjugated idler. As shown in⁵, saturation of the signal gain in such a scheme may be achieved for a large range of pump to signal power ratios; the larger the ratio, the smaller the SPM induced in the signal. By controlling this ratio, we may balance the SPM induced by the amplitude regenerator with that in-



duced by the phase regenerator.

Experimental Setup

Figure 1 shows the experimental setup of the regenerator, with the various stages colour-coded for clarity. Firstly, light from a laser operating at 192.5 THz is divided into two paths. One leads to the transmitter stage, where a 10 Gbaud QPSK modulation is applied. The modulated signal then enters the noise loading stage, where a 70 kHz sinusoidal phase dither and broadband phase noise are added using a phase modulator, and in-band ASE is added using an EDFA, a filter and a coupler. Meanwhile, the other path of the laser is used to produce an optical frequency comb with 40 GHz spacing using a Mach-Zehnder modulator. This comb is then passed through a programmable filter, where the undesired frequencies are filtered out, leaving only lines at 192.54 THz (P1) and 192.38 THz (P2) which are to be used as the pumps in the PSA stage.

The signal and pumps are then recombined and amplified to a total power of about 25dBm (spectrum provided in Fig. 2-a) before entering 300 m of low dispersion HNLF to undergo PSA, resulting in the output presented in Fig. 2-b. As described above, the PSA stage is wavelength converting, and so to extract the phase squeezed signal, a filter is placed at 192.42 THz, the location of the signal's third harmonic.

The phase squeezed, conjugated and wavelength converted signal then enters the amplitude squeezing stage. All that is required is for a single CW pump at 192.46 THz to be coupled with the signal and for the pair to be amplified to approximately 35 dBm before being launched into multiple segments of low dispersion HNLF (totalling 2 km in length) connected with optical isolators to increase the Brillouin threshold⁵. The input and output spectra of the HNLF are given in Fig. 2-c and Fig. 2-d, respectively. At the end of the HNLF, a filter is used to extract the output, which is unconjugated relative to the original signal and located at the original wavelength (192.5 THz). The

system was tuned at each stage by analysing the output using an OMA and optimising to minimise phase noise at the very end of the regenerator.

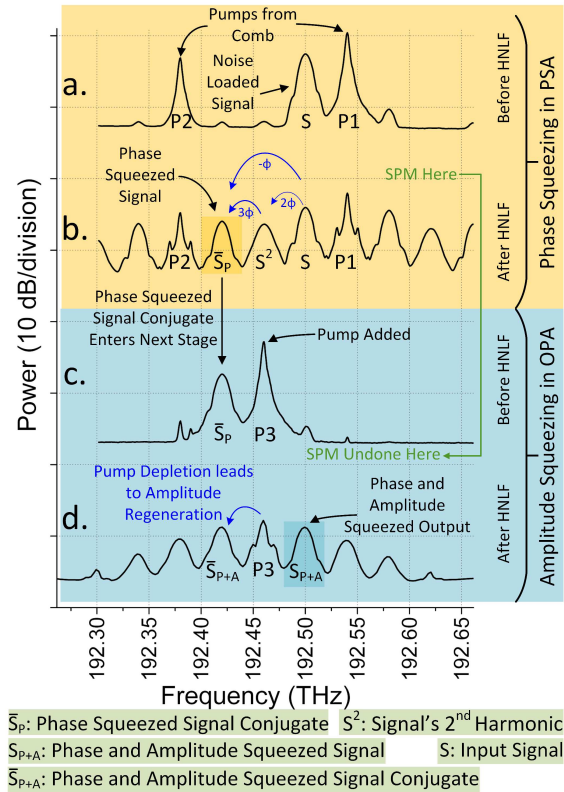


Fig. 2: Spectra: a. Before PSA; b. After PSA; c. Before amplitude regeneration; d. After amplitude regeneration.

Noise Scenario	Metric	Units	Before Regen	Phase Regen	Phase + Amp Regen
No Added Noise	EVM	% rms	7.3	10.4	7.3
	$\Delta\phi$	deg rms	3.0	3.8	3.4
	ΔMag	% rms	5.1	8.0	4.3
Phase Noise Only	EVM	% rms	14.7	11.3	8.2
	$\Delta\phi$	deg rms	7.9	4.1	3.9
	ΔMag	% rms	5.3	8.8	4.5
Phase Noise + ASE	EVM	% rms	21.9	17.7	11.7
	$\Delta\phi$	deg rms	10.2	6.3	5.4
	ΔMag	% rms	13.1	16.0	7.3

Table 1: Table of noise statistics of the signal.

Results

For varying input noise scenarios and at different stages in the scheme, constellation plots and BER curves are provided in Figs. 3 -a and -b, respectively, with noise statistics provided in Table 1. Without additional noise being added to the signal, the constellation plot after phase and am-

plitude regeneration (blue plot Fig. 3-a, top row) is comparable to that before regeneration (yellow plot 3-a) and shows a small decrease in amplitude noise, but a small increase in phase noise, with a marginal power penalty of 0.23dB for a BER of 10^{-4} , as shown in Fig. 3-b (black squares).

The second row of plots in Fig. 3-a shows the case phase noise only was added resulting in a signal phase noise of 8 deg rms. After the phase regenerator (green), the phase noise has been greatly reduced, but at the expense of an increase in amplitude noise, which is typical behaviour for this regenerator^{1,4}. Comparison of the constellation plots after phase regeneration (green) and after both phase and amplitude regeneration (blue), clearly shows the benefit of this additional, amplitude regenerating stage. This is also reflected in the noise statistics in Table 1 and it is interesting to note how the phase noise after amplitude regeneration is smaller than that before; this is the effect of the optical phase conjugation discussed earlier. The BERs for this noise level (blue circles) show an improvement in receiver sensitivity of about 1.1 dB for a BER of 10^{-4} .

The third row in Fig. 3-a is the result of contaminating the phase noise loaded signal with ASE. Once again, the regenerator clearly reduces the noise, and the amplitude regenerator proves its worth in reducing the large amount of amplitude noise present after phase squeezing as well as undoing the SPM accrued in the PSA. For this case (orange triangles, Fig. 3-b), the improvement in receiver sensitivity is 2 dB for a BER of 10^{-4} and we witness an extra 1 deg rms reduction in phase noise through the addition of the amplitude regenerator. The error floor in the BER curves is a consequence of the noise loading that takes place after the transmitter. After the phase and amplitude regenerating scheme, the EVM is roughly halved for this noise level (see Table 1).

Conclusion

Phase and amplitude squeezing was demonstrated using an idler-free PSA followed by a saturated pump-degenerate FWM based wavelength converter. By exploiting phase conjugation in the PSA, SPM accrued in the first nonlinear stage may be undone in the second, reducing output phase noise and permitting higher launch powers to be used. A near halving of EVM, phase noise and magnitude noise is demonstrated using the scheme, and BER measurements demonstrate an improvement in receiver sensitivity of 2 dB for a BER of 10^{-4} in the highest noise case.

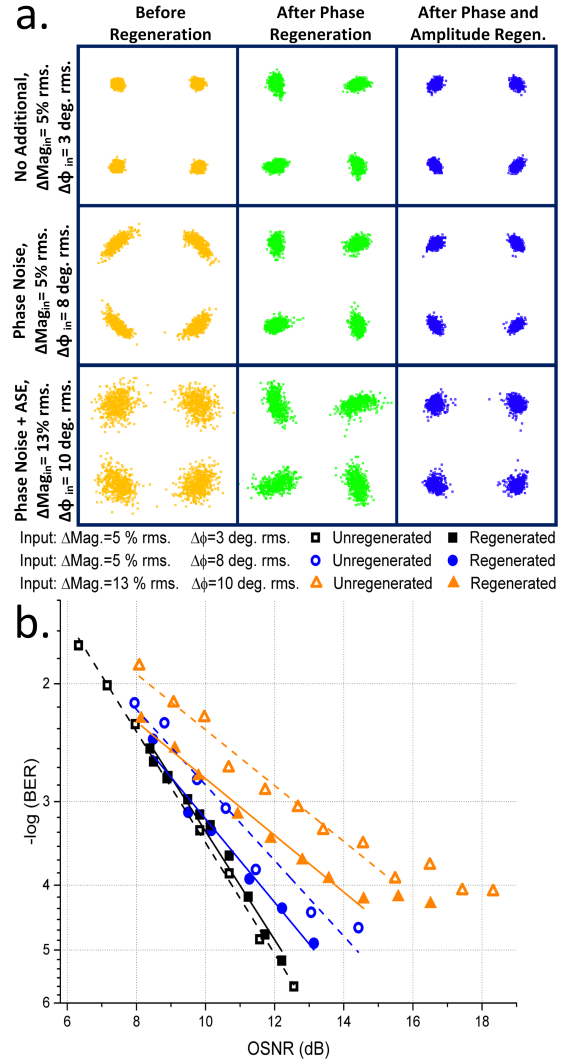


Fig. 3: a. Constellation plots; b. BER curves.

Acknowledgements

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