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# **A Regional Thermohaline Inverse Method for Estimating Circulation and Mixing in the Arctic and subpolar North Atlantic**

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## ABSTRACT

13 A Regional Thermohaline Inverse Method (RTHIM) is presented that esti-  
14 mates velocities through the section bounding an enclosed domain and trans-  
15 formation rates due to interior mixing within the domain, given inputs of sur-  
16 face boundary fluxes of heat and salt and interior distributions of salinity and  
17 temperature. The method works by invoking a volumetric balance in thermo-  
18 haline coordinates between the transformation due to mixing, surface fluxes  
19 and advection, while constraining the mixing to be down tracer gradients. The  
20 method is validated using a 20-year mean of outputs from the NEMO model in  
21 an Arctic and subpolar North Atlantic domain, bound to the south by a section  
22 with a mean latitude of  $66^{\circ}\text{N}$ . RTHIM solutions agree well with the NEMO  
23 model ‘truth’ and are robust to a range of parameters; the MOC, heat and  
24 freshwater transports calculated from an ensemble of RTHIM solutions are  
25 within 12%, 10% and 19%, respectively, of the NEMO values. There is also  
26 bulk agreement between RTHIM solution transformation rates due to mixing  
27 and those diagnosed from NEMO. Localized differences in diagnosed mixing  
28 may be used to guide the development of mixing parameterizations in mod-  
29 els such as NEMO, whose downgradient diffusive closures with prescribed  
30 diffusivity may be considered oversimplified and too restrictive.

## 31 **1. Introduction**

32 The complex spatial structure of the global ocean circulation often obscures its key physical phe-  
33 nomena and drivers, including mechanisms involving both internal mixing and external forcing.  
34 Lagrangian observations have shown that cartoon-like schematics of the thermohaline circulation  
35 may oversimplify the true complexity of the flow pathways (Bower et al. 2009; Lozier 2012), yet  
36 it remains desirable to seek a view that is both simple and physically accurate. Thermohaline co-  
37 ordinates have long been used to characterize different water masses. Recent studies have shown  
38 that expressing circulation and mixing in this non-geographical coordinate system (e.g. Zika et al.  
39 2012; Hieronymus et al. 2014) filters out adiabatic fluctuations and therefore enables insight into  
40 diabatic process which are relevant to the climate system over long timescales.

41 Globally, it has been demonstrated that a thermohaline-coordinate circulation streamfunction and  
42 internal mixing may be diagnosed from observations or model data (Groeskamp et al. 2014a). A  
43 companion study further showed that an inverse method, an extension of Walin (1982), may be  
44 used to infer the circulation and internal mixing from knowledge of the temperature and salin-  
45 ity combined with surface fluxes - the Thermohaline Inverse Method (THIM) (Groeskamp et al.  
46 (2014b); hereafter G14b). THIM elucidates the connectivity of the global transport of heat and  
47 freshwater and their drivers, but the tradeoff is that detailed regional information may be lost  
48 through the transformation from geographical to thermodynamic coordinates, due to the integra-  
49 tion of water masses with the same temperature-salinity properties.

50 Motivated by the need to understand regional circulation and mixing, this study describes a new  
51 Regional Thermohaline Inverse Method (RTHIM) and its validation against output from the Nu-  
52 cleus for European Modelling of the Ocean (NEMO) model (Madec 2008), with a particular ap-  
53 plication to the Arctic and subpolar North Atlantic (Fig. 1). The equivalent transformation in the

54 regional domain once again achieves a simplified view of the complex circulation and mixing, but  
55 the integration of water masses retains information specific to the region of interest, rather than  
56 this information being a smaller fraction of a global integral. The outputs from traditional “box in-  
57 verse” models (Wunsch 1978) have been analyzed in thermohaline coordinates to provide insight  
58 into the circulation in specific regions such as the Weddell Gyre (Naveira Garabato et al. 2016)  
59 and the Arctic Ocean (Tsubouchi et al. 2012), but RTHIM is unique as an inverse method which  
60 directly uses a thermohaline coordinate system applied to a specific region of the ocean, rather than  
61 the global ocean, as in THIM. In THIM, water of particular  $S - \theta$  properties may exist in more  
62 than one region. Due to the averaging process, such regional distinction is lost, but in RTHIM the  
63 diagnostics remain regionally specific. There is a tradeoff between sufficient averaging to obtain  
64 a simpler view and dilution of regional information by excessive averaging. Both approaches are  
65 arguably valid, depending on the particular question or goal. In addition, previous methods that  
66 have solved for interior mixing have done so by imposing a simplified spatial structure on the  
67 diagnosed diffusivities. RTHIM does not impose such a structure, instead applying only simple  
68 constraints on mixing which we describe in section 2b.

69 Climate models suggest that buoyancy changes in the Arctic and subpolar North Atlantic strongly  
70 influence the Atlantic Meridional Overturning Circulation, yet observational evidence is actively  
71 being sought to support the model predictions (Lozier et al. 2017). This paper is a first step to-  
72 wards providing relevant robust observational estimates based on RTHIM, which will be used to  
73 complement more traditional direct observations provided by new trans-basin arrays such as in the  
74 Overturning in the Subpolar North Atlantic Programme (OSNAP; [www.o-snap.org](http://www.o-snap.org)).

75 The paper is organized as follows: in section 2 we describe the principles of the new inverse  
76 method and detail the background to its development. Section 3 explains how we have applied

77 RTHIM to outputs from the NEMO model for validation. In section 4 we present the results of the  
78 validation, and section 5 contains discussion and conclusions.

## 79 **2. The Regional Thermohaline Inverse Method**

### 80 *a. Distributions in thermohaline coordinates*

81 When working in thermohaline coordinates, it is helpful to consider the distribution of water  
82 masses in  $S - \theta$  space. For example, if we are looking at the transport through a section (e.g. the  
83 section indicated by the red line on Fig. 1), the section itself can be divided up using contours  
84 of  $S$  and  $\theta$  (Fig. 2 (a)). The section area distribution in  $S - \theta$  space from a 20 year time-mean  
85 of the NEMO fields (Fig. 2 (b)) is calculated by summing the areas of the section which fall  
86 between contours of  $S$  and  $\theta$ , defined by  $S \in (S \pm \frac{\Delta S}{2})$ ,  $\theta \in (\theta \pm \frac{\Delta \theta}{2})$ , where  $\Delta S = 0.1$  PSU and  
87  $\Delta \theta = 0.2$  °C. Similarly, the volumetric distribution (Fig. 2 (c)) is calculated by summing the  
88 volumes enclosed by contours of  $S$  and  $\theta$  over the whole physical domain. Both distributions are  
89 concentrated in comparatively small regions of  $S - \theta$  space. For the area distribution, 76% of the  
90 total section area of  $2.6 \times 10^9 \text{ m}^2$  is covered by 10% of the occupied  $(S, \theta)$  bins (that is 10% of  
91 the bins which have non-zero associated section area). For the volumetric distribution, 95% of the  
92 total volume of  $1.8 \times 10^{16} \text{ m}^3$  is contained within 10% of the occupied bins.

93 Processes acting on and within the ocean affect the distribution of water masses in  $S - \theta$  space  
94 (Groeskamp et al. 2014a; Pemberton et al. 2015). Surface heat fluxes increase the spread of water  
95 masses along the  $\theta$  axis, while freshwater fluxes increase their spread along the  $S$  axis. Interior  
96 mixing processes on the other hand act to reduce the spread of water masses in  $S - \theta$  space, since  
97 mixing acts down tracer gradients. In addition to the most familiar effects of heating/cooling  
98 and freshening/salinification, ice melting causes water masses below to cool. This is particularly

99 relevant along the Atlantic Water inflow (Fram Strait and around Svalbard) where surface waters  
 100 are relatively warm and sea ice melting on top creates large cold freshwater lenses, which get  
 101 mixed during storms. The competition between boundary and interior processes allows us to  
 102 diagnose interior mixing in the absence of direct observations, by inferring it from other quantities  
 103 which are more easily measured (see e.g. Zika et al. 2015).

#### 104 *b. The volume budget*

105 The aim is to estimate, as outputs from the method, section volume advection and interior dif-  
 106 fusive processes (described later), given inputs of surface boundary fluxes and interior  $S$  and  $\theta$ .  
 107 As in G14b, we begin by considering a volume element bound by pairs of isohaline and isother-  
 108 mal surfaces,  $V = V(S \pm \frac{\Delta S}{2}, \theta \pm \frac{\Delta \theta}{2}, t)$  (Fig. 3). G14b have absolute salinity  $S_A$  and conservative  
 109 temperature  $\Theta$  as their coordinates which is appropriate for application to real ocean observations;  
 110 here we use practical salinity  $S$  and potential temperature  $\theta$  which are conserved in NEMO. The  
 111 conservation equations for volume, salt and heat mirror those in equations 7-9 of G14b for the  
 112 global THIM, except that we express the conservation per unit  $S$  and  $\theta$ , and we add terms involv-  
 113 ing  $I_{adv} = I_{adv}(S, \theta)$ , which we define as the volume advection (inward normal velocity component  
 114 times area of volume element at the bounding section) into the regional volume at its open bound-  
 115 ary per unit  $S$  and  $\theta$ , leading to the following:

$$\frac{\partial}{\partial t}(V) + \nabla_{S\theta} \cdot \mathbf{U}_{S\theta}^{dia} = \frac{1}{\rho_0} f_m + I_{adv}, \quad (1)$$

116 where  $\frac{\partial}{\partial t}(V)$  is the volume tendency per unit  $(S, \theta)$ ,  $\nabla_{S\theta} \cdot \mathbf{U}_{S\theta}^{dia}$  is the diathermohaline volume  
 117 transport divergence per unit  $(S, \theta)$ ,  $\rho_0 = 1024 \text{ kg m}^{-3}$  is a reference density of seawater,  $f_m$  is the

118 surface boundary mass flux per unit  $(S, \theta)$  and  $I_{adv}$  is the section volume advection per unit  $(S, \theta)$ ;

$$\frac{\partial}{\partial t}(VS) + \nabla_{S\theta} \cdot (SU_{S\theta}^{dia}) = \frac{1}{\rho_0} m_S + I_{adv}S, \quad (2)$$

119 where  $\frac{\partial}{\partial t}(VS)$  is the salt tendency per unit  $(S, \theta)$ ,  $\nabla_{S\theta} \cdot (SU_{S\theta}^{dia})$  is the diathermohaline salt transport  
 120 divergence per unit  $(S, \theta)$ ,  $m_S$  is the salt convergence due to interior diffusion per unit  $(S, \theta)$ , and  
 121  $I_{adv}S$  is the section salt advection per unit  $(S, \theta)$ ; and

$$\frac{\partial}{\partial t}(V\theta) + \nabla_{S\theta} \cdot (\theta U_{S\theta}^{dia}) = \frac{1}{\rho_0 c_p^0} (f_h + m_\theta) + I_{adv}\theta, \quad (3)$$

122 where  $\frac{\partial}{\partial t}(V\theta)$  is the heat tendency per unit  $(S, \theta)$ ,  $\nabla_{S\theta} \cdot (\theta U_{S\theta}^{dia})$  is the diathermohaline heat trans-  
 123 port divergence per unit  $(S, \theta)$ ,  $c_p^0$  is the specific heat capacity of seawater ( $4000 \text{ J kg}^{-1} \text{ K}^{-1}$ ),  $f_h$   
 124 is the heat convergence due to boundary fluxes per unit  $(S, \theta)$ ,  $m_\theta$  is the heat convergence due to  
 125 interior diffusion per unit  $(S, \theta)$ , and  $I_{adv}\theta$  is the section heat advection per unit  $(S, \theta)$ . Note that  
 126 the superscript ‘*dia*’ denotes a transport through a surface of constant temperature or salinity.

127 We begin the separation into inputs and outputs by identifying the component terms of the time-  
 128 mean diathermohaline volume transport  $U_{S\theta}^{dia} = (U_{|S}^{dia}, U_{|\theta}^{dia})$ . Here  $U_{|S}^{dia}$  is the transport across an  
 129  $S$  surface between two  $\theta$  surfaces per unit  $\theta$ ; and  $U_{|\theta}^{dia}$  is the transport across a  $\theta$  surface between  
 130 two  $S$  surfaces per unit  $S$ . We repeat the algebraic manipulation used in G14b on the analogous  
 131 equations to (1 – 3), but using a different definition of the thermohaline divergence operator (and  
 132 similar for the gradient operator),  $\nabla_{S\theta} \cdot [\ ] = (\frac{\partial}{\partial S}, \frac{\partial}{\partial \theta}) \cdot [\ ]$ . The discrete  $\frac{\partial}{\partial S}$  operator is defined at the  
 133 central  $S$  value of the grid cell corresponding to  $(S \pm \frac{\Delta S}{2}, \theta \pm \frac{\Delta \theta}{2})$  and analogous for  $\theta$ . Note that  
 134  $\frac{\partial S}{\partial S} = 1$  and  $\frac{\partial \theta}{\partial S} = 0$ , and similar when  $S$  is swapped with  $\theta$ . The rightmost terms involving  $I_{adv}$  in  
 135 equations (1 – 3) above are found to cancel, leading to the following expressions for each of the  
 136 components in thermohaline coordinates (an overbar represents a time-mean):

$$U_{|S}^{dia}(S, \theta) = U_{|S}^{surf} + U_{|S}^{mix} - U_{|S}^{loc}, \quad (4)$$



$$U_{|\theta}^{dia}(S, \theta) = U_{|\theta}^{surf} + U_{|\theta}^{mix} - U_{|\theta}^{loc}, \quad (5)$$

138 where

$$U_{|S}^{surf} = -\frac{1}{\rho_0} \overline{S f_m}, \quad U_{|\theta}^{surf} = \frac{1}{\rho_0 c_p^0} \overline{f_h - c_p^0 \theta f_m} \quad (6)$$

139 are due to surface processes;

$$U_{|S}^{mix} = \frac{1}{\rho_0} \overline{m_S}, \quad U_{|\theta}^{mix} = \frac{1}{\rho_0 c_p^0} \overline{m_\theta} \quad (7)$$

140 are due to interior diffusive processes, defined in more detail later; and

$$U_{|S}^{loc} = \frac{1}{\rho_0} \overline{l_S}, \quad U_{|\theta}^{loc} = \frac{1}{\rho_0 c_p^0} \overline{l_\theta} \quad (8)$$

141 are related to the local response,  $\overline{l_S} = \rho_0 V \frac{\partial S}{\partial t}$  and  $\overline{l_\theta} = \rho_0 c_p^0 V \frac{\partial \theta}{\partial t}$ . The local response expresses the  
 142 rate of change of heat (salt) due to the rate of change of temperature (salinity), for a given volume  
 143 within a discrete  $(S, \theta)$  grid cell. Equivalently, it is the amount of heat (salt) that can be added  
 144 or removed from the system, changing the temperature (salinity) of a water mass by an amount  
 145 whereby it remains within that grid cell.

146 We may now use equations (4) and (5) to rewrite the time-mean of equation (1) in terms of desired  
 147 output estimates (LHS) balanced by specified inputs (RHS):

$$I_{adv} - \nabla_{S\theta} \cdot \mathbf{U}_{S\theta}^{mix} = \frac{\partial V}{\partial t} - \frac{1}{\rho_0} \overline{f_m} + \nabla_{S\theta} \cdot \mathbf{U}_{S\theta}^{surf} - \nabla_{S\theta} \cdot \mathbf{U}_{S\theta}^{loc} \quad (9)$$

148 For the sake of simplicity, we follow the approach of Groeskamp et al. (2017) and neglect the local  
 149 response term, since it is small for the  $(S, \theta)$  grids used in this study. In addition, the mass flux  
 150 term,  $f_m$ , is also negligible for the NEMO solution used here, so that is omitted too.

151 At this point, we again deviate from G14b by including a more general formulation for the interior  
 152 mixing, which no longer depends on the assumption of a constant diffusivity with a fixed geo-  
 153 graphical distribution. We may write the diathermohaline volume transport vector due to interior

diffusive processes,  $U_{S\theta}^{mix}$ , as the divergence of a tensor,  $\mathbf{F}$ , whose properties we may constrain to ensure net downgradient mixing:

$$U_{S\theta}^{mix} = \nabla_{S\theta} \cdot \mathbf{F} = \left( \frac{\partial}{\partial S} F_{SS} + \frac{\partial}{\partial \theta} F_{S\theta}, \frac{\partial}{\partial S} F_{\theta S} + \frac{\partial}{\partial \theta} F_{\theta\theta} \right) \quad (10)$$

where  $\mathbf{F}$  is constrained to be a symmetric diffusive flux tensor in thermohaline coordinates (see the Appendix for an explanation of the symmetric constraint).

Combining this definition of the diffusive flux tensor with equation (9), we may define the inverse problem,

$$I_{adv} - \nabla_{S\theta}^2 \mathbf{F} = \frac{\partial V}{\partial t} + \nabla_{S\theta} \cdot \mathbf{U}_{S\theta}^{surf} + \varepsilon, \quad (11)$$

where  $\varepsilon$  is the error in the inverse solution, which we aim to minimize. Equation 11 is our volume budget, representing the fact that the time-mean change in volume of a volume element results from a balance between advection, surface fluxes and interior mixing.

We solve equation (11) for  $I_{adv}$  and the elements  $F_{C_1 C_2}$  of  $\mathbf{F}$  using constrained optimization (MATLAB's `fmincon`), with constraints  $F_{SS}, F_{\theta\theta} \geq 0$  (net downgradient mixing), and  $F_{S\theta} = F_{\theta S}$  (symmetric diffusive flux tensor). Note that, since equation (11) involves the  $\nabla_{S\theta}^2$  operator applied to  $\mathbf{F}$ , it is possible to conceive of an arbitrary, non-divergent gauge,  $\mathbf{N}$ , to be added to  $\mathbf{F}$ , e.g.  $\mathbf{F}' = \mathbf{F} + \mathbf{N}$ , where  $\nabla_{S\theta}^2 \mathbf{N} = 0$ , and  $\mathbf{F}'$  is the modified  $\mathbf{F}$ , yet to still obtain the same volume balance:  $\nabla_{S\theta}^2 \mathbf{F} = \nabla_{S\theta}^2 \mathbf{F}'$ . Often a Helmholtz decomposition is used to solve similar gauge problems, given appropriate boundary conditions on  $\mathbf{F}$ . However, there is no appropriate physical metric in thermohaline coordinates for such a decomposition (in Cartesian coordinates  $(x, y)$ , one metric could be a measure of distance, proportional to  $(\Delta x^2 + \Delta y^2)^{\frac{1}{2}}$ ). Therefore, we emphasize that the interpretation of the RTHIM solution should be focused solely on the role of  $\nabla_{S\theta} \cdot \mathbf{U}_{S\theta}^{mix}$ , rather than on the individual terms in  $\mathbf{F}$ .

### 3. Application to NEMO

#### *a. NEMO model domain*

The model data used for the validation of RTHIM come from a  $1^\circ$  resolution NEMO simulation run at the National Oceanography Centre (NOC) known as ORCA1-N403. It is a z-level Boussinesq global model, with the OPA ocean model (Madec 2008) coupled to the LIM2 sea-ice model (Timmermann et al. 2005). The horizontal grid is tripolar, giving a resolution of  $\sim 50$  km over the Arctic ocean. There are 75 vertical level ranging in thickness from  $\sim 1$  m at the surface to  $\sim 200$  m at the bottom. The model is forced by CORE atmospheric forcing (Large and Yeager 2004) which has  $2.5^\circ$  resolution. We took monthly mean outputs of net surface fluxes of heat and freshwater and of ocean temperature and salinity, from 20 years of the simulation from 1988-2007 and averaged them to produce a monthly climatology. The limited resolution of the simulation means that mesoscale features of the circulation are not resolved; however our focus is to validate the inverse method against an internally consistent system where subgrid mixing is parameterized. The Arctic and subpolar North Atlantic domain volume to which we apply RTHIM is bounded to the south by a line of constant latitude index on the ORCA1-N403 grid. The model has a tripolar grid, so the constant latitude index line is curved in latitude-longitude coordinates (see red lines on Fig. 1). The flow into and out of the domain is through a full-depth section defined by this line. In order for the balance of Eq. 11 to hold, the water masses that flow through the section must be geographically connected within the model so that they can mix. We therefore exclude ranges from the section corresponding to Hudson Bay and part of the Canadian Archipelago ( $94^\circ\text{W}$  to  $68^\circ\text{W}$ , although the latter is connected to the rest of the Arctic in the real ocean it is not connected in the model); and the Gulf of Bothnia ( $18^\circ\text{E}$  to  $22^\circ\text{E}$ ). We also mask out the surface fluxes and interior

water masses associated with these ranges since these do not contribute to the volume budget for the domain.

#### *b. $S - \theta$ grid*

We design an irregular  $S - \theta$  grid for use with RTHIM (see Appendix for grid node definitions). We saw in Fig. 2 that the majority of the area of the section occupies a small region in  $S - \theta$  space. The along-section distance  $\Delta x$  that can be resolved in the RTHIM solution is related to the  $\theta$  grid spacing  $\Delta \theta$  by  $\Delta x \approx (\frac{\partial \theta}{\partial x})^{-1} \Delta \theta$ , where  $\frac{\partial \theta}{\partial x}$  is the horizontal gradient of  $\theta$  (the equivalent applies in the  $S$  coordinate). An irregular grid allows us to resolve details of the flow through the section, while keeping the size of the inverse problem manageable. We want to focus the resolution in the regions of  $S - \theta$  space where gradients of  $S$  and  $\theta$  are small, with additional focus given to parts of the section where the transports are large. In order to do this, we first construct cumulative transport functions in  $S$  and  $\theta$  which measure the magnitude of the transport through the section below a contour, based on the absolute model velocities  $|v|$  normal to the section at each model grid cell:

$$|T|_S(S) = \sum_{S_{min}}^S |v| \Delta A, \quad |T|_\theta(\theta) = \sum_{\theta_{min}}^\theta |v| \Delta A \quad (12)$$

Here the sums are over the area of the section for which the salinity (temperature) is below the salinity (temperature) in the bracket. We then plot the transport functions normalized by their totals, which allows the  $\theta$  and  $S$  ranges to be discretized according to an equipartition of  $|T|$  (Fig. 4). Each point in  $\theta$  (or  $S$ ) identified by the red dashed lines on Fig. 4(b) (4(c)) as they intersect the  $x$ -axis then becomes a node in the  $\theta$  ( $S$ ) vectors used to construct the  $S - \theta$  grid.

216 *c. Advective flux*

217 During the constrained optimization, we want RTHIM to compute the advection term  $I_{adv}$  from  
 218 a surface reference level velocity  $v_{ref}$ .  $I_{adv}$  is calculated by assuming a relative velocity  $v_{rel}$  to be  
 219 added to  $v_{ref}$ :

$$v(x, z) = v_{ref}(x) + v_{rel}(x, z) \quad (13)$$

220

$$I_{adv}(S, \theta) = I_{ref}(S, \theta) + I_{rel}(S, \theta) \quad (14)$$

221 where  $(x, z)$  are coordinates in the along-section and vertical directions. The components of  $I_{adv}$   
 222 are found by binning relative velocities at the section:

$$I_{rel}(S, \theta) = \frac{1}{\Delta S \Delta \theta} \iint \Pi(S) \Pi(\theta) v_{rel} dA, \quad (15)$$

223 (and similarly for  $I_{ref}$ ), where  $v_{rel}(x, z) = v(x, z) - v_{surf}(x)$  is the NEMO section velocity relative to  
 224 the fixed surface velocity. The ‘ $\Pi$ ’s mask in only regions of the section between isohalines  $S \pm \frac{\Delta S}{2}$   
 225 and isotherms  $\theta \pm \frac{\Delta \theta}{2}$ , and the quantities are integrated over the whole section. We construct a  
 226 matrix  $\mathbf{A}$  such that  $I_{ref} = \mathbf{A} v_{ref}$ , then  $I_{adv}(S, \theta)$  can be calculated using Eq. 14.

227 In the initial condition,  $v_{ref}$  is taken as the model values with random noise added of between -5  
 228 cm/s and +5 cm/s with 5-cell boxcar smoothing applied (equivalent to smoothing over 5 degrees  
 229 longitude). This initial condition is designed to reflect the uncertainty on the surface velocities that  
 230 might be expected when applying RTHIM to observations and using surface geostrophic velocity  
 231 from satellite altimetry data for the initial  $v_{ref}$ . The 5 cm/s is slightly larger than the 3 cm/s  
 232 estimated by Gourcuff et al. (2011) as the uncertainty on altimetrically derived surface geostrophic  
 233 velocities, but also represents an upper limit on the uncertainty that might be expected from in-  
 234 situ current meter measurements (see e.g. Tsubouchi et al. 2012). We also constrain  $v_{ref}$  in the  
 235 solution to be within 10 cm/s of the NEMO model ‘truth’, which limits the range of solutions

while allowing for a generous amount of uncertainty on our ‘best guess’ by doubling the expected value.

#### d. Surface flux

Here we describe how the fluxes of heat and freshwater that forced the NEMO run are used to calculate  $\nabla_{S\theta} \cdot \mathbf{U}_{S\theta}^{surf}$  for input to RTHIM. The contribution of the surface fluxes to the volume budget,  $\nabla_{S\theta} \cdot \mathbf{U}_{S\theta}^{surf}$ , is a prescribed term in the RTHIM solution, assumed perfectly known. This is appropriate for validating with a model which is an internally consistent system; we discuss the implications for applying RTHIM to observations in section 5. The freshwater flux in  $m s^{-1}$  (see Fig. 1, left panel) is divided by the thickness of the model’s top layer,  $\Delta z^{surf}$ , obtaining  $f_w$  in  $s^{-1}$ , and  $U_{|S}^{surf}$  is then calculated as follows:

$$U_{|S}^{surf}(S^*, \theta^*) = \frac{-S_0}{\Delta S \Delta \theta} \iiint \Pi(S^*) \Pi(\theta^*) f_w dV. \quad (16)$$

Here the  $\Pi$ s mask in regions on the surface layer between isohalines  $S^*$  and  $S^* + \Delta S$  and between isotherms  $\theta^* \pm \frac{\Delta \theta}{2}$ . The different masking here compared with Eq. 15 for  $I_{adv}$  ensures that  $\nabla_{S\theta} \cdot \mathbf{U}_{S\theta}^{surf}$  will coincide with  $I_{adv}$  on the discrete grid, since  $U_{|S}^{surf}$  is calculated between  $S$  nodes and on  $\theta$  nodes, while  $U_{|\theta}^{surf}$  (below) is calculated on  $S$  nodes and between  $\theta$  nodes, therefore  $\nabla_{S\theta} \cdot \mathbf{U}_{S\theta}^{surf} = (\frac{\partial}{\partial S}, \frac{\partial}{\partial \theta}) \cdot (U_{|S}^{surf}, U_{|\theta}^{surf})$  will be on  $S$  and  $\theta$  nodes, as is  $I_{adv}$ . The heat flux in  $W m^{-2}$  (Fig. 1, right panel) is divided by  $(\rho_0 c_p^0 \Delta z^{surf} = 4.1 \times 10^6 \Delta z^{surf})$  to obtain  $f_\theta$  in  $K s^{-1}$ , and  $U_{|\theta}^{surf}$  calculated as follows:

$$U_{|\theta}^{surf}(S^*, \theta^*) = \frac{1}{\Delta S \Delta \theta} \iiint \Pi(S^*) \Pi(\theta^*) f_\theta dV \quad (17)$$

The  $\Pi$ s mask in regions on the surface layer between isohalines  $S^* \pm \frac{\Delta S}{2}$  and between isotherms  $\theta^*$  and  $\theta^* + \Delta \theta$ .

### 255 *e. Diffusive flux*

256 We described constructing an initial condition for the reference level velocities in section 3c.  
 257 We also require an initial condition for the components of the diffusive flux tensor  $\mathbf{F}$ . Using the  
 258 NEMO fields, we calculate the  $x, y$  and  $z$  components of the along-isopycnal gradients of  $S$  and  
 259  $\theta$  and their vertical gradients, assuming small isopycnal slopes (note that this assumption only  
 260 applies to the initial condition for  $\mathbf{F}$ , and is not required for the solution). We then calculate  
 261 the 4 components of  $\mathbf{F}$  by defining a diffusion tensor  $\mathbf{K}$  with a uniform isopycnal and vertical  
 262 component for the purposes of the initial condition (see Appendix). We also apply some smoothing  
 263 to the components of  $\mathbf{F}$  in the initial condition, since with our variable  $S - \theta$  grid they can be noisy  
 264 where  $\Delta S$  or  $\Delta \theta$  is small. We therefore apply a simple 2D boxcar smoothing to these terms.  
 265 Along with the surface flux term  $\nabla_{S\theta} \cdot \mathbf{U}_{S\theta}^{surf}$ , the diffusive fluxes are calculated for each month of  
 266 our NEMO monthly climatology, and the mean of each set of 12 fields is calculated for input to  
 267 RTHIM.

### 268 *f. Optimization*

269 Having established the inputs to Eq. 11, RTHIM can now be solved by minimizing the cost  
 270 function  $r^2$  in units of  $\text{Sv}^2$  ( $1 \text{ Sv} = 10^6 \text{ m}^3 \text{ s}^{-1}$ ) in the following:

$$r^2 = \sum_{S, \theta} (\epsilon \Delta S \Delta \theta)^2 + w \left[ \sum_{S, \theta} I_{adv} \Delta S \Delta \theta - T_{net} \right]^2 \quad (18)$$

271 where the term in square brackets on the RHS is a constraint on the net transport through the  
 272 section, calculated as the difference between the integrated section transport from the RTHIM  
 273 solution advection term  $I_{adv}$  and the known 1988-2007 time-mean NEMO net section transport  
 274 including Bering Strait ( $T_{net} = -0.41 \text{ Sv}$ ). This net section transport constraint is multiplied by  
 275 a weighting factor  $w$ , which adjusts the relative importance of the constraint compared to that of

276 the volume budget (the sensitivity of our results to the factor  $w$  is explored in section 4b). When  
277 applying RTHIM to observations,  $T_{net}$  would be set to zero or a known value; since we have an  
278 enclosed domain, zero net transport would be an appropriate assumption in the absence of other  
279 information.

280 An initial control vector is constructed in two sections: the first from the 4 components of  $\mathbf{F}$ ,  
281 which are arrays of values at each  $S$  and  $\theta$  on our grid; and the second from  $v_{ref}$ . Each section is  
282 normalized by the mean of that section's values to make all the values in the control vector of order  
283 1; this enables the minimization algorithm to more efficiently search the parameter space. Within  
284 Matlab/fmincon, we use the Interior Point algorithm to carry out the minimization (Byrd et al.  
285 1998). There is more than one option for terminating the optimisation on arrival at a satisfactory  
286 solution. We explored using the default criterion based on cost function gradient becoming smaller  
287 than a certain value (it should tend to zero at an extremum), but this was susceptible to gradient  
288 noise and oscillations in the solution. Instead we used a criterion based on the cost function value  
289 itself. When  $r^2$  drops below  $10^{-4} \text{ Sv}^2$ , we accepted the solution (corresponding to a misfit,  $r$ , of  
290 0.01 Sv, chosen to be significantly less than observational uncertainty of hydrographic sections or  
291 trans-basin mooring arrays).

## 292 4. Solution

### 293 *a. Section transport*

294 In this section we will examine the part of the RTHIM solution that diagnoses the transport  
295 through the section bounding the domain. We quantify the method's skill in reproducing the model  
296 'truth' from NEMO using a number of metrics and test the sensitivity of the solution to a range of  
297 reasonable parameters. The purpose is to demonstrate that RTHIM will find a good solution given,



for example, an uncertainty on  $v_{ref}$  that reflects that which would be present when applying the method to observations (i.e. the uncertainty in the surface absolute geostrophic velocities). RTHIM finds a surface  $v_{ref}$  by solving Eq. 11, given an initial condition obtained by taking the surface velocities from NEMO and adding some random noise. Given such an initial guess, RTHIM has sufficient skill to converge on the model truth with a high degree of precision (top panel of Fig. 5). The rms error between the RTHIM  $v_{ref}$  and the model truth for this solution was  $v_{rms} = 0.06 \text{ cm s}^{-1}$ . The longitude range shown corresponds to the part of the section indicated by the red line on Fig. 1 between Baffin Island to the west and Norway to the east. The longitude range west of Baffin Island including the Hudson bay is not part of our solution as explained in section 3a; Bering Strait is included in the solution but is not plotted. We then obtain the full section velocities by adding the known model shear to  $v_{ref}$  (in applying RTHIM to observations the shear will be obtained from thermal wind balance). Even with a high degree of agreement between the RTHIM and NEMO surface velocities, it is still possible to see differences in the full section velocities in the deep part of the section east of the Icelandic Plateau (note that since we use the actual NEMO model shear to construct the section velocities from  $v_{ref}$ , any differences at depth must be due to differences at the surface). This highlights the importance of obtaining a good solution for  $v_{ref}$ , particularly where the ocean is deepest. We define an additional skill measure comparing the section transport from the RTHIM solution as follows:

$$T_{skill} = \frac{1}{N} \sqrt{\sum_{x=1}^N \left[ \sum_z T_{sol}(x, z) - \sum_z T_{mod}(x, z) \right]^2} \quad (19)$$

where  $T_{sol}(x, z) = v_{sol}(x, z) dA(x, z)$  and  $T_{mod}(x, z) = v_{mod}(x, z) dA(x, z)$  are the volume transports in Sv through the geographical grid cell  $(x, z)$  at the section from RTHIM and NEMO, respectively. The sums over  $z$  in Eq. 19 are over the water column, and  $N$  is the number of  $x$ -grid cells along the section.  $T_{skill}$  therefore measures the rms error (RTHIM vs NEMO) for the depth-integrated

transports at each grid cell in  $x$ . For the RTHIM solution shown in Fig. 5,  $T_{skill}=0.03$  Sv, which is  
 less than 4% of the rms of the NEMO depth-integrated transports along the section.  
 The RTHIM solution  $v_{ref}$  is robust to a range of parameters. If we take an ensemble of initial  
 conditions (blue lines on Fig. 6, top panel) while varying a number of other model parameters  
 which will be described in the next subsection, the solutions (red lines on the same figure) cluster  
 around the model truth (black line). We can further demonstrate the model skill in solving for  $v_{ref}$   
 by examining the solution as it converges (Fig. 6, bottom panel). With a convergence tolerance of  
 $r^2 = 1$ , the solution (solid blue line) has only deviated from the initial condition (dotted blue line)  
 in a few places; however we note that in this initial period of optimization the cost function  $r^2$  has  
 reduced from  $\sim 10^6$  to  $< 1$ . This is achieved mainly through adjustments of the elements of  $\mathbf{F}$ ,  
 with some small adjustments to  $v_{ref}$  required to reduce the net transport constraint in Eq. 18 from  
 $\sim 10^3$  to  $\sim 10^{-5}$ . As the convergence tolerance is decreased, the  $v_{ref}$  solutions converge towards  
 the model truth, with a tolerance of  $10^{-4}$  yielding a solution (solid green line) that almost matches  
 the model (dotted black line).

### b. Solution sensitivities

We wish to establish some useful metrics for the RTHIM solution appropriate to a wider oceano-  
 graphic context and assess the sensitivity of the solution to a range of parameters in terms of those  
 metrics. First we define familiar streamfunctions of the section transport diagnosed from the  
 RTHIM solution, binned in terms of density, temperature and salinity:

$$\psi_{\sigma}(\sigma^*) = \int_{\sigma \leq \sigma^*} v dA \quad (20)$$

where  $v dA$  is the transport through the section, in this case integrated below contours of constant  
 potential density  $\sigma_2$  referenced to 2000 m. The similar streamfunctions  $\Psi_{\theta}(\theta^*)$  and  $\Psi_S(S^*)$

are defined in the same way, but integrated below contours of temperature and salinity. We then calculate the Meridional Overturning Circulation (MOC), Meridional Heat Transport (MHT) and Meridional Freshwater Transport (MFWT) through the section as follows:

$$MOC = \sum_{\sigma_{min}}^{\sigma_{max}} T(\sigma) \quad \text{for } T(\sigma) > 0 \quad (21)$$

$$MHT = \rho_0 c_p^0 \int_{\theta_{min}}^{\theta_{max}} \psi_{\theta} d\theta \quad (22)$$

$$MFWT = \frac{-1}{S_0} \int_{S_{min}}^{S_{max}} \psi_S dS \quad (23)$$

where in this case  $T(\sigma)$  represents the transport integrated between density contours  $0.001 \text{ kgm}^{-3}$  apart,  $\rho_0 c_p^0 = 4.1 \times 10^6 \text{ Jm}^{-3}\text{K}^{-1}$ , and  $S_0 = 35 \text{ PSU}$  is a reference salinity. Note that we calculate the MOC from  $T'(\sigma)$  as in Li et al. (2017) (their Eq. 7) rather than from the streamfunction.

There are a number of parameters which can affect the RTHIM solution. We have already mentioned adding random noise to the  $v_{ref}$  initial condition. We also produce an initial condition for the components of the diffusive flux  $\mathbf{F}$ , the other unknown in our inverse problem, based on a uniform diffusivity  $\mathbf{K}$  made up of along-isopycnal and vertical components,  $K$  and  $D$ . We test  $K$  values of  $10 \text{ m}^2\text{s}^{-1}$ ,  $20 \text{ m}^2\text{s}^{-1}$ ,  $50 \text{ m}^2\text{s}^{-1}$ ,  $100 \text{ m}^2\text{s}^{-1}$ ,  $200 \text{ m}^2\text{s}^{-1}$ ,  $500 \text{ m}^2\text{s}^{-1}$ ,  $1000 \text{ m}^2\text{s}^{-1}$ , and  $2000 \text{ m}^2\text{s}^{-1}$ ; and  $D$  values of  $10^{-5} \text{ m}^2\text{s}^{-1}$  and  $10^{-4} \text{ m}^2\text{s}^{-1}$ . There is also the 2D boxcar smoothing applied to the components of  $\mathbf{F}$  in the initial condition, which has an associated parameter for the number of cells over which to apply the smoothing (we smooth uniformly in both the  $S$  and  $\theta$  directions). We test integer values of 3, 5, 7 and 9 of this parameter, and an additional case where we simply replace each element of  $F_{C_1C_2}(S, \theta)$  with the mean of that component over all  $S - \theta$  space. In section 3b we described the design of an irregular  $S - \theta$  grid over which we bin all the terms of our volume budget, to focus the available resolution where it is needed by dividing up the transport through the section equally in  $S$  or  $\theta$  coordinates. We can choose the number of segments to divide the ranges into, and test grids of  $10 \times 10$ ,  $13 \times 13$ ,  $15 \times 15$ , and  $17 \times 17$ ; at

363 higher resolution than this the number of possible solutions becomes very large and RTHIM has  
 364 difficulty converging. Finally the constraint on the net section transport in Eq. 18 has a weighting  
 365 factor  $w$  which we vary, testing values of 0, 1, 10, 20, 50, 100, 200, 500, and 1000. We summarize  
 366 the sensitivity to all these parameters of the streamfunctions and metrics defined above, in Fig. 7  
 367 and Table 1.

368 The principle sensitivities of the RTHIM solutions are to the  $S - \theta$  grid and the diffusivity  $K$  ap-  
 369 plied to the  $\mathbf{F}$  initial condition. This is evident in the purple and dark blue lines on Fig. 7 and in  
 370 the first 5 rows below the headings of Table 1. In particular a value of  $K = 10 \text{ m}^2\text{s}^{-1}$  significantly  
 371 degrades the solution (see Fig. 8 and upper values in the ranges of row 4, columns 3 and 4 on  
 372 Table 1). The sensitivity to the other parameters is small; however we find that if no smoothing  
 373 is applied to  $\mathbf{F}$  in the initial condition, RTHIM will not converge, and if we remove the net trans-  
 374 port constraint (i.e. set  $w = 0$ ), the solution suffers dramatically (see Fig. 8). If we consider that  
 375 this exercise has informed the appropriate choices of parameters as a minimum  $S - \theta$  grid size of  
 376  $(13 \times 13)$  and a  $K$  of  $100 - 500 \text{ m}^2\text{s}^{-1}$ , from the last row of Table 1 we can say that the MHT and  
 377 MFWT are determined by RTHIM with uncertainties of  $\pm 0.03 \text{ PW}$ , and  $\pm 0.03 \text{ Sv}$ , respectively,  
 378 and their mean values agree perfectly with the NEMO model truth. In the case of the MOC, the  
 379 distribution is slightly skewed, with a range of 10.76-12.91 Sv surrounding a mean of 11.64 Sv;  
 380 the mean is still in good agreement with the model truth of 11.53 Sv. These uncertainties on the  
 381 MOC, MHT and MFWT metrics translate to percentage errors of less than 12%, 10% and 19%,  
 382 respectively, when compared with the model truth.

383 A strength of this method is the ability to view the circulation in thermohaline coordinates. Fig.  
 384 9 (left panel) shows  $I_{adv}$  as it is used within RTHIM: binned in  $S - \theta$  coordinates. The small  
 385 residual between the term provided by the RTHIM solution and the term constructed by binning  
 386 the NEMO section transports on the same grid (right panel) shows the two are very similar. The

387 transport through the section is dominated by a northward flow of warm, salty waters (red colors)  
388 and a compensating southward flow of cooler, fresher waters (blue colors). This is what would be  
389 expected for this region, since warm, salty North Atlantic water flowing northward is balanced by  
390 cooler, fresher water created by boundary processes in the Arctic and Subpolar Gyre.

### 391 *c. Volume budget*

392 In section 2b we described the volume budget in thermohaline coordinates which RTHIM uses  
393 to obtain a solution. We can examine the terms in the volume budget to gain an insight into the  
394 contributions of each process to the increase or decrease in volume of water masses in each region  
395 of  $S - \theta$  space (Fig. 10). Mixing processes (Fig 10 (a)) tend to increase the volume of water  
396 towards the center of the  $S - \theta$  distribution while decreasing the volume of water at its fringes.  
397 This is in accordance with what we expect, since mixing acts down tracer gradients to homogenize  
398 extremes in  $S$  and  $\theta$ . By contrast, surface fluxes (b) tend to increase the volume of water at the  
399 fringes of the  $S - \theta$  distribution while decreasing the volume towards the center. This again is an  
400 expected consequence of surface forcing: in particular we can see cooling of the warm surface  
401 waters due to the Arctic winds and salinification of the cooler water due to brine rejection in ice  
402 formation, both leading to the formation of dense waters. We have already discussed the advection  
403 term (c) in terms of the inflow and outflow of different water masses; what we can also see on Fig.  
404 10 is how the residual created by adding the mixing and surface flux terms is largely accounted  
405 for by the advection term. The volume trend (d) is comparatively small. After adding together  
406 the terms in the volume budget, we are left with a residual,  $\epsilon$ . This reduces by several orders of  
407 magnitude between the initial condition and the RTHIM solution (Fig. 11).

408 An alternative way to view the volume budget is by integrating in one direction or the other in  
409 thermohaline coordinates. This helps us to see more quantitatively the size of the contributions

of each process to the volume budget, and their relative roles at each point in the  $S$  or  $\theta$  range. Integrated first through  $S$  and then cumulatively in  $\theta$  (Fig. 12, left panel), we see that at low temperatures the balance is dominated by a competition between mixing and surface fluxes; whereas at higher temperatures the advection is the larger term, balancing out the other two. The y-values of the lines on Fig. 12 at a given  $x$  represent the transformation in volume below that isotherm (or isohaline). This means that a range in  $x$  where the gradient  $\frac{dy}{dx}$  is positive corresponds to an increase in the volume of water in that temperature or salinity range by a given process, and a range with negative gradient corresponds to a decrease in volume. Therefore on the left panel of Fig. 12 we see surface fluxes increasing the volume of the coldest water and decreasing the volume of the warmer water; meanwhile mixing decreases the volume of the coldest ( $-3^\circ$  to  $-1.3^\circ\text{C}$ ) and warmest waters ( $> 2.5^\circ\text{C}$ ) and increases the volume of waters at intermediate temperatures; and finally advection decreases the volume of water up to  $2.5^\circ\text{C}$  (outflow) and increases the volume above that temperature (inflow). The trend term is relatively small. In salinity coordinates (right panel of Fig. 12) the balance is between mixing and surface fluxes between 29.5 and 32.5 PSU; and between mixing and advection at higher salinities, with surface fluxes playing a smaller role. Mixing increases the volume between 29.5-31.5 PSU and decreases the volume between 31.5-32.5 PSU; meanwhile surface fluxes have the opposing effect. Mixing then increases volume between 32.5-34.5 PSU and decreases volume of the saltiest water; in this range balanced by advection. In section 4b we validated one of the unknowns in our RTHIM solution, the advection term, by comparing section velocities with a known model ‘truth’ from NEMO and exploring the solution sensitivities. We now examine the other unknown: the mixing term. As noted in section 2b, the term constrained in the RTHIM solution is  $\nabla_{S\theta} \cdot \mathbf{U}_{S\theta}^{mix}$ , the mixing term from Fig. 10. Using NEMO diagnostics of the tendencies in temperature and salinity due to mixing, we can construct

the components of the transformation vector due to mixing as:

$$U_{|S}^{mix-NEMO}(S^*, \theta^*) = \frac{-S_0}{\Delta S \Delta \theta} \iiint \Pi(S^*) \Pi(\theta^*) \frac{dS^{mix}}{dt} dV. \quad (24)$$

$$U_{|\theta}^{mix-NEMO}(S^*, \theta^*) = \frac{1}{\Delta S \Delta \theta} \iiint \Pi(S^*) \Pi(\theta^*) \frac{d\theta^{mix}}{dt} dV \quad (25)$$

where  $\frac{d\theta^{mix}}{dt}$  and  $\frac{dS^{mix}}{dt}$  are the NEMO temperature and salinity trends due to mixing in  $\text{Ks}^{-1}$  and  $\text{s}^{-1}$ , respectively. We can then calculate  $\nabla_{S\theta} \cdot U_{S\theta}^{mix-NEMO}$ , the NEMO equivalent of our RTHIM mixing term, to compare with the RTHIM solutions.

We can compare the mixing terms from the RTHIM solution and NEMO by plotting each on the same  $S - \theta$  grid (Fig. 13). There are some broadly similar patterns such as the decrease in volume of waters at low temperatures and an increase in volume towards the center of the  $S - \theta$  distribution, and there are differences such as the larger values in NEMO at lower salinities. It is not surprising that RTHIM does not capture the details of the NEMO diffusive transformation. The mixing term is highly differentiated (it is calculated from  $\nabla_{S\theta}^2 F$ ) and the dominant signals are likely the advection at the boundary and surface fluxes, with mixing being a small residual in many cases. So a small percentage error in the flow at the boundary may manifest as a large sized error in the mixing terms. We can also integrate the mixing terms from Fig. 13 in  $S - \theta$  space, in one dimension or the other (Fig. 14). Although the structure of the NEMO and RTHIM terms differs, the convergence of the blue and black lines at the top end of the ranges on each panel demonstrates that the total diffusive transformation integrated over all  $S - \theta$  space is almost the same (0.42 Sv and 0.14 Sv in RTHIM and NEMO, respectively). This shows that the bulk diffusive transformation is in the same balance as in the NEMO ‘truth’, in equilibrium with advection and surface fluxes when integrated over the control volume.

## 5. Discussion and conclusions

### *a. Summary*

We have developed ‘RTHIM’, a new inverse method in thermohaline coordinates to use temperature, salinity and surface flux observations to provide estimates of water mass transformation and circulation in an enclosed domain. The method builds on the work of Groeskamp et al. (2014a,b) and others, and allows analysis previously done globally to be applied to a specific region of the ocean, thereby retaining additional useful geographical information about the circulation. Using inputs of time-mean  $S$ ,  $\theta$ , and surface fluxes of heat and salt, RTHIM solves for a surface reference level velocity  $v_{ref}$  at the section bounding the domain and interior mixing within it, while constraining the mixing to be down tracer gradients and  $v_{ref}$  to be within  $\pm 10 \text{ cm s}^{-1}$  of an initial guess. Full section velocities are constructed from  $v_{ref}$  assuming a known vertical velocity shear. RTHIM was applied to model data from NEMO, and the solution compared to the model ‘truth’. The rms error between RTHIM and NEMO for  $v_{ref}$  was less than  $0.63 \text{ cm s}^{-1}$  from an ensemble of solutions with varying parameters in RTHIM. Estimates of the MOC from the ensemble were 10.76-12.91 Sv with a mean of 11.64 Sv, compared to 11.53 Sv in NEMO. The MHT and MFWT from RTHIM were  $0.29 \pm 0.03 \text{ PW}$  and  $-0.16 \pm 0.03 \text{ Sv}$ , in exact agreement with NEMO. The transformation due to mixing from the RTHIM solutions was also compared with that obtained diagnostically from NEMO, and while there are some similar patterns the agreement is not as strong. However this is expected because the mixing in NEMO is governed by a parameterization including a specified horizontal eddy diffusivity, whereas in RTHIM we only constrain the diffusive flux tensor  $F$ .



474 *b. Previous studies of the region*

475 We have applied RTHIM to a domain including the Arctic and part of the subpolar North At-  
476 lantic, since our future aim is to use it to estimate the circulation and mixing from observations in  
477 the OSNAP study region. There have been some previous efforts to study the circulation in these  
478 regions using a thermohaline coordinate system. In a purely diagnostic study, Pemberton et al.  
479 (2015) calculated the contributions of mixing, surface fluxes and advection to water mass trans-  
480 formation in the Arctic using NEMO model outputs. They used much higher resolution in  $S - \theta$   
481 space than we were able to achieve with RTHIM, and they also separated the effects of isopyc-  
482 nal and diapycnal mixing; however since their method was diagnostic it could not be applied to  
483 observations where the complete fields are not available. In comparing our Fig. 10 to their Fig.  
484 16, there is striking similarity between the advection terms. The surface and interior mixing terms  
485 are broadly similar, with formation of water at the fringes of the  $S - \theta$  distribution by the surface  
486 fluxes with destruction towards the center, and vice-versa for the interior mixing (note the opposite  
487 sign convention for the formation/destruction of water masses). However there are some differ-  
488 ences in the details. We see relatively little transformation of the coldest water between salinities  
489 of 29-32 PSU in the RTHIM solution where Pemberton see significant transformation. On the  
490 other hand, we see significant transformation up to  $\sim 2^\circ\text{C}$  in the salinity range 32-34 PSU where  
491 Pemberton find almost all the transformation occurs below  $0^\circ\text{C}$  in the same salinity range. The  
492 differences are likely due to a combination of the higher resolution in the Pemberton study, the dif-  
493 ferent domains (Pemberton's Arctic does not include the GIN seas), and the differences between  
494 RTHIM and NEMO's treatment of the interior mixing that we have already discussed. An inverse  
495 estimate based on observations was carried out by Tsubouchi et al. (2012) for one month of data  
496 in the summer of 2005. Their method relied on current data from moorings and CTD sections,

and they calculated boundary fluxes and water mass transformation using a box-inverse approach. RTHIM could be applied to observational reanalysis to obtain such estimates over a much longer time period.

### c. RTHIM sensitivity

In section 4b we found that RTHIM solutions were robust provided some constraints are placed on the parameters involved in the inverse model setup. RTHIM demonstrated good skill for an  $S - \theta$  grid of at least  $13 \times 13$  cells; however the remainder of the sensitivity study was carried out with a grid size of  $17 \times 17$ , the highest resolution for which RTHIM was able to converge. When applying RTHIM to observations it would make sense to use the highest possible resolution so as to retain the maximum information both in  $S - \theta$  space and in physical space for the determination of  $v_{ref}$ . The trade-off would be one of computation time, and this would become a factor if large numbers of RTHIM runs were required. For the diapycnal diffusivity  $D$  applied to the initial condition of the diffusive flux tensor, we only explored two values:  $10^{-4}$  and  $10^{-5} \text{ m}^2\text{s}^{-1}$ . This is reasonable because the average diapycnal diffusivity over the global ocean is well constrained, although its value can vary locally by several orders of magnitude (see e.g. Munk and Wunsch 1998). The volume-weighted time- and spatial-mean of the vertical diffusivity in NEMO for our domain was  $5.6 \times 10^{-5} \text{ m}^2\text{s}^{-1}$ . We explored a wider range of the isopycnal diffusivity  $K$  since this is a more uncertain parameter involved in the parameterization of unresolved eddies in the NEMO model. Our optimal initial condition values of  $K = 100 - 500 \text{ m}^2\text{s}^{-1}$  are also consistent with NEMO, where the volume-weighted mean lateral diffusivity for our domain was  $473 \text{ m}^2\text{s}^{-1}$ . The inability of RTHIM to converge on a solution when  $\mathbf{F}$  is not smoothed in the initial condition reflects the fact that  $\mathbf{F}$  is twice differentiated in  $S - \theta$  space, so that any noise on the initial fields may be amplified causing very large initial values of  $\nabla_{S\theta} \cdot \mathbf{U}_{S\theta}^{mix}$ . A minimal amount of smoothing

520 of  $F$  proved to be enough to overcome this problem. The sensitivity to the other parameters  
521 explored was small.

#### 522 *d. Future application to observations*

523 This validation exercise has proven the effectiveness of RTHIM when applied to an internally  
524 consistent system, where the ocean has been forced by the prescribed surface fluxes, and where  
525 there are no gaps in the data input to the inverse model. When applying the model to observations,  
526 there will be some additional challenges to overcome.

527 We can obtain the temperature and salinity fields needed to construct the diffusive fluxes initial  
528 condition and bin the advective fluxes in  $S - \theta$  space from observational reanalysis such as EN4  
529 (Good et al. 2013). However, the sparseness of observations over much of the Arctic means that  
530 these regions are heavily weighted towards model data. It remains to be seen how much of an  
531 obstacle this will pose to obtaining good RTHIM solutions, however since the interior observa-  
532 tions are only required for constructing the initial condition, and the validation has proven some  
533 resilience to this, it seems reasonable to be optimistic.

534 In our validation we have also assumed the surface fluxes to be a known quantity. This will not be  
535 the case for the application, where again there is quite significant uncertainty in places due to a lack  
536 of available observations. This will contribute a degree of uncertainty to the mixing solution, which  
537 is affected through the volume budget. Our intended approach is to run RTHIM using a range  
538 of surface flux products (for example Lindsay et al. 2014, suggest ERA-INTERIM, CFSR and  
539 MERRA are the most consistent with observations in the Arctic) to constrain our estimates. Recent  
540 efforts to address the lack of observations such as the N-ICE2015 expedition (Granskog et al. 2016)  
541 and the upcoming MOSAiC expedition (<http://www.mosaicobservatory.org/index.html>)  
542 may also provide valuable data for the application of RTHIM to the region.

During the validation we have calculated an initial condition for the reference level velocity by adding noise to the model truth, and have taken the vertical velocity shear as the model shear. When applying to observations, we will obtain our  $v_{ref}$  initial condition from AVISO surface geostrophic velocities. We have accounted for uncertainties in the AVISO velocities through the noise added to the initial condition, but these errors can be larger at land boundaries. Gourcuff et al. (2011) found that uncertainties in altimetric surface geostrophic velocities near the oceanic western boundary with Greenland led to uncertainties in the East Greenland Irminger Current from an inverse method of  $\sim 30\%$ , and that in general altimetric velocities were weaker than those obtained from Ship Acoustic Doppler Current Profiler observations along the OVIDE section between Greenland and Portugal. These factors will need to be considered when making use of AVISO surface geostrophic velocities with RTHIM. The assumption of known velocity shear could be met by a variety of observational constraints. For example, current meter moorings could give direct measurements of velocity. Alternatively, below the Ekman layer and away from strong currents, the flow is geostrophic, so thermal wind shear may be derived from observations of  $S$  and  $\theta$  along the section. For the OSNAP section, both types of observational constraint are present. The region is also well sampled by the ARGO program, so reanalyses are well constrained by observations (Good et al. 2013). Furthermore, for the OSNAP region, the Ekman component of the advection is weak, contributing only  $\sim 1$  Sv to the overturning (Mercier et al. 2015). Finally, we have carried out the current analysis for a 20-year mean of NEMO data. Ultimately our intention is to use RTHIM to examine temporal variability in the circulation, which would mean shortening the averaging period, perhaps to inter-annual or shorter variability. This could increase the size of the trend term, which in the validation proved small enough to neglect (although we have not done so); since it will be harder to calculate from uncertain observed interior distributions of  $S$  and  $\theta$ , its importance will place a lower limit on the timescale of variability we can study.

567 *e. Comparison with earlier methods*

568 RTHIM has built on previously developed inverse methods for diagnosing the oceanic circu-  
569 lation from hydrographic observations, and has several advantages over its predecessors. It is a  
570 natural extension of the traditional box inverse method for determining the flow through a section  
571 by solving for a reference level velocity, but instead of dividing the section into layers of depth  
572 or density, we use contours of  $S$  and  $\theta$ , thereby defining a coordinate system suitable for studying  
573 the conservation of heat and salt. The Bernoulli method (Killworth 1986) and beta-spiral method  
574 (Stommel and Schott 1977) both make use of gradients of tracers such as potential vorticity on  
575 isopycnals, but assume no mixing in their solution. The Tracer Contour Inverse Method (TCIM)  
576 of Zika et al. (2010) and Thermohaline Inverse Method of Groeskamp et al. (2014a) have mixing  
577 as a leading-order process, however as for the box inverse, the mixing has a fixed spatial structure.  
578 In the case of TCIM and the box inverse they assume one coefficient of isopycnal and diapyc-  
579 nal mixing in each layer. The ability of RTHIM to constrain mixing to be downgradient without  
580 imposing such a simplified structure makes it a major advance on earlier methods.

581 *f. Conclusion*

582 In summary, we have presented and carried out a successful validation of a new inverse method,  
583 RTHIM. While its application to observations will present some challenges, the method has the  
584 potential to provide independent estimates of circulation and interior mixing complementary to the  
585 OSNAP array observations, and could ultimately be applied to any enclosed region of the ocean in  
586 future work. A verification test of RTHIM and its assumptions may be derived from a hindcast of  
587 independently-observed section transport, such as from the OSNAP array. If the hindcast proves  
588 to be skillful, that further supports the likely validity of RTHIM solutions for the OSNAP section  
589 at other times.

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 594 (NOC) for their help with the NEMO outputs. The model output used for the inverse model  
 595 validation is stored at the British Oceanographic Data Centre under doi:10.5285/6371e0e7-8197-  
 596 2959-e053-6c86abc0630d.

## 597 APPENDIX

### 598 **Symmetric diffusive flux tensor constraint**

599 Here we derive the constraint that the diffusive flux tensor is symmetric as used in RTHIM. Con-  
 600 sider temperature and salinity iso-surfaces with unit normal vectors  $\nabla\theta/|\nabla\theta|$  and  $\nabla S/|\nabla S|$  respec-  
 601 tively. The flux of heat and salt per unit  $\theta$  and  $S$  across these surfaces is given by the flux tensor  $\mathbf{F}$   
 602 with components

$$F_{\theta\theta}(S^*, \theta^*) = \frac{1}{\Delta S} \iint \Pi(S^*) (\mathbf{K} \nabla\theta \cdot \nabla\theta / |\nabla\theta|) dA_{\theta^*}, \quad (\text{A1})$$

$$F_{\theta S}(S^*, \theta^*) = \frac{1}{\Delta\theta} \iint \Pi(\theta^*) (\mathbf{K} \nabla\theta \cdot \nabla S / |\nabla S|) dA_{S^*}, \quad (\text{A2})$$

$$F_{S\theta}(S^*, \theta^*) = \frac{1}{\Delta S} \iint \Pi(S^*) (\mathbf{K} \nabla S \cdot \nabla\theta / |\nabla\theta|) dA_{\theta^*}, \quad (\text{A3})$$

$$F_{SS}(S^*, \theta^*) = \frac{1}{\Delta\theta} \iint \Pi(\theta^*) (\mathbf{K} \nabla S \cdot \nabla S / |\nabla S|) dA_{S^*}, \quad (\text{A4})$$

606 where  $\Pi(S^*)$  is a boxcar function over  $S^* \pm \Delta S/2$ ,  $\mathbf{K}$  is a 3D and time dependent diffusion tensor  
 607 and  $\iint dA_{S^*}$  is an area integral over the surface where  $S = S^*$ . Each component of  $\mathbf{F}$ ,  $F_{C_1 C_2}$  represents  
 608 the diffusive flux of tracer  $C_1$  across and in the direction perpendicular to the iso-surface of tracer  
 609  $C_2$ .

Considering specifically the diffusive flux of temperature across the salinity surface and salt across the temperature surface in the limit as  $\Delta\theta$  and  $\Delta S$  become small we have

$$F_{\theta\theta}(S^*, \theta^*) = \frac{1}{\Delta S \Delta \theta} \iiint \Pi(\theta^*) \Pi(S^*) \mathbf{K} \nabla \theta \cdot \nabla \theta dV \quad (\text{A5})$$

$$F_{\theta S}(S^*, \theta^*) = \frac{1}{\Delta S \Delta \theta} \iiint \Pi(\theta^*) \Pi(S^*) \mathbf{K} \nabla \theta \cdot \nabla S dV \quad (\text{A6})$$

$$F_{S\theta}(S^*, \theta^*) = \frac{1}{\Delta S \Delta \theta} \iiint \Pi(\theta^*) \Pi(S^*) \mathbf{K} \nabla S \cdot \nabla \theta dV \quad (\text{A7})$$

$$F_{SS}(S^*, \theta^*) = \frac{1}{\Delta S \Delta \theta} \iiint \Pi(\theta^*) \Pi(S^*) \mathbf{K} \nabla S \cdot \nabla S dV \quad (\text{A8})$$

Typically coarse resolution ocean models use diffusion tensors with off diagonal terms to account for sub-grid adiabatic advective effects which arise in Eulerian coordinates (e.g. Stoke's drift and transient eddy advection). These are not relevant to transport across iso-surfaces which move with such adiabatic advection and the diffusion tensor can be assumed to have only diagonal elements. We assume the same diffusion tensor applies to both heat and salt (i.e. that turbulent dominates over molecular diffusion). The diffusivity tensor having only diagonal elements and being equivalent for both heat and salt implies that  $\mathbf{K} \nabla \theta \cdot \nabla S = \mathbf{K} \nabla S \cdot \nabla \theta$  and hence that  $F_{S\theta} = F_{\theta S}$ .

### **$S - \theta$ grid nodes**

The grid nodes constructed from the transport functions detailed on Fig. 4, including additional nodes at either end to ensure binning of the whole range of  $(S, \theta)$  found within the control volume, are as follows:

$\theta$ :  $[-4, -3.05, -1.65, -1, -0.75, -0.1, 0.55, 0.95, 1.3, 2, 3.05, 6.1, 7.2, 7.55, 8.8, 13.15, 14]$

$S$ :  $[6, 6.93, 32.15, 32.86, 33.76, 34.12, 34.46, 34.67, 34.75, 34.78, 34.83, 34.88, 34.95, 35.01, 35.05, 35.55, 36]$ .

### **Sensitivity study breakdown**

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729

## LIST OF TABLES

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**Table 1.** A summary of the sensitivities of RTHIM metrics to various parameters. Each row details an ensemble of runs where a particular parameter (column 1) is varied within a range (column 2). All other parameters are kept constant while exploring a particular parameter. The remaining columns give the metrics of the rms difference between NEMO and RTHIM reference level velocities and depth-integrated transports  $v_{rms}$  and  $T_{skill}$ ; and the Meridional Overturning Circulation (MOC), Meridional Heat Transport (MHT) and Meridional Freshwater Transport (MFWT) as described in section 4. Where ‘range’ appears at the column head, the lower and upper values of the metric from the ensemble are given. Where a value appears in italics at the column head, these are the NEMO values. The parameters are the number of nodes in  $S$  and  $\theta$  on the RTHIM  $S - \theta$  grid, the vertical and lateral diffusivities  $D$  and  $K$  applied to the diffusive flux initial condition, the weighting factor  $w$  applied to the section net transport constraint, the random noise applied to the  $v_{ref}$  initial condition, and the number of cells of boxcar smoothing applied to the diffusive flux initial condition. The MOC and MFWT are in Sv; the MHT is in PetaWatts (PW). The last row of the table summarizes the results excluding rows 1 and 4. The break down of the results used to construct this table is given in Table 2 in the Appendix . . . . 37

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**Table 2.** Breakdown of the results of the sensitivity study summarised in Table 1. For each group of runs (column 2) all parameters (columns 3-7) are kept constant except the one being tested for the sensitivity of the metrics (columns 8-12) to that parameter. The parameters are the number of nodes on the RTHIM  $S$  and  $\theta$  grids, the vertical and lateral diffusion coefficients applied to the diffusive flux initial condition  $D$  and  $K$  in  $m^2 s^{-1}$ , the weighting factor  $w$  on the section solution net transport constraint, the random noise applied to the  $v_{ref}$  initial condition (no column), and the smoothing applied to the diffusive flux initial condition. The metrics of  $v_{rms}$  in  $cms^{-1}$ ,  $T_{skill}$  in Sv, MOC in Sv, MHT in PW and MFWT in Sv are as described in section 4. Where metric values are reported as N/A RTHIM failed to converge on a solution.  $5cms^{-1}$  random noise is added to the initial  $v_{ref}$  for all runs, but for each grouping except for the  $v_{ref}$  I.C. noise grouping the same noise profile is used for each run within a group. . . . . 38

TABLE 1. A summary of the sensitivities of RTHIM metrics to various parameters. Each row details an ensemble of runs where a particular parameter (column 1) is varied within a range (column 2). All other parameters are kept constant while exploring a particular parameter. The remaining columns give the metrics of the rms difference between NEMO and RTHIM reference level velocities and depth-integrated transports  $v_{rms}$  and  $T_{skill}$ ; and the Meridional Overturning Circulation (MOC), Meridional Heat Transport (MHT) and Meridional Freshwater Transport (MFWT) as described in section 4. Where ‘range’ appears at the column head, the lower and upper values of the metric from the ensemble are given. Where a value appears in italics at the column head, these are the NEMO values. The parameters are the number of nodes in  $S$  and  $\theta$  on the RTHIM  $S - \theta$  grid, the vertical and lateral diffusivities  $D$  and  $K$  applied to the diffusive flux initial condition, the weighting factor  $w$  applied to the section net transport constraint, the random noise applied to the  $v_{ref}$  initial condition, and the number of cells of boxcar smoothing applied to the diffusive flux initial condition. The MOC and MFWT are in Sv; the MHT is in PetaWatts (PW). The last row of the table summarizes the results excluding rows 1 and 4. The break down of the results used to construct this table is given in Table 2 in the Appendix

Parameter	Range	$v_{rms}$	$T_{skill}$	MOC (11.53)	MOC	MHT (0.29)	MHT	MFWT (-0.16)	MFWT
		(range)	(range)	(mean)	(range)	(mean)	(range)	(mean)	(range)
Grid size	10-17	0.14, 0.92	0.09, 0.74	12.61	11.00, 15.05	0.32	0.28, 0.37	-0.13	-0.18, -0.06
Grid size	13-17	0.14, 0.35	0.09, 0.20	11.80	11.00, 12.25	0.30	0.28, 0.32	-0.15	-0.18, -0.13
$D$ ( $m^2 s^{-1}$ )	$10^{-4} - 10^{-5}$	0.07, 0.15	0.04, 0.10	11.58	11.44, 11.72	0.30	0.29, 0.30	-0.17	-0.17, -0.17
$K$ ( $m^2 s^{-1}$ )	10-2000	0.07, 1.99	0.04, 1.90	14.49	11.44, 28.30	0.26	0.21, 0.31	-0.18	-0.32, -0.14
$K$ ( $m^2 s^{-1}$ )	100-500	0.07, 0.63	0.04, 0.34	11.85	11.44, 12.36	0.28	0.26, 0.31	-0.16	-0.17, -0.14
$w$	1-1000	0.09, 0.32	0.06, 0.23	11.50	10.76, 12.91	0.29	0.28, 0.29	-0.16	-0.19, -0.14
$v_{ref}$ I.C.	$\pm 5 \text{ cms}^{-1}$ noise	0.07, 0.23	0.04, 0.17	11.74	11.34, 12.25	0.29	0.28, 0.31	-0.17	-0.17, -0.15
$\mathbf{F}$ smoothing	3-9 and mean	0.06, 0.09	0.04, 0.06	11.42	11.36, 11.55	0.29	0.29, 0.29	-0.17	-0.17, -0.16
Overall		0.06, 1.99	0.04, 1.90	12.78	10.76, 28.30	0.28	0.21, 0.37	-0.17	-0.32, -0.06
Excl. outliers		0.06, 0.63	0.04, 0.34	11.64	10.76, 12.91	0.29	0.26, 0.32	-0.16	-0.19, -0.13

TABLE 2. Breakdown of the results of the sensitivity study summarised in Table 1. For each group of runs (column 2) all parameters (columns 3-7) are kept constant except the one being tested for the sensitivity of the metrics (columns 8-12) to that parameter. The parameters are the number of nodes on the RTHIM  $S$  and  $\theta$  grids, the vertical and lateral diffusion coefficients applied to the diffusive flux initial condition  $D$  and  $K$  in  $\text{m}^2 \text{s}^{-1}$ , the weighting factor  $w$  on the section solution net transport constraint, the random noise applied to the  $v_{ref}$  initial condition (no column), and the smoothing applied to the diffusive flux initial condition. The metrics of  $v_{rms}$  in  $\text{cm s}^{-1}$ ,  $T_{skill}$  in Sv, MOC in Sv, MHT in PW and MFWT in Sv are as described in section 4. Where metric values are reported as N/A RTHIM failed to converge on a solution.  $5 \text{ cm s}^{-1}$  random noise is added to the initial  $v_{ref}$  for all runs, but for each grouping except for the  $v_{ref}$  I.C. noise grouping the same noise profile is used for each run within a group.

Run	Parameter varied	Grid size	$D$	$K$	$w$	$F$ smoothing	$v_{rms}$	$T_{skill}$	MOC	MHT	MFWT
1	Grid size	$10 \times 10$	$10^{-4}$	200	10	3-cell boxcar	0.92	0.74	15.05	0.37	-0.06
2	Grid size	$13 \times 13$	$10^{-4}$	200	10	3-cell boxcar	0.35	0.19	12.25	0.32	-0.13
3	Grid size	$15 \times 15$	$10^{-4}$	200	10	3-cell boxcar	0.23	0.20	11.00	0.28	-0.15
4	Grid size	$17 \times 17$	$10^{-4}$	200	10	3-cell boxcar	0.14	0.09	12.14	0.29	-0.18
5	F I.C. diffusivities	$17 \times 17$	$10^{-4}$	10	10	3-cell boxcar	1.84	1.81	22.08	0.25	-0.12
6	F I.C. diffusivities	$17 \times 17$	$10^{-4}$	20	10	3-cell boxcar	1.03	0.69	12.64	0.25	-0.24
7	F I.C. diffusivities	$17 \times 17$	$10^{-4}$	50	10	3-cell boxcar	N/A	N/A	N/A	N/A	N/A
8	F I.C. diffusivities	$17 \times 17$	$10^{-4}$	100	10	3-cell boxcar	0.34	0.32	12.36	0.27	-0.16
9	F I.C. diffusivities	$17 \times 17$	$10^{-4}$	200	10	3-cell boxcar	0.07	0.04	11.72	0.29	-0.17
10	F I.C. diffusivities	$17 \times 17$	$10^{-4}$	500	10	3-cell boxcar	0.27	0.16	11.64	0.31	-0.17
11	F I.C. diffusivities	$17 \times 17$	$10^{-4}$	1000	10	3-cell boxcar	0.80	0.51	13.74	0.22	-0.16
12	F I.C. diffusivities	$17 \times 17$	$10^{-4}$	2000	10	3-cell boxcar	1.02	0.63	14.36	0.21	-0.15
13	F I.C. diffusivities	$17 \times 17$	$10^{-5}$	10	10	3-cell boxcar	1.99	1.90	28.30	0.30	-0.32
14	F I.C. diffusivities	$17 \times 17$	$10^{-5}$	20	10	3-cell boxcar	0.85	0.70	12.84	0.27	-0.20
15	F I.C. diffusivities	$17 \times 17$	$10^{-5}$	50	10	3-cell boxcar	N/A	N/A	N/A	N/A	N/A
16	F I.C. diffusivities	$17 \times 17$	$10^{-5}$	100	10	3-cell boxcar	0.63	0.34	12.07	0.27	-0.14
17	F I.C. diffusivities	$17 \times 17$	$10^{-5}$	200	10	3-cell boxcar	0.15	0.10	11.44	0.30	-0.17
18	F I.C. diffusivities	$17 \times 17$	$10^{-5}$	500	10	3-cell boxcar	0.37	0.23	11.85	0.26	-0.17
19	F I.C. diffusivities	$17 \times 17$	$10^{-5}$	1000	10	3-cell boxcar	0.70	0.41	13.24	0.24	-0.16
20	F I.C. diffusivities	$17 \times 17$	$10^{-5}$	2000	10	3-cell boxcar	1.06	0.66	14.52	0.21	-0.15
21	$v_{ref}$ I.C. noise	$17 \times 17$	$10^{-4}$	200	10	3-cell boxcar	0.11	0.09	12.25	0.29	-0.17
22	$v_{ref}$ I.C. noise	$17 \times 17$	$10^{-4}$	200	10	3-cell boxcar	0.21	0.17	11.34	0.30	-0.16
23	$v_{ref}$ I.C. noise	$17 \times 17$	$10^{-4}$	200	10	3-cell boxcar	0.07	0.04	11.70	0.29	-0.17
24	$v_{ref}$ I.C. noise	$17 \times 17$	$10^{-4}$	200	10	3-cell boxcar	0.08	0.05	11.59	0.29	-0.17
25	$v_{ref}$ I.C. noise	$17 \times 17$	$10^{-4}$	200	10	3-cell boxcar	0.08	0.06	11.66	0.28	-0.17
26	$v_{ref}$ I.C. noise	$17 \times 17$	$10^{-4}$	200	10	3-cell boxcar	0.23	0.13	11.93	0.31	-0.15
27	F I.C. smoothing	$17 \times 17$	$10^{-4}$	200	10	3-cell boxcar	0.06	0.04	11.37	0.29	-0.17
28	F I.C. smoothing	$17 \times 17$	$10^{-4}$	200	10	5-cell boxcar	0.09	0.06	11.38	0.29	-0.17
29	F I.C. smoothing	$17 \times 17$	$10^{-4}$	200	10	7-cell boxcar	0.09	0.06	11.46	0.29	-0.17
30	F I.C. smoothing	$17 \times 17$	$10^{-4}$	200	10	9-cell boxcar	0.08	0.05	11.36	0.29	-0.16
31	F I.C. smoothing	$17 \times 17$	$10^{-4}$	200	10	Mean of all cells	0.09	0.06	11.55	0.29	-0.17
32	$w$	$17 \times 17$	$10^{-4}$	200	1	3-cell boxcar	0.14	0.10	10.98	0.28	-0.15
33	$w$	$17 \times 17$	$10^{-4}$	200	10	3-cell boxcar	0.09	0.06	11.81	0.28	-0.17
34	$w$	$17 \times 17$	$10^{-4}$	200	20	3-cell boxcar	0.15	0.09	11.25	0.29	-0.15
35	$w$	$17 \times 17$	$10^{-4}$	200	50	3-cell boxcar	0.32	0.23	11.20	0.29	-0.14
36	$w$	$17 \times 17$	$10^{-4}$	200	100	3-cell boxcar	0.16	0.10	11.18	0.29	-0.15
37	$w$	$17 \times 17$	$10^{-4}$	200	200	3-cell boxcar	0.24	0.17	10.76	0.28	-0.15
38	$w$	$17 \times 17$	$10^{-4}$	200	500	3-cell boxcar	0.14	0.10	11.87	0.28	-0.18
39	$w$	$17 \times 17$	$10^{-4}$	200	1000	3-cell boxcar	0.25	0.20	12.91	0.28	-0.19

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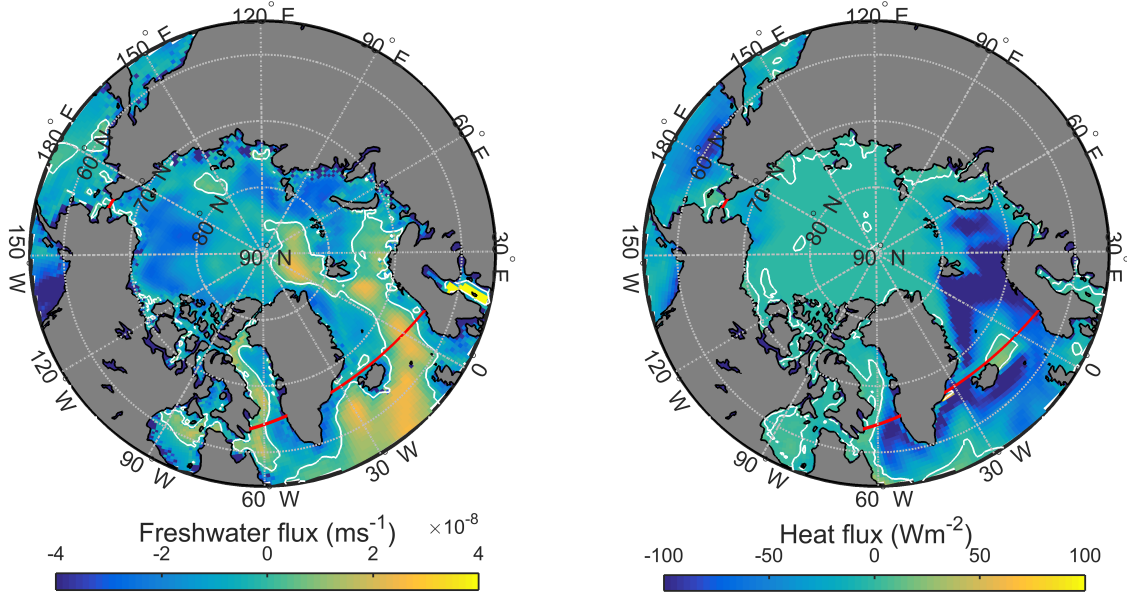


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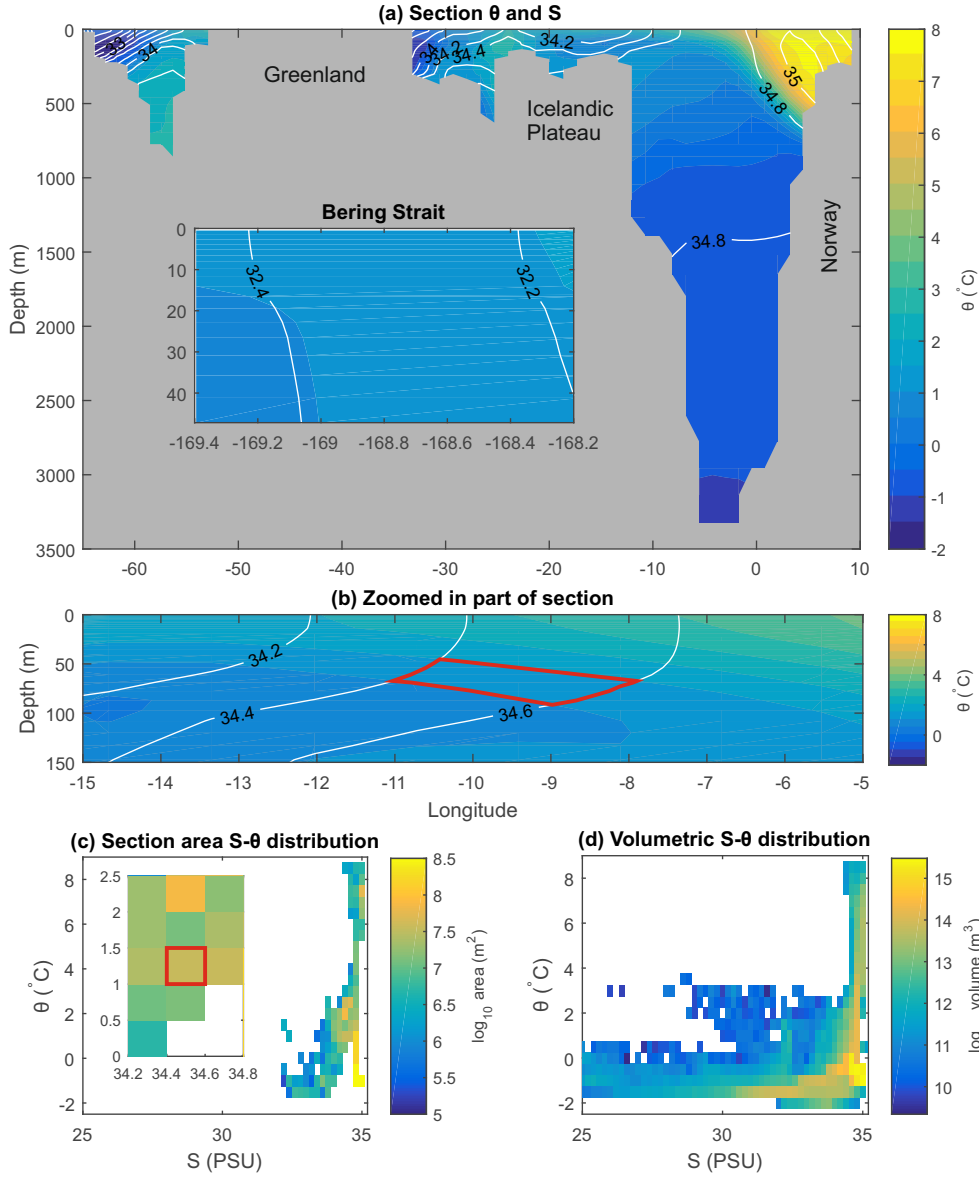
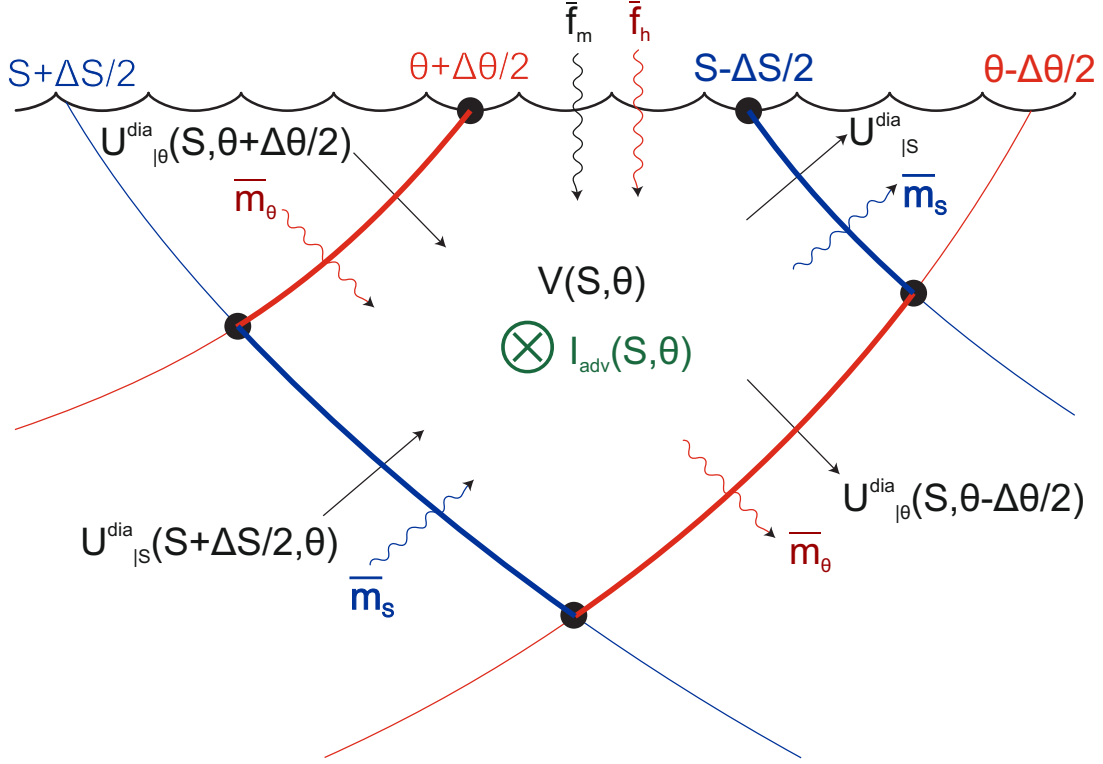


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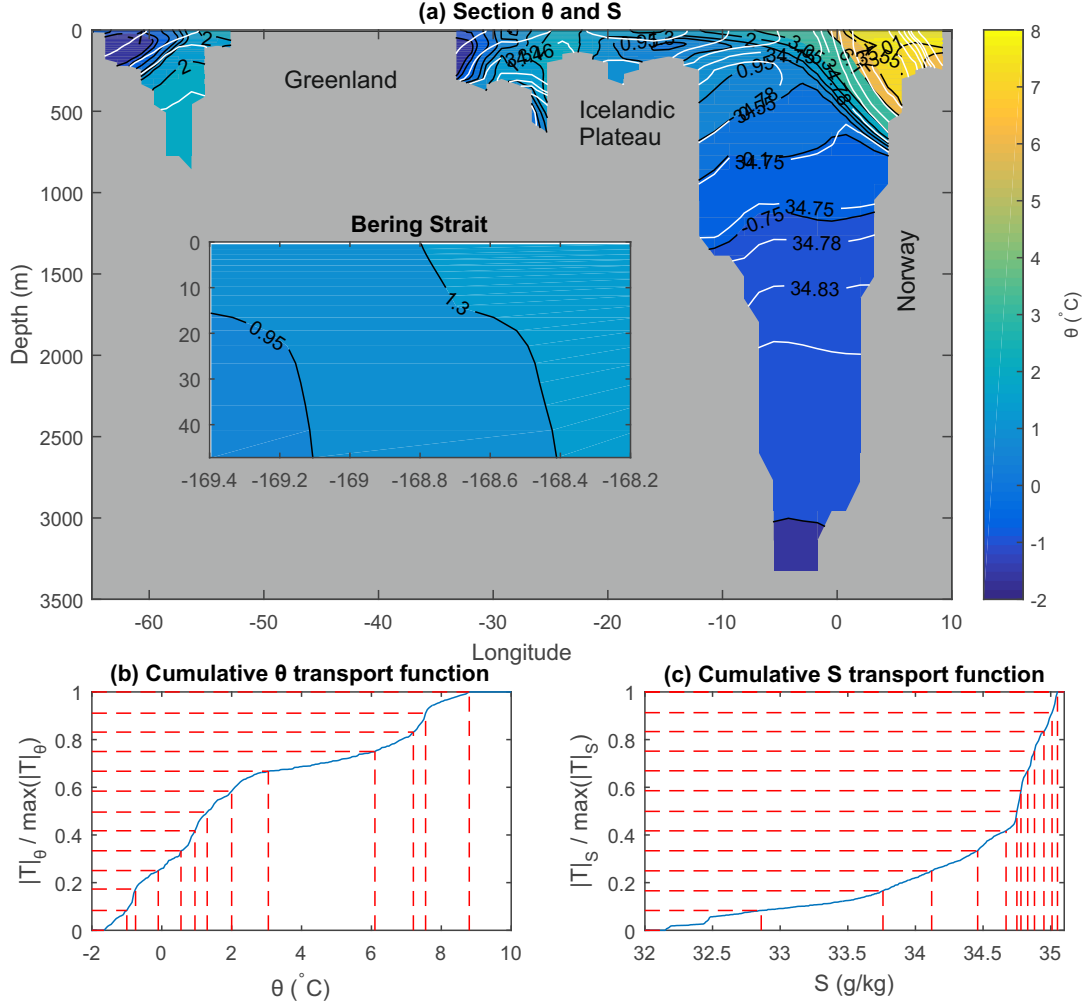


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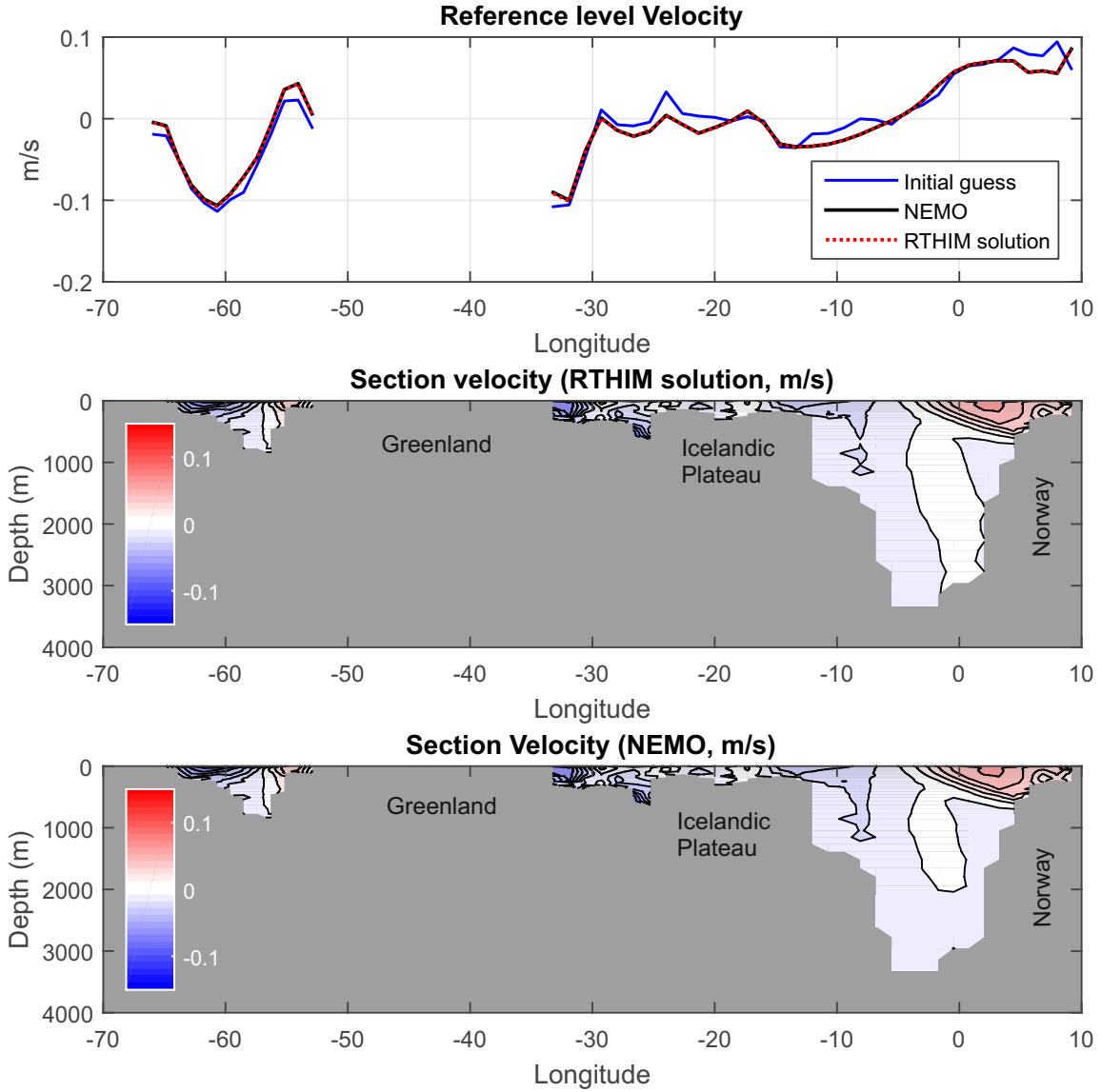


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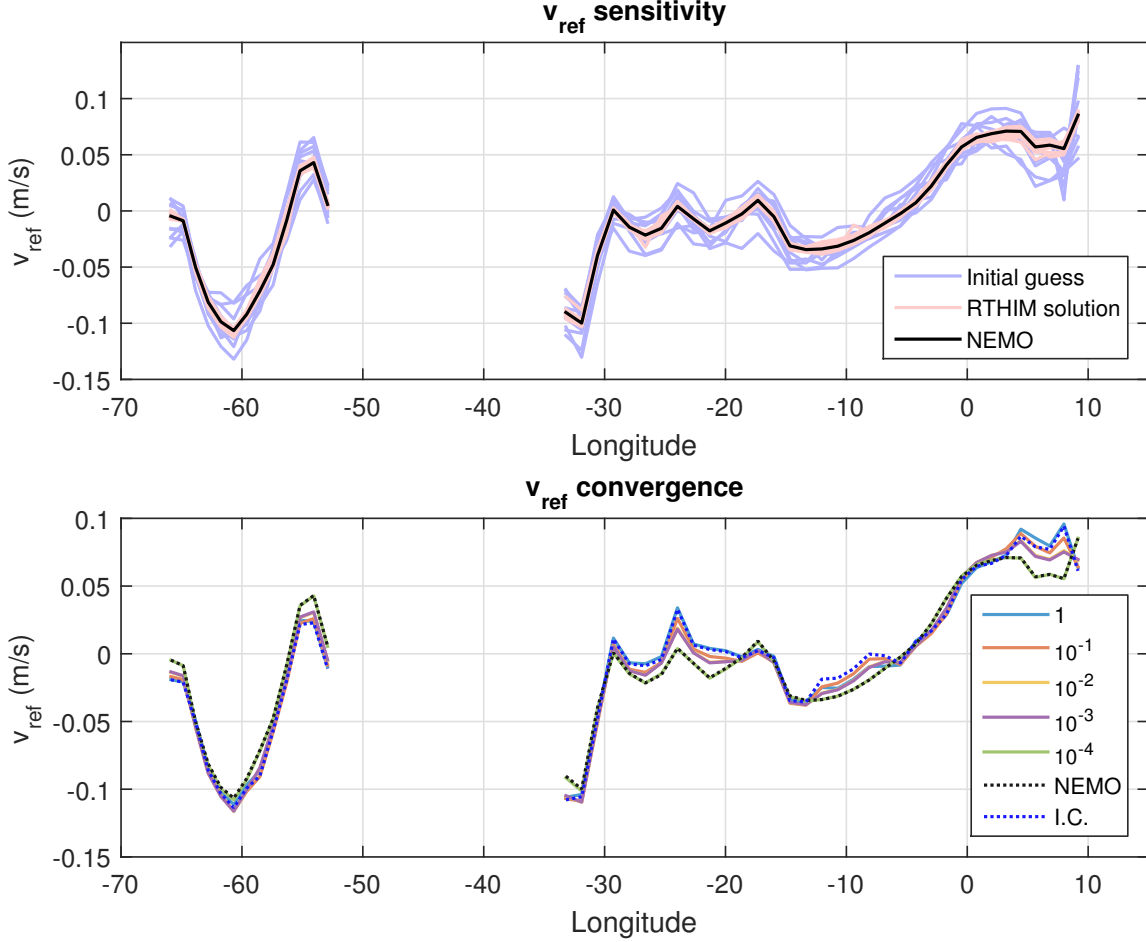


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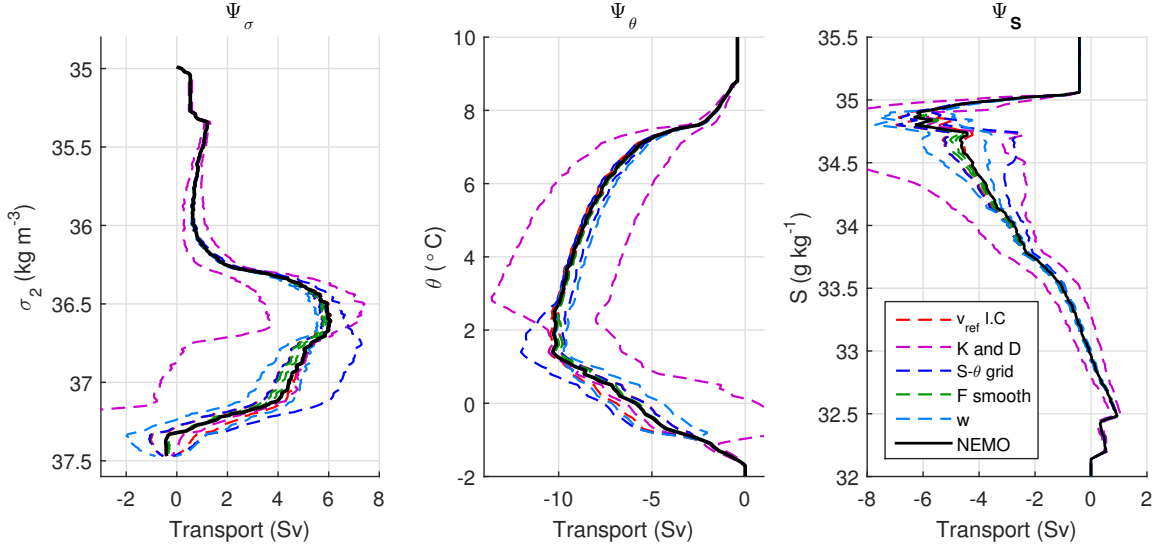


FIG. 7. Streamfunctions in  $\sigma$  (left),  $\theta$  (middle) and  $S$  (right) coordinates calculated from RTHIM solution section velocities from ensembles varying a range of parameters. The same-colored pairs of dashed lines give the upper and lower limits at each point on the y-axis of the streamfunctions for an ensemble. The parameters varied were the  $v_{ref}$  initial condition (red lines), the isopycnal and diapycnal mixing coefficients applied to the  $\mathbf{F}$  initial condition (purple lines), the  $S - \theta$  grid used for binning the terms in the volume budget (dark blue lines), the smoothing factor applied to the  $\mathbf{F}$  initial condition (green lines), and the weighting factor on the net transport constraint (light blue lines). The streamfunctions calculated from the NEMO section velocities are shown in black, and a black dotted zero line is also plotted for reference. Note that the x-axis ranges have been set to assist the reader in discerning details of the contributions of different parameters to the uncertainty, for which it is necessary not to include the full range of the  $K$  and  $D$  lines. Their full extent can be seen in the solid red lines on Fig. 8. For  $\Psi_\sigma$  the lower bounds have contributions from RTHIM runs runs 6, 12 and 13 detailed in Table 2 in the Appendix; the upper bounds have contributions from runs 2 and 13. For  $\Psi_\theta$  the lower bounds have contributions from runs 2 and 13; the upper bounds have contributions from runs 6, 11 and 13. For  $\Psi_S$  the lower bound comes from run 13 and the upper bound from run 5.



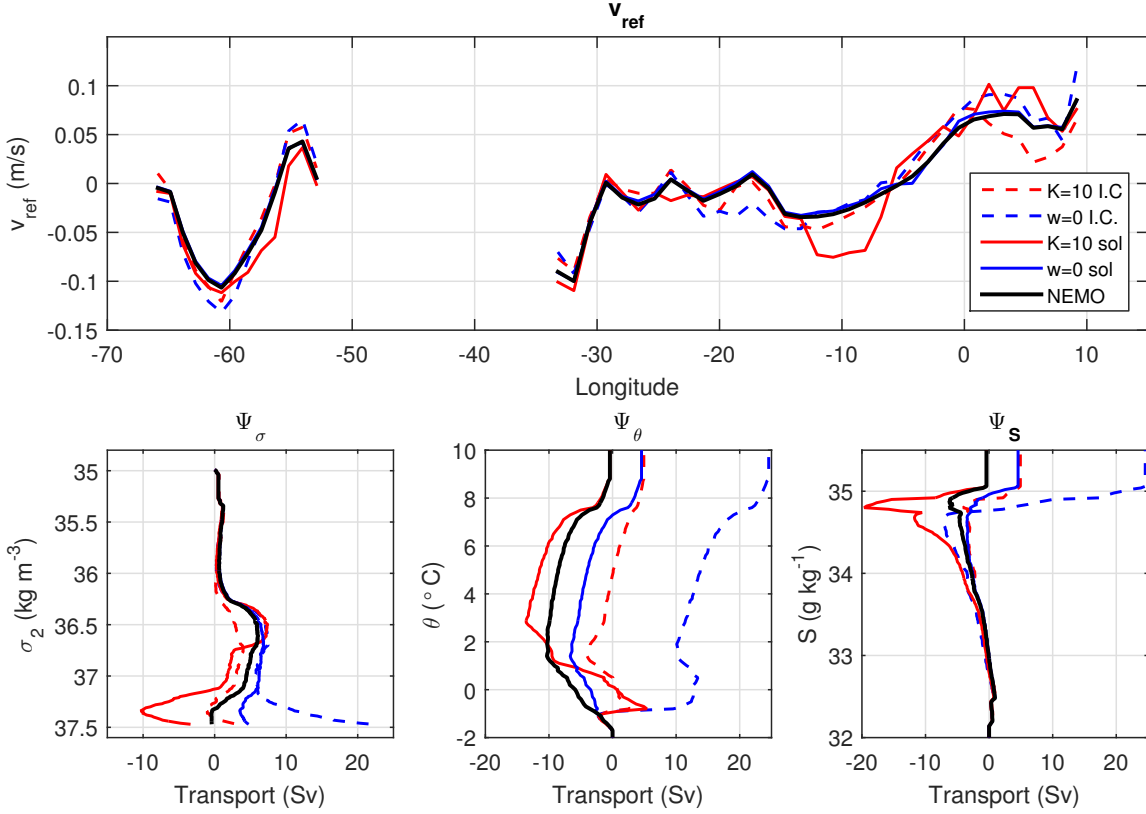


FIG. 8. Two RTHIM runs where the selection of model parameters has significantly degraded the solution. In red is the result of setting  $K = 10 \text{ m}^2\text{s}^{-1}$  in the calculation of the  $\mathbf{F}$  initial condition. In blue is the result of removing the net transport constraint. The top panel shows  $v_{ref}$  for the initial condition (dashed lines) and solution (solid lines) for each run. The bottom 3 panels show the streamfunctions in density (left), temperature (middle) and salinity (right) coordinates.

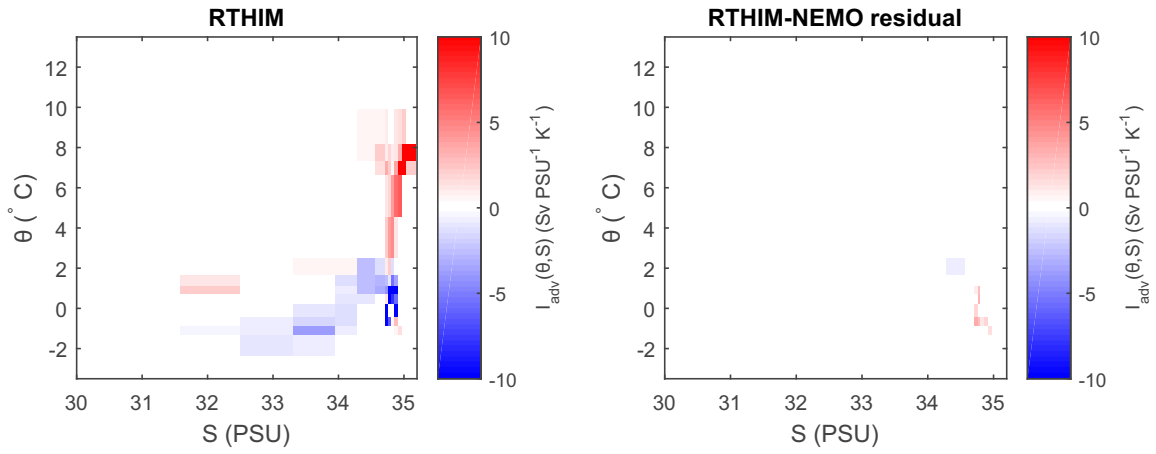


FIG. 9. The advection term  $I_{adv}$  plotted in  $S - \theta$  coordinates from an RTHIM solution (left panel) and the residual with the same term based on the NEMO section velocities (right panel).

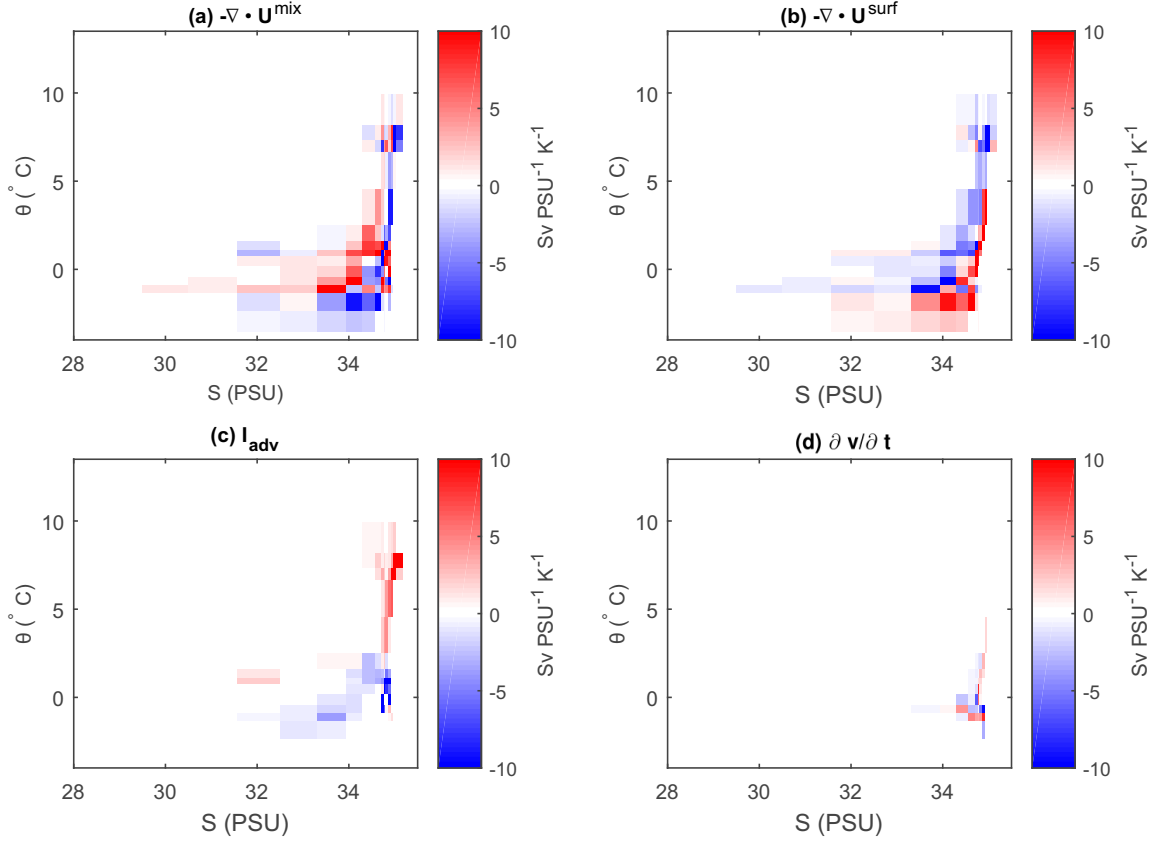


FIG. 10. Each term from the volume budget of Eq. 11, plotted in  $S-\theta$  coordinates, from an RTHIM solution. The terms are (a) the mixing term, (b) the surface flux term (c) the advection term and (d) the volume trend. Red colors indicate a net positive contribution to the volume of water in that  $(S, \theta)$  bin by a given process; blue colors indicate a net negative contribution.

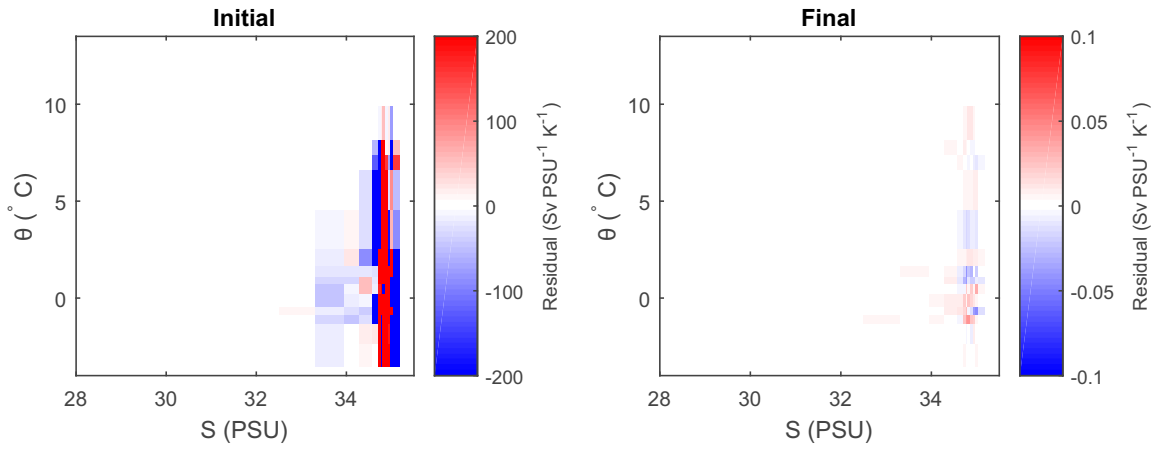


FIG. 11. The residual,  $\varepsilon$ , in the volume budget in  $S - \theta$  coordinates from the RTHIM initial condition (left) and after optimization (right). Note the different color scales.

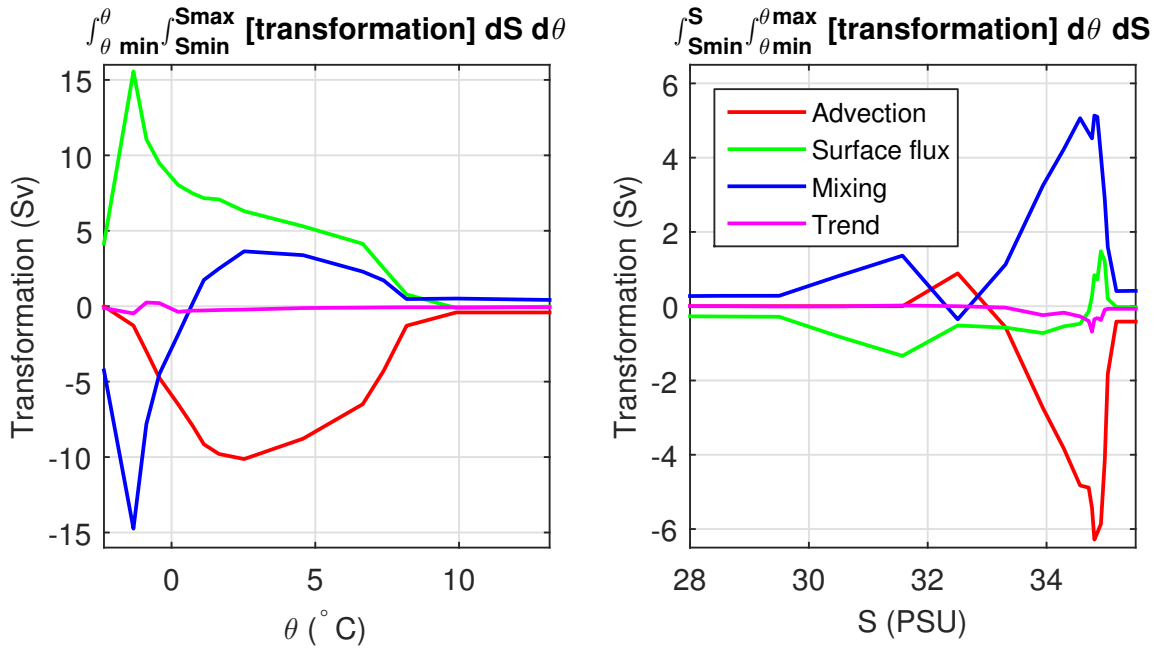
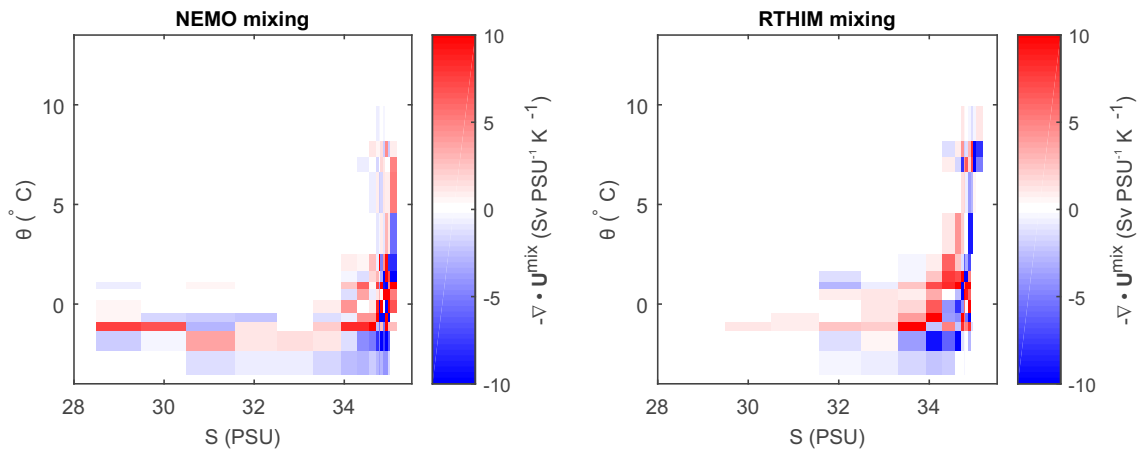


FIG. 12. Terms in the volume budget integrated in  $S-\theta$  space. On the left panel, each term has been integrated first through all  $S$  and then cumulatively in  $\theta$ , and plotted against  $\theta$ . On the right panel, each term has been integrated first through all  $\theta$  and then cumulatively in  $S$ , and plotted against  $S$ .



939 FIG. 13. Mixing terms diagnosed directly from NEMO tendencies (left panel) and from an RTHIM solution  
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 941 indicate a net negative contribution.

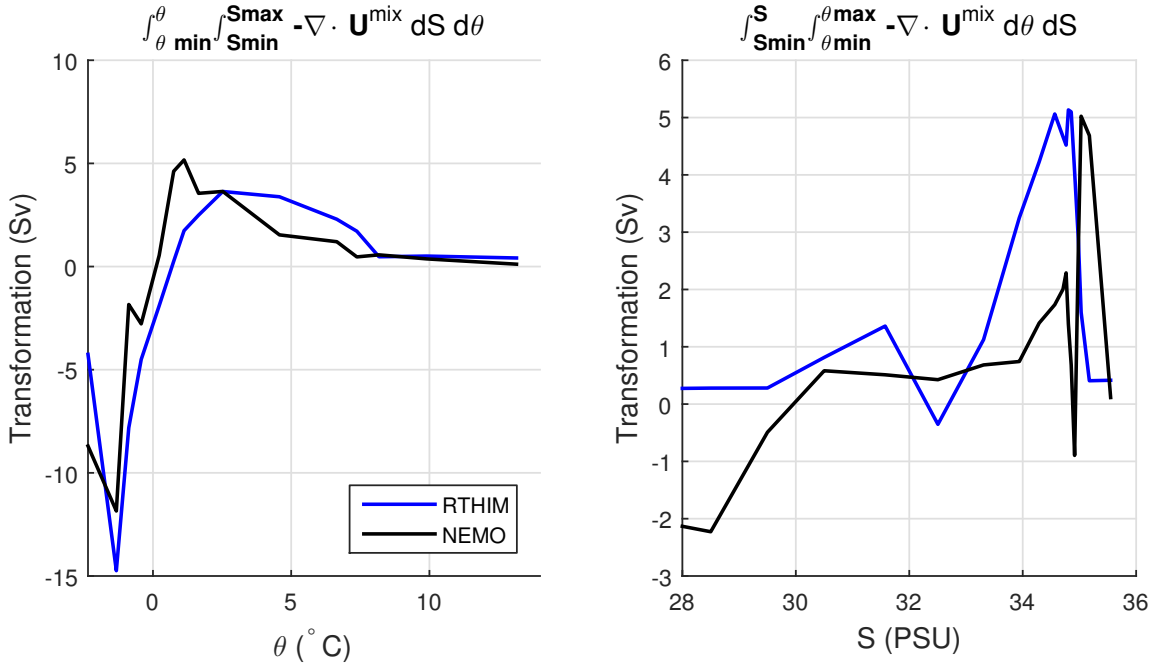


FIG. 14. Mixing terms from an RTHIM solution (blue line) and NEMO (black line) integrated in  $S-\theta$  space. On the left panel, each term has been integrated first through all  $S$  and then cumulatively in  $\theta$ , and plotted against  $\theta$ . On the right panel, each term has been integrated first through all  $\theta$  and then cumulatively in  $S$ , and plotted against  $S$ .