# On the Influence Chemical Defects and Structural Factors on Charge Transport and Failure in Polyethylene

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# **ABSTRACT**

A blend of high and low density polyethylene was aged at 160 °C in air and the impact of the chosen aging protocol on local chemistry, crystallinity and charge transport dynamics was considered. The aging conditions were chosen in order to exploit oxygen diffusion effects, such that the resulting systems could be considered as bi-layer specimens, containing two regions: a highly aged layer and a lightly aged layer, which vary in the concentrations of aging-related defects such as carbonyl groups and unsaturation. For aging periods up to 3 h, little space charge was found to accumulate within both the highly and lightly aged layers. However, after aging for about 3.5 h an abrupt change in behavior was observed, whereby charges move rapidly through the highly aged layer, accumulating at the interface with the lightly aged layer. Although sample-melting behavior, as determined by differential scanning calorimetry, was found to vary with aging time, we primarily associate this with retarded reorganization kinetics. As such, we suggest that this abrupt change in charge transport behavior is not structurally related but, rather, is a direct consequence of the local concentration of chemically related trapping sites exceeding some critical threshold. The consequence of the resulting space charge distribution is a dramatic increase in the local electric field across the lightly aged layer and a consequent reduction in the overall DC breakdown strength. However, while further aging exacerbates these space charge effects, counter to expectations, the breakdown strength then recovers somewhat, suggesting a change in the underlying mechanism of electrical failure.

Index Terms —polyethylene, aging, space charge, charge trapping, dielectric breakdown

#### 1 INTRODUCTION

THE topic of charge transport through disordered polymeric systems is of great scientific interest and technological importance. Scientifically, the issue has been addressed in a number of ways, including, theoretically, through simulation and by experiment. Early approaches to the evaluation of the band structure of polymers considered these as idealized infinite regular systems; in their 1971 paper, McAloon and Perkins [1], for example, contrasted the application of a linear combination of atomic orbitals molecular orbital (LCAO MO) approach with alternative published work and proposed a resulting band gap for polyethylene (PE) of around 19 eV, a value that is unreasonably large. The influence of the

theoretical approach on the calculated band gap of a single, infinite polymer chain was discussed in detail by Süle et al. [2], where band gap energies ranging from 4.4 eV to 9.7 eV were reported, depending on the methodology used. However, such an idealized structure differs greatly from the true nature of polymers and, as a result, the impact of structural factors attracted considerable interest, notably, through computational simulation approaches. The impact of local ordering on the electronic structure of PE has been considered and band gap energy values of 6.2 eV, 6.7 eV and 5.9 eV were reported for amorphous, crystalline and interfacial structures respectively [3]. In addition to structural disorder, chemical factors also serve to create localized energy states (traps) near the band edges; an early study of the effect of carbonyl groups on the electronic properties of an oligomeric PE analogue suggested that the carbonyl group led to the formation of trap states at a depth of ~0.45 eV [4]. Elsewhere, Wang et al. [5] considered the impact of a range of different chemical moieties (hydroxyl carbonyl and unsaturation) on the electronic structure of another oligomeric PE. This work indicated that the energy gap between the highest occupied and lowest unoccupied molecular orbitals was significantly reduced to 5.35 eV in the case of their chosen conjugated structure.

Chemical species such as those described above are produced in PE as a result of degradation/aging. At elevated temperatures, chain scission results in the generation of free radicals, which may subsequently take part in a range of reactions. In the presence of oxygen, the formation of hydroperoxides is of particular importance, in that they can decompose, leading to branching reactions, further radical production [6] and the formation of ketones, esters, carboxylic acids and aldehydes [7]. Furthermore, Chabira *et al.* [8] related vinyl group production in LDPE to the decomposition of ketones; the further reaction of such species can then facilitate crosslinking in PE at temperatures above the melting transition [9].

From the above account, it is evident that the products of degradation in polymers markedly modify the band structure of such systems and, consequently, the effect of this on the characteristics of technologically insulation systems has been addressed. While macroscopic electrical degradation features, such as electrical trees, are reasonably well-understood, this is not the case for precursor phenomena, where a number of different processes have been suggested to lead to the modification of the material at the nanoscopic level. These include: chain scission at electric fields >20 kV/mm and consequent formation of submicrocavities causing local accumulation of space charge [10]; charge recombination and consequent electroluminescence leading to local degradation through photo-oxidation [11]; field-induced mechanical stress and consequent propagating cracking associated with breaking of inter-lamellar tie chains [12].

Nevertheless, whatever the precise mechanisms, while it is accepted that changes in local chemistry and microstructure are closely linked to modified electrical properties [13], the details are not fully understood. The work described here considers the effect of a specifically chosen aging protocol on the chemistry, lamellar texture and charge transport dynamics in a designed PE blend. The aging conditions were specifically chosen such that the local degradation reactions were kinetically controlled by oxygen diffusion into the system [14]. The rationale behind the choice of a PE blend stems from the ability to generate a wide range of different morphologies in a single system, while retaining a constant molecular composition [15]. Consequently, by varying the precise thermal history imposed on the system it is possible to position the chemical products of degradation at different locations within the system, on both the macroscopic and microscopic levels. Here, we focus on the former, where the specimen production route was chosen to provide as a simple morphology as possible [15]. The effect of varying the morphology and the microscopic distribution of degradation products within it will be reported elsewhere.

# 2 EXPERIMENTAL

#### 2.1 SAMPLE PREPARATION

All samples were composed of a PE blend containing 20 wt.% of high density PE (HDPE: HD5813EA, BP Chemicals) plus 80 wt.% of low density PE (LDPE: LD100BW, Exxon Mobil), which was prepared by mixing the constituent components for 20 min at 160 °C in a HAAKE Polylab twin rotor R600 mixer. The required samples, with a nominal thickness of 0.2 mm, were then prepared by melt-pressing between sheets of polyethylene terephthalate (PET), before being quenched into distilled water [15].

Thermal aging was performed in a fan oven (Heraeus, Kendro Laboratory Products UT6) at 160 °C for various ageing times from 1 to 6 h. These conditions were determined from initial scoping experiments, in which treatment temperatures from 120 °C to 160 °C and treatment times from 30 min to 24 h were explored. During the aging process, each film was placed with its lower surface in contact with a PET substrate and its upper surface exposed to air, in order to produce specimens where the extent of aging varied through the thickness. Hereafter, the upper, more affected surface/layer is referred to as the highly aged surface/layer, while the lower less affected surface/layer is termed the lightly aged surface/layer. After aging, all samples were again quenched directly into distilled water, in order to generate as simple a lamellar morphology as possible.

# 2.2 MOLECULAR CHARACTERIZATION

The spatial variation of aging-induced chemical changes was determined by confocal Raman microprobe spectroscopy. To prepare the required sample cross-sections, the aged film of interest was sandwiched between two sheets of a styrene, ethylene/butylene, styrene triblock copolymer (KRATON G1650), which had previously been softened through exposure to toluene. After evaporation of the toluene, the resulting layered sample was microtomed at -40 °C using an RMC MT7, CR-21 cryo-ultramicrotome. Raman analysis was then performed using a Renishaw RM1000 system with a Renishaw NIR 780TF diode laser (wavelength 780 nm and maximum output power of 25 mW). Data were acquired with a x50 objective lens and with the laser power set at 50%, from 500 cm<sup>-1</sup> to 3200 cm<sup>-1</sup>, using 10 consecutive 10 s extended scans. The resulting data were processed to remove background scattering and normalized with respect to the Raman peak at 1295 cm<sup>-1</sup> (C-C twisting mode) [16]. Carbonyl index (CI) values were determined using:

$$CI = \frac{A_c}{A_{ref}}$$
 (1)

where  $A_c$  and  $A_{ref}$  are, respectively, the areas under the peaks at 1720 cm<sup>-1</sup> (C=O stretching) and around 2850 cm<sup>-1</sup> (CH<sub>2</sub> and CH<sub>3</sub> symmetric and asymmetric stretching).

Complementary spectral data were obtained from highly aged surfaces using attenuated total internal reflectance (ATR) Fourier transform infrared spectroscopy (FTIR). For this, a Thermo Scientific Nicolet iS5 FT-IR spectrometer with iD7 ATR diamond crystal plates was used; all spectra were obtained over the wavenumber range 400-4000 cm<sup>-1</sup> and, for each spectrum, 16 scans were averaged with 4 cm<sup>-1</sup> resolution.

While the above approaches provide information on the effect of aging at the functional group level, they do not readily reveal changes in molecular topology. As such, gel content measurements were also conducted using xylene extraction at 140 °C for 6 h, in accordance with ASTM D2765-01. The gel content was calculated as the ratio of the dried insoluble residue to the initial sample mass (typically, ~0.3 g).

#### 2.3 MORPHOLOGY

Different scanning calorimetry (DSC) (Perkin Elmer DSC 7, running Pyris software) was used to determine the melting behavior of each specimen. All experiments were performed after calibration of the DSC with high-purity indium; all sample melting data were acquired from 40 °C to 170 °C at a scan rate of 10 °C/min. Subsequent data analysis was conducted using the Origin 2018 software package.

#### 2.4 ELECTRICAL PROPERTIES

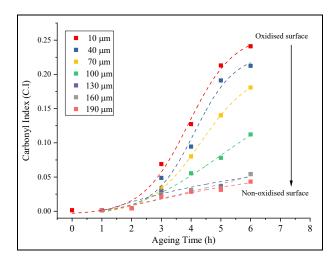
Electrical properties were determined at room temperature (20 °C) using the following techniques. The accumulation and dissipation of space charge (SC) was examined using the pulsed electro-acoustic (PEA) method, using a semiconducting composite anode (held at high voltage) and an aluminum cathode (at ground potential). For this, an applied voltage of 8 kV was chosen and data were, first, acquired for 3600 s with the field applied (voltage-on) and, subsequently, with the sample short-circuited (voltage-off). In view of the inherent asymmetry in the aged samples, experiments were performed with the highly aged surface in contact with the anode and with the highly aged surface in contact with the cathode.

DC breakdown strength was measured according to ASTM D3755-14. For this, the sample was immersed in silicone oil between spherical electrodes, 6.3 mm in diameter, and the applied voltage increased at a rate of 350 V/s. Breakdown voltage and sample thickness data were collected from twenty breakdown sites per sample and the resulting breakdown fields were analyzed assuming two parameter Weibull statistics with 90 % confidence bounds, using the Origin 2018 software.

# **3 RESULTS**

# 3.1 AGING-INDUCED PHYSICOCHEMICAL CHANGES

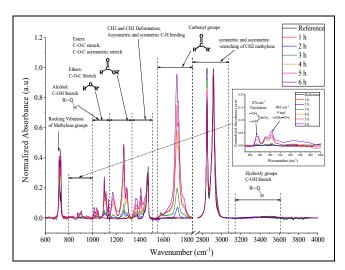
Figure 1 shows the effect of the chosen aging regime on the time evolution of CI at different locations with the samples. Carbonyl formation occurs through chain scission followed by reaction with available oxygen [7, 14] and, therefore, CI is used here as a simple proxy for the extent of aging. Consider, first, the data obtained at 130-190 µm below the uppermost



**Figure 1.** Confocal Raman data presented in the form of carbonyl index as a function of aging time at different positions within sample cross-sections.

highly aged surface, where CI increases progressively with aging time. Conversely, at depths from zero to 100 µm, the Raman data evince a marked increase in the rate of oxidation beyond an induction period of 2-3 h. Thus, initially, aging in air at 160 °C for times up to 2 h has relatively little effect on the measured carbonyl index at any point within the specimens which, we suggest, is related to local consumption of the included antioxidant [6], as described by Winslow et al. [17]. Thereafter, for aging times beyond 2 h, the observed position dependent increase in the CI value is associated with the local degree of autoxidation, which is driven primarily by the availability of oxygen at each location within the sample. Audouin et al. [14] described this in terms of diffusion-limited effects, whereby an oxidized "layer" is formed of approximate thickness  $(D/k)^{0.5}$ , where D is the diffusion coefficient and k is the pseudo-first-order reaction rate constant for oxygen consumption. In summary, aging occurs non-uniformly throughout the sample and, as described above, can be considered in terms of a highly aged layer which, from Figure 1, ranges from the uppermost sample surface to a depth of ~130 μm. Below this, the material is relatively lightly aged.

Figure 2 shows complementary data obtained by FTIR from the uppermost highly aged surface of samples aged for different times. These show that the strength of carbonylrelated absorption bands, including ketones and carboxylic acids (at 1716 cm<sup>-1</sup>), esters and aldehyde (at 1725 cm<sup>-1</sup>) and  $\gamma$ lactone (at 1780 cm<sup>-1</sup>), increase significantly with aging time beyond 2 h. As such, these data mirror the above Raman data. While the use of CI as a general proxy for extent of aging is not unreasonable, it does fail to recognize all of the products of thermal treatment. Indeed, Figure 2 shows the presence of esters (1170, 1264 and 1289 cm<sup>-1</sup>), ethers (1112 and 1134 cm<sup>-1</sup>) alcohols (1012 and 1046 cm<sup>-1</sup>), vinyl groups (vinylidenes at 874 cm<sup>-1</sup>, vinyls at 903 cm<sup>-1</sup>) and hydroxyl groups (over 3,000-3,600 cm<sup>-1</sup>) [8, 18]. On aging for more than 2 h, the intensity of the majority of these bands increase significantly, while the intensity of absorption bands related to hydroxyl groups (over 3,000-3,600 cm<sup>-1</sup>) remains close to



**Figure 2.** The IR spectra obtained from the highly aged surface of the samples with respect to the variation of aging times from 0 to 6 h.

constant. While variations in the carbonyl group concentration can, as above, be used as a chemical indicator of extent of aging, Chabira *et al.* [8] have suggested that vinyl groups can be used as complementary chemical indicators of chain scission processes. Specifically, these workers have associated the formation of vinylidenes to β-scission of branched (tertiary) alkyls abstracted from tertiary carbon in PE chains, while vinyl groups arise from Norrish type II-scission of ketones [8, 18]. Additionally, Johnston *et al.* [9] reported that cross-linking becomes the dominant process in place of chain scission when polyethylene experiences high degrees of oxidative degradation at a high temperature; for this reason, gel fraction measurements were undertaken.

Figure 3 shows the effect of aging time on gel content. Up to 2 h aging time, negligible gel was formed while, beyond this, the measured gel content increased progressively, in a comparable manner to the changes seen in CI within the highly aged layer. Crosslinking during the thermo-oxidative aging of polyethylene was described by Ranby and Rabek [19] and related to reactions between alkoxy radicals (R-CO•-R) or between alkoxy and alkyl radicals, leading to the formation of esters and ethers respectively. As such, the existence of strong IR absorbance in the ester and ether regions for samples aged beyond 2 h may be associated with such crosslinking processes. Elsewhere, it has been suggested that crosslinks may also form through the linkage of alkyl radicals (R-•CH<sub>2</sub>-R; secondary and tertiary alkyls) or vinyl groups and alkyl radicals [18]. The presence of vinylidenes and vinyl groups indicates that such processes are viable here, while their low concentration may be a consequence of their consumption through crosslinking [8, 18].

In summary, data shown above present a consistent picture of the effects of the chosen aging conditions, which include the formation of molecular defects ranging from discrete chemical species to modified molecular topologies. Specifically, the extent of degradation varies through the cross-section of the aged samples, which can be considered to consist to highly aged and lightly aged layers.

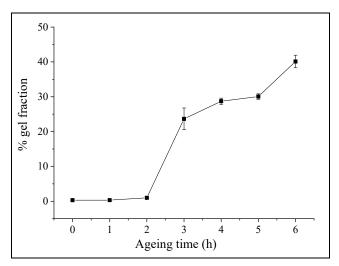
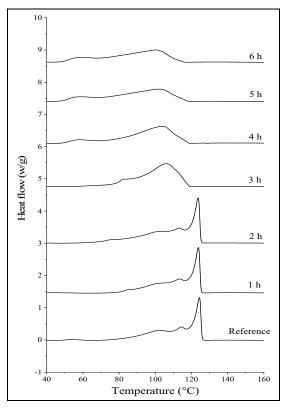


Figure 3. The percentage of crosslinks in the samples with the variation of aging times.

#### 3.2 STRUCTURAL CONSEQUENCE OF AGING

The aging-related changes described above can be considered as introducing molecular defects into the system, which could affect its ability to crystallize. Figure 4 presents DSC data obtained from samples aged for the times indicated. From this, it is evident that, for aging times of 2 h and below, quenching of the blend system considered here results in the formation of a lamellar population which, on heating in the DSC, exhibits a broad melting endotherm that spans the range



**Figure 4.** DSC melting traces of the samples with the variation of aging times from 0 to 6 h.

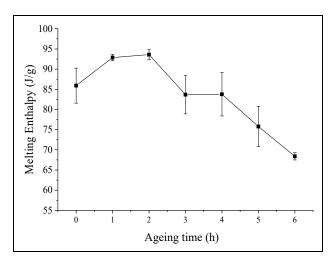


Figure 5. Variation in total melting peak enthalpy with aging.

from 60 °C to 125 °C and which contains a number of features. First, there is a well-defined peak (maximum at ~124 °C), which results from the melting of a lamellar population composed principally of HDPE. The location of this peak is a consequence of a fraction of the initially formed lamellar population, coupled with subsequent thickening during the course of the DSC scan itself [20]. The next feature in the melting behavior (minor peak, maximum at ~115 °C) results from co-crystallization of HDPE and the more linear molecular sequences from within the LDPE; as a consequence of the latter, annealing during the DSC scan is suppressed, hence the intermediate location. Finally, the broad melting transition that extends down in temperature to ~60 °C is associated with the melting of crystals formed from the remnant, more highly branched LDPE fraction [15].

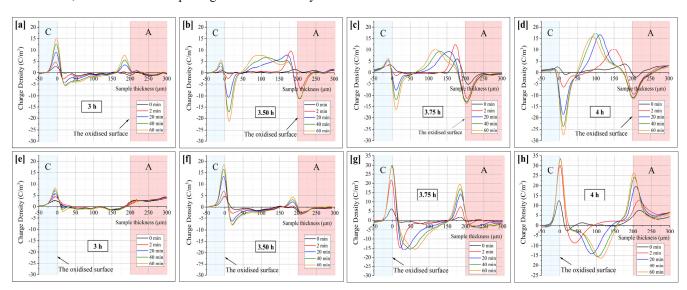
Aging for 3 h dramatically changes the melting endotherm, which now spans the temperature range 60-120 °C and differs in form from that observed following shorter aging times. From above, it is clear that samples aged for 3 h and beyond

contain a higher concentration of aging-induced chemical defects and a gel fraction, compared with less aged specimens. While it is tempting to associate changes in melting behavior with aging-induced defects acting to reduce sample crystallinity, the data presented in Figure 5 show that samples aged for up to 4 h are all characterized by comparable melting enthalpy values. As such, we interpret the marked difference in the form of the melting endotherm exhibited by samples aged for 2 h and 3 h as being a consequence of the latter system crystallizing within the constraints of a cross-linked network, which markedly limits dynamic reorganization during the DSC heating scan [21].

From Figure 5, it would appear that the molecular changes that result from aging within the induction period lead to a slight increase in crystallinity whereas, during autoxidation, they serve to broaden the melting endotherm to lower temperatures and, progressively, reduce crystallinity. This behavior is consistent with a number of studies of thermal aging effects in PE [22], where it has been related to the recrystallization of segments of abstracted and disordered PE chains in amorphous regions. The subsequent reduction in crystallinity is then a consequence of an increasing concentration of molecular defects, which are excluded on thermodynamic groups from lamellar crystals, such that the melting endotherm is broadened and displaced to lower temperatures and the overall melting enthalpy is reduced.

# 3.3 AGING AND CHARGE TRAPPING

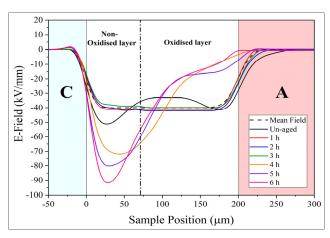
Elsewhere [23], we have presented a general overview of aging and space charge accumulation in a quenched HDPE/LDPE and, therefore, we will focus here on specimens aged from 3 h to 4 h, where dramatic changes occur. For the traces presented in Figure 6, the charge on the electrodes has been subtracted from the raw data in order better to reveal the space charge within the polyethylene and the consequent induced charges on the electrodes. From Figure 6a it is clear



**Figure 6.** Charge accumulation profiles (voltage-on) obtained from samples aged for between 3 h and 4 h with the highly aged surface in contact with: (a-d) the semiconducting composite high voltage anode (A) and (e-h) the aluminum earth potential cathode (C).

that little space charge accumulates within the bulk of the sample aged for 3 h, space charge profiles indicating the accumulation of a small amount of negative homocharge within the lightly aged layer of the specimen adjacent to the cathode (to the left of the plots). This occurs in spite of the molecular changes revealed above that occur on aging for periods up to 3 h. In contrast, the data presented in Figure 6b reveal that after aging for 3.5 h, positive charge is injected from the anode (to the right of the plots) and, over a period of about 40 min, moves progressively through the sample towards the cathode. Further aging results in an increase in the density of space charge and more rapid movement (see Figures 6b – 6d). Data obtained with the sample geometry reversed are presented in Figures 6e to 6h; that is, with the more highly aged surface adjacent to the cathode (to the left of the plots). Again, in the sample aged for 3 h, only a relatively small amount of homocharge is evident within the lightly aged layer within the specimen; after 3.5 h of aging, negative homocharge can be seen to be injected from the cathode into the highly aged layer, where it is trapped locally. Increasing the aging time by just 15 min serves dramatically to increase both the amount of negative injected space charge and its rate of movement through the highly aged layer towards the anode.

While data obtained with the two sample configurations are broadly comparable, Figures 6 indicates that the transition from the accumulation of a small quantity of homocharge within the lightly aged layer to the injection and propagation of large amounts of charge through the highly aged layer is displaced to longer times when the highly aged surface is in contact with the aluminum cathode. Multiple experimental repeats showed this to be reproducible and, therefore, we suggest that it is a genuine effect that is related either to the nature of the dominant charge carrier under different polarities, or associated with differences in charge injection/extraction from the semiconducting composite (SC) anode and an aluminum (Al) cathode. Such effects have been addressed in a number of studies. Wang et al. [24] used density functional theory (DFT) to demonstrate that positive charge injection and accumulation are dominated by the low



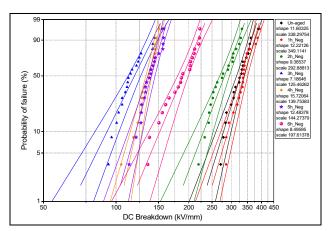
**Figure 7.** Spatial variation in electric field through the sample thickness as a consequence of accumulated space charge. Anode in contact with the highly aged surface.

hole injection barrier in LDPE, compared with electron injection. Chen, et al [25], studied the effects of electrode material and polarity on space charge formation in polyethylene and showed that the use of a semiconducting composite electrode leads to increased charge injection and space charge accumulation in polyethylene, compared to an Al electrode. This effect was reported to be independent of the applied polarity, suggesting that the nature of the charge carrier is less important than the interfacial potential barrier for injection. The results presented in Figure 6 indicate the early onset of positive charge injection from the semiconducting composite anode and, as such, are consistent with both the theoretical and experimental studies described above.

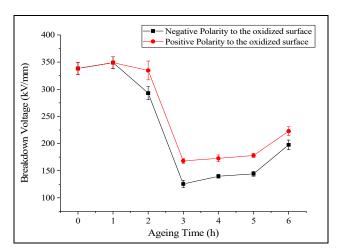
# 3.4 AGING, CHARGE TRANSPORT AND BREAKDOWN

The accumulation of space charge within a dielectric directly affects the distribution of the electric field within the system and, therefore, this issue was considered for the case of the anode in contact with the highly aged surface; the results are shown in Figure 7. In the unaged sample, heterocharge accumulation adjacent to the cathode results in a local increase in the local electric field at this location to about 50 kV mm<sup>-1</sup>. In the case of samples aged for up to 3 h, the replacement of this heterocharge with the small amount of homocharge seen in Figure 6, leads to the maximum local electric field determined from the space charge plots being constant at 37-41 kV mm<sup>-1</sup>. This is quantitative as expected for the Laplacian fields in the case of a parallel-sided sample, ~200 µm in thickness when subjected to an applied voltage of 8 kV. However, in the case of the sample aged for 4 h, the marked change in the space charge profile discussed above results in a highly non-uniform field distribution within the specimen, such that the electric field is strongly intensified within the lightly aged layer, whereby the maximum value exceeds 90 kV mm<sup>-1</sup>.

Figure 8 shows DC breakdown data presented in the form of Weibull plots obtained with the high voltage in contact with



**Figure 8.** Weibull plot for the dielectric breakdown strength of the reference sample and aged samples in case of the highly aged surface in contact with the cathode.



**Figure 9.** Plots comparing the DC breakdown strength of the reference sample and the aged samples with the highly aged surface in contact with the anode and cathode electrodes.

the highly aged surface, while Figure 9 summarizes such behavior in terms of the derived Weibull scale parameter,  $\alpha_{ta}$ , where ta indicates the aging time in hours. First, comparison of the data sets obtained with the anode and the cathode in contact with the highly aged surface reveals that the change in experimental geometry, beyond ageing times of just 1 h, results in significantly reduced breakdown strength values with the latter arrangement. While this asymmetry parallels the different ageing times required for the onset of extensive space charge accumulation seen in Figure 6, it is intuitive why the geometry corresponding to suppressed space charge accumulation leads to consistently reduced values of  $\alpha_{ta}$ . Furthermore, from Figure 9, it is evident that both data sets can, broadly, be considered in terms of two regimes, which are characterized by very different breakdown strength values. For example, compare the results obtained with the anode in contact with the highly aged surface after 2 h and 4 h of aging, where  $\alpha_2$  equates to 335  $\pm$  17 kV/mm and  $\alpha_4$  = 173  $\pm$  6 kV/mm. That is, the latter value is only about 50% of the former. From Figure 7, the peak internal field within the specimen, based upon the space charge profiles acquired with 8 kV applied across samples nominally 200 µm in thickness with the anode in contact with the aged surface, is 42 kV/mm in the sample aged for 2 h and 72 kV/mm in the sample aged for 4 h - a field intensification of some 58%. While these two metrics are broadly consistent, a more detailed analysis indicates that the variation in breakdown strength seen in Figure 9 is not solely attributable to space charge effects.

Consider samples aged for between 3 h and 6 h and, as above, consider data acquired with the highly aged surfaces in contact with the anode. From Figure 7, the peak internal field based upon the PEA data rises monotonically from 40 kV/mm to 92 kV/mm with increasing aging time. In parallel, from Figure 9, the overall measured breakdown strength *increases* from  $\alpha_3 = 168 \pm 5$  kV/mm to  $\alpha_6 = 223 \pm 8$  kV/mm despite the marked field intensification deduced from the space charge profiles.

While it could be argued that is inappropriate to compare the PEA and breakdown two data sets too closely, in view of the different voltages and durations used in the two experimental set-ups, we nevertheless would argue that the behavior reported is worthy of collective discussion. For example, in the case of the specimens aged for 3 - 4 h, the duration of a breakdown experiment is ~100 s; from the data presented in Figure 6, little space charge accumulates within the specimen in these less heavily aged specimens. Conversely, in the sample aged for 6 h, space charge accumulates rapidly [23] and would therefore be expected to promote breakdown, which not what is seen. The implication of this is therefore that the measured breakdown strength is not dominated by the accumulated space charge but, rather, results from a combination of space charge effects and variations in material properties. In this regard, it is worth returning at this point to Figure 3 and 5; from the former, the gel content increases with increased aging times in the range 3 - 6 h while overall crystallinity decreases. This implies that in the systems considered here, which were deliberately prepared so as to suppress extensive lamellar development, morphology per se is of little importance in determining breakdown strength, whereas possible variations in mechanical properties that result from the presence of an increasing gel fraction may be significant. Indeed, optical examination of failure regions in samples aged from 3 - 6 h was highly suggestive of mechanically-related variations in the final failure. The role of morphology will be reported in due course, where different thermal histories are used to produce, structurally, very different systems.

# 4 CONCLUSIONS

The work described above reports on effects of aging on structural and electrical factors in PE, where the spatial distribution of ageing-induced moieties has been controlled by exploiting diffusion-limited oxidation process such that the resulting specimens can be considered in terms of highly and lightly aged layers. For aging times up to 2 h at 160 °C, analysis by confocal Raman spectroscopy, FTIR spectroscopy, DSC and the measurement of gel content, reveals few material changes, which we attribute to the stabilizing effect of the included antioxidant. Within this ageing regime, minimal space charge accumulation occurs and the measured DC breakdown strength remains close to that measured for the unaged system. Beyond about 3 h, the chemical and structural consequence of aging increase progressively monotonically, as represented by indicators such as carbonyl index, gel content and crystallinity. In contrast, abrupt and marked changes in space charge behavior were seen. These are consistent with space charge limited conduction (SSLC) effects, whereby low concentrations of chemical changes equate to a relatively low density of deep traps while, beyond some threshold, the increased density of comparable moieties serves to facilitate rapid migration of space charge through the highly aged layer, resulting in intensification of the local field within the lightly aged layer. However, quantitative comparison of the degree of field intensification and the measured breakdown strength indicate poor agreement. Indeed, for aging times beyond 3 h under the conditions described here, increases in DC breakdown strength with increasing ageing times can be observed in samples where field intensification from space charge is increasingly severe. As such, we suggest that breakdown in such specimens cannot be solely related to space charge effects and related field intensification, but suggest that, in parallel, certain aspects of the aging process are serving to reinforce the material, leading to the observed increases in breakdown strength with increased degrees of aging.

#### **ACKNOWLEDGMENT**

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