## UNIVERSITY OF SOUTHAMPTON

# Simultaneous Confidence Bands For Linear And Logistic Regression Models

by

## Shan Lin

A thesis submitted in partial fulfillment for the degree of Doctor of Philosophy

in the

Faculty of Engineering, Science and Mathematics School of Mathematics

July 2007

## UNIVERSITY OF SOUTHAMPTON FACULTY OF ENGINEERING, SCIENCE AND MATHEMATICS SCHOOL OF MATHEMATICS

Doctor of Philosophy

## SIMULTANEOUS CONFIDENCE BANDS FOR LINEAR AND LOGISTIC REGRESSION MODELS

by

Shan Lin

#### ABSTRACT

This thesis considers the construction of simultaneous confidence bands for a normal-error linear regression model and a linear logistic regression model with a binary response variable respectively. For linear regression, three general methods are summarized to construct exact one-sided and twosided confidence bands over an ellipsoidal restricted region of the predictor space, and they are found to have the equivalent formulae for calculating critical values. Also, several methods are available to construct confidence bands over a rectangular region. We compare these methods in terms of the critical value. For logistic regression, several methods are considered for the construction of confidence bands with or without predictor constraint, which is based on the asymptotic normality of the estimator. Simulation studies are provided to assess the performances of some key bands. Several useful conclusions can be drawn.

i

# Contents

ł

Intr	oduct	ion	1
1.1	Backg	round	1
1.2	The o	rganization of this thesis	9
1.3	Conce	pts and basic tools	10
Ger	neralize	ed linear models and logistic regression model with	
bina	ary da	ta	12 <sup>°</sup>
2.1	Introd	luction	12
2.2	Model	specification	13
	2.2.1	Generalized linear models	13
	2.2.2	Binary response and logistic regression model $\ldots$ .	14
2.3	Paran	neter estimation	16
2.4	Asym	ptotic behavior of estimators	20
	2.4.1	Introduction	20
	2.4.2	The first type of asymptotic $\ldots \ldots \ldots \ldots \ldots \ldots$	22
	2.4.3	The second type of asymptotic	30
2.5	Goodr	ness of fit statistics	31
	2.5.1	Deviance	31
	2.5.2	Pearson chi-squared statistic	32
	2.5.3	Equivalence	33
2.6	Sampl	ing distributions of statistics	33
2.7	Residu	ıal analysis	35
	Intr 1.1 1.2 1.3 Ger bina 2.1 2.2 2.3 2.4 2.5 2.6 2.7	Introduct 1.1 Backg 1.2 The o 1.3 Concernation Generalized binary dat 2.1 Introd 2.2 Model 2.2.1 2.2 2 2.3 Param 2.4 Asymp 2.4.1 2.4.2 2.4.3 2.5 Goodn 2.5.1 2.5.2 2.5.3 2.6 Sampl 2.7 Reside	Introduction         1.1       Background         1.2       The organization of this thesis         1.3       Concepts and basic tools         1.3       Concepts and basic tools         Generalized linear models and logistic regression model with         binary data         2.1       Introduction         2.2       Model specification         2.2.1       Generalized linear models         2.2.2       Binary response and logistic regression model         2.3       Parameter estimation         2.4       Asymptotic behavior of estimators         2.4.1       Introduction         2.4.2       The first type of asymptotic         2.4.3       The second type of asymptotic         2.5.4       Goodness of fit statistics         2.5.2       Pearson chi-squared statistic         2.5.3       Equivalence         2.6       Sampling distributions of statistics         2.7       Residual analysis

3	Exa	Exact simultaneous confidence bands for a simple linear re-			
	gre	ssion v	with restricted predictor variable	37	
	3.1	Exact	one-sided confidence bands $\ldots \ldots \ldots \ldots \ldots \ldots$	37	
		3.1.1	Method following the idea of Bohrer $(1973)$	39	
		3.1.2	Algebraical method	42	
		3.1.3	Tubular neighborhood method	44	
		3.1.4	Equivalence of the formulae $\ldots \ldots \ldots \ldots \ldots \ldots$	46	
	3.2	Exact	two-sided confidence bands $\hdots$	48	
		3.2.1	Method following the idea of Bohrer $(1973)$	49	
		3.2.2	Algebraical method	50	
		3.2.3	Tubular neighborhood method	51	
		3.2.4	Equivalence of the formulae $\ldots \ldots \ldots \ldots \ldots \ldots$	53	
Δ	Event simultaneous confidence bands for a multiple linear				
т	regression over an ellipsoidal region			55	
	4 1	Exact	one-sided confidence hands	55	
	1.1	411	Method of Bohrer (1973)	58	
		4.1.2	Algebraical method	62	
		4.1.3	Tubular neighborhood method	65	
		414	Equivalence of the formulae	66	
	4.2	Exact	two-sided confidence bands	68	
		4.2.1	Method following the idea of Bohrer (1973)	68	
		4.2.2	Algebraical method	70	
,		4.2.3	Tubular neighborhood method	71	
		4.2.4	Equivalence of the formulae	73	
_	<b>a</b> .				
5	Sim	ultane	ous contidence bands for a regression model over a		
	rectangular region and comparisons			75	
	5.1	Conse	rvative confidence bands	76	
	5.2	Appro	ximate confidence bands	80	
	5.3	Simula	ation-based confidence bands for a polynomial regression	82	

i

β

	5.4	Simulation-based confidence bands for a multiple linear regres-		
		sion		
	5.5	Comp	arisons	
		5.5.1	For simple linear regression	
		5.5.2	For polynomial regression of various orders 100	
		5.5.3	For bivariate linear regression	
		5.5.4	Conclusions	
	5.6	Nume	rical examples	
		5.6.1	Example for simple linear regression	
		5.6.2	Example for polynomial regression	
		5.6.3	Example for bivariate linear regression	
_	a	17		
6	Sim	ultane	ous confidence bands for a logistic regression model 128	
	6.1	Conne	lence bands for a logistic regression without constraint	
		on pre	dictor variables	
		6.1.1	For a simple logistic regression	
		6.1.2	For a multiple logistic regression	
	6.2	Confid	lence bands for a logistic regression with restricted pre-	
		dictor	variables	
		6.2.1	For a simple logistic regression	
		6.2.2	For a multiple logistic regression	
	6.3	Simula	ations	
		6.3.1	For one-dimensional case	
		6.3.2	For two-dimensional case	
		6.3.3	Conclusions	
7	Con	clusio	ns and future work 161	
-	7.1	Conclu	isions	
		7.1.1	For linear regression	
		7.1.2	For logistic regression	
	7.2	Future	e work	

3

,

Α	Cod	Codes for computing the critical value and simulated cover-		
	age	probal	bility	165
	A.1	For co	mputing the critical value for linear regression	. 165
		A.1.1	Obtaining $c$ , using the exact method for simple linear	
			regression	. 165
		A.1.2	Obtaining $c$ , using the approximate method for simple	
			linear regression	. 167
		A.1.3	Obtaining $c$ , using the simulation-based method for	
			simple linear regression	. 168
		A.1.4	Obtaining $c$ , using Naiman's method for polynomial	
			regression	. 169
		A.1.5	Obtaining $c$ , using the approximate method for poly-	
			nomial regression	. 172
		A.1.6	Obtaining $c$ , using the simulation-based method for	
			polynomial regression	. 174
		A.1.7	Obtaining $c$ , using the approximate method for bivari-	
			ate linear regression	. 183
	A.2	For co	mputing the simulated coverage probability for logistic	
		regress	sion	. 188
		A.2.1	Obtaining $scp$ , using the WB method for simple logistic	
			regression	. 188
		A.2.2	Obtaining <i>scp</i> of Type 4 band for simple logistic re-	
			gression, using parfit on S-plus	. 191
		A.2.3	Obtaining <i>scp</i> , using the simulation-based method for	
			bivariate logistic regression	. 193

ŧ

References

# List of Figures

1.1	Simultaneous and individual confidence statements 4
1.2	Confidence band for a simple linear regression 6
1.3	Confidence band for a bivariate linear regression 6
3.1	For the method following Bohrer (1973) in one-sided case 40 $$
3.2	For the algebraical method in one-sided case
3.3	For the tubular neighborhood method in one-sided case $45$
3.4	Picture obtained by rotating the coordinates system 47
3.5	For the method following Bohrer (1973) in two-sided case $49$
3.6	For the tubular neighborhood method in two-sided case 52 $$
4.1	For the method of Bohrer (1973) 60
4.2	For the algebraical method in one-sided case 63
4.3	For the tubular neighborhood method in one-sided case $66$
4.4	For the method following Bohrer (1973) in two-sided case 69
4.5	For the tubular neighborhood method in two-sided case 72
5.1	Tubular neighborhood of a path
5.2	The cone determined by three angles
5.3	Confidence bands for 90% confidence level $\ldots \ldots \ldots \ldots \ldots 120$
5.4	Confidence bands for 95% confidence level
5.5	Confidence bands for 99% confidence level
5.6	Confidence bands for 90% confidence level $\ldots \ldots \ldots \ldots \ldots \ldots 122$
5.7	Confidence bands for 95% confidence level
5.8	The approximate band for 90% confidence level

5.9	The approximate band for 95% confidence level $\ . \ . \ . \ . \ .$ . 126
5.10	The simulation-based band for 90% confidence level 126
5.11	The simulation-based band for 95% confidence level 127
6.1	For Wynn and Bloomfield's method
6.2	95%-level confidence bands for probability of deaths 140
6.3	90%-level confidence band for probability of that ESR larger
	than 20
6.4	95%-level confidence band for probability of that ESR larger
	than 20

í

# List of Tables

1.1	Observations for simple linear regression model 5
5.1	Critical values for simple linear regression
5.2	Critical values for simple linear regression
5.3	Critical values for simple linear regression
5.4	Critical values for simple linear regression
5.5	Critical values for simple linear regression
5.6	Critical values for simple linear regression
5.7	Critical values for simple linear regression
5.8	Critical values for simple linear regression
5.9	Critical values for simple linear regression
5.10	Critical values for simple linear regression
5.11	Critical values for quadratic regression
5.12	Critical values for cubic regression
5.13	Critical values for 4th order polynomial regression 108
5.14	Critical values for quadratic regression
5.15	Critical values for cubic regression
5.16	Critical values for 4th order polynomial regression 111 $$
5.17	Critical values for bivariate linear regression
5.18	Critical values for bivariate linear regression
5.19	Forbes' 1857 data on boiling point and barometric pressure
	for 17 locations in the Alps and Scotland $\ldots \ldots \ldots \ldots \ldots \ldots \ldots 119$
5.20	Hardwood concentration in pulp and tensile strength of kraft
	paper

÷

5.21	Delivery time data for bivariate example		
6.1	Number of deaths to different doses of serum		
6.2	Squared critical values for 95% confidence level $\ldots \ldots \ldots 141$		
6.3	The levels of two plasma proteins and the value of a binary		
	response that denotes whether ESR ${\geq}20$ for each individual 143		
6.4	Designs for predictor variable and restricted interval 147		
6.5	Design for total sample size		
6.6	Designs for true regression coefficients		
6.7	Simulated coverage probabilities for $95\%$ confidence level $\ .$ 149		
6.8	Simulated coverage probabilities for 95% confidence level $\ .\ .\ .$ 150		
6.9	Simulated coverage probabilities for $95\%$ confidence level $\ .$ 151		
6.10	Simulated coverage probabilities for $95\%$ confidence level $\ . \ . \ . \ 152$		
6.11	Design points for two predictor variables		
6.12	Designs for restricted intervals of predictor variables $153$		
6.13	Designs for total sample size		
6.14	Designs for true regression coefficients		
6.15	Simulated coverage probabilities for two-dimensional case 156 $$		
6.16	Simulated coverage probabilities for two-dimensional case $157$		
6.17	Simulated coverage probabilities for two-dimensional case 158 $$		
6.18	Simulated coverage probabilities for two-dimensional case 159 $$		

ć

.

### Acknowledgements

I wish to thank Professor Wei Liu very much for providing many valuable ideas and kind supervision, from which I have greatly benefited during my PhD period. Also, the staff in School of Mathematics gave me lots of timely help which drove me to move forward. I would like to thank them as well. Moreover, I got much concern and encouragement from my wife and our parents, who made me feel and enjoy the wonderful life outside the absolutely boring studies. So this thesis is to them, and additionally to my unborn daughter - Peiyao Lin.

> Shan Lin University of Southampton July 2007

# Chapter 1

## Introduction

## 1.1 Background

Consider the classical normal-error linear regression model

$$\mathbf{Y} = X\boldsymbol{\beta} + \boldsymbol{\varepsilon}$$

where  $\mathbf{Y}_{n\times 1}$  is the vector of the observed responses,  $X_{n\times p}$  is the design matrix with the first column given by  $(1, \ldots, 1)^T$  and the *j*th  $(2 \leq j \leq p)$  column given by  $(x_{1,j}, \ldots, x_{n,j})^T$ ,  $\boldsymbol{\beta} = (\beta_1, \ldots, \beta_p)^T$  is the vector of regression coefficients, and  $\boldsymbol{\varepsilon}$  is the error vector which has the  $N_n(\mathbf{0}, \sigma^2 I)$  distribution with  $\sigma^2$  unknown. Assume  $X^T X$  is non-singular, then the least squares estimator of  $\boldsymbol{\beta}$  is given by  $\hat{\boldsymbol{\beta}} = (X^T X)^{-1} X^T \mathbf{Y}$  which has the  $N_p(\boldsymbol{\beta}, \sigma^2 (X^T X)^{-1})$  distribution. Let  $\hat{\sigma}^2$  denote the usual unbiased estimator of  $\sigma^2$ , then  $\hat{\sigma}^2 \sim \sigma^2 \chi_{\nu}^2 / \nu$ with the degree of freedom  $\nu = n - p$  and is independent of  $\hat{\boldsymbol{\beta}}$ .

For statistical inference, the commonly considered pointwise confidence interval plays an important role which is concerned for the mean response  $\mathbf{x}_0^T \boldsymbol{\beta}$  at one specific point  $\mathbf{x}_0$ . It has the form given by

$$\mathbf{x}_{0}^{T}\boldsymbol{\beta} \in \mathbf{x}_{0}^{T}\hat{\boldsymbol{\beta}} \pm t_{\nu,1-\alpha/2}\hat{\sigma}\sqrt{\mathbf{x}_{0}^{T}(\boldsymbol{X}^{T}\boldsymbol{X})^{-1}\mathbf{x}_{0}},$$
(1.1)

where  $t_{\nu,1-\alpha/2}$  is the percentage point of a t random variable with  $\nu$  degrees of freedom that leaves a probability  $\alpha/2$  in the upper tail, and so  $1 - \alpha/2$  in the lower tail.

A simultaneous confidence band is constructed for the mean responses  $\mathbf{x}^T \boldsymbol{\beta}$  for all possible values of  $\mathbf{x}$  within a given region  $\mathcal{X}$  of p-1 predictor variables. The most popular simultaneous confidence band is of hyperbolic shape, and has the following form

$$\mathbf{x}^{T}\boldsymbol{\beta} \in \mathbf{x}^{T}\hat{\boldsymbol{\beta}} \pm c\hat{\sigma}\sqrt{\mathbf{x}^{T}(X^{T}X)^{-1}\mathbf{x}}$$
 for all  $\mathbf{x} \in \mathcal{X}$ , (1.2)

where c is the critical value such that the confidence band has the simultaneous coverage probability equal to a preassigned confidence level  $1 - \alpha$ . The key of constructing a confidence band is to find the appropriate critical value c. Another frequently mentioned confidence band is of fixed band width, which has the form given by

$$\mathbf{x}^T \boldsymbol{\beta} \in \mathbf{x}^T \hat{\boldsymbol{\beta}} \pm c \hat{\sigma} \quad \text{for all } \mathbf{x} \in \mathcal{X}.$$
 (1.3)

It is of natural interest to compare the simultaneous confidence band with the pointwise confidence interval. The key difference between them is that the simultaneous confidence band is constructed for all possible  $\mathbf{x}$  while the pointwise confidence interval is only at a specific point  $\mathbf{x}_0$ .

On the other hand, consider a confidence interval for the parameter vector  $\beta$ , which is given by

$$\boldsymbol{\beta} \in \hat{\boldsymbol{\beta}} \pm t_{\nu,1-\alpha/2} \text{s.e.}(\hat{\boldsymbol{\beta}}), \tag{1.4}$$

where s.e. $(\hat{\beta})$  is the standard error of  $\hat{\beta}$  and is formed by the square roots of the diagonal terms of the matrix  $\hat{\sigma}^2 (X^T X)^{-1}$ . The confidence interval for  $\beta$  contains p individual confidence intervals for p regression coefficients respectively. And these individual intervals can be used to define a rectangular region in the parameter space. Note that this rectangular region is not a proper simultaneous confidence region for  $\beta$ .

To obtain a simultaneous confidence region for  $\beta$ , we start with the fact that  $\hat{\beta} \sim N_p(\beta, \sigma^2(X^T X)^{-1})$ . Define a  $p \times p$  non-singular matrix P such that

 $P^T P = (X^T X)^{-1}$ . Then we have

$$(P^{-1})^{T}(\hat{\boldsymbol{\beta}} - \boldsymbol{\beta})/\sigma \sim N_{p}(0, \boldsymbol{I})$$

$$\Rightarrow \quad (\hat{\boldsymbol{\beta}} - \boldsymbol{\beta})^{T}(P^{T}P)^{-1}(\hat{\boldsymbol{\beta}} - \boldsymbol{\beta})/\sigma^{2} \sim \chi_{p}^{2}$$

$$\Rightarrow \quad \frac{(\hat{\boldsymbol{\beta}} - \boldsymbol{\beta})^{T}X^{T}X(\hat{\boldsymbol{\beta}} - \boldsymbol{\beta})/p\sigma^{2}}{\hat{\sigma}^{2}/\sigma^{2}} \sim F_{p,\nu}, \quad (1.5)$$

where  $\chi_p^2$  and  $F_{p,\nu}$  denote the Chi-square distribution with p degrees of freedom and the F distribution with p and  $\nu$  degrees of freedom. Therefore, a  $(1 - \alpha)$ -level simultaneous confidence region for  $\beta$  can be obtained from the inequality

$$(\boldsymbol{\beta} - \hat{\boldsymbol{\beta}})^T X^T X (\boldsymbol{\beta} - \hat{\boldsymbol{\beta}}) \le p \hat{\sigma}^2 F_{p,\nu,1-\alpha}, \qquad (1.6)$$

where  $F_{p,\nu,1-\alpha}$  is the upper  $\alpha$  point of the  $F_{p,\nu}$  distribution. The equality obtained by changing " $\leq$ " to "=" in (1.6) specifies the boundary of an ellipsoidal contour in the parameter space.

Note that the simultaneous confidence region for  $\beta$  in (1.6) can also be obtained from the simultaneous confidence band for  $\mathbf{x}^T \beta$  in (1.2) when  $\mathcal{X} = \mathcal{R}^{p-1}$  which is the setting in Scheffé (1953). Assume the band (1.2) has  $1 - \alpha$ confidence level. Then we have

$$P\{\mathbf{x}^{T}\boldsymbol{\beta}\in\mathbf{x}^{T}\hat{\boldsymbol{\beta}}\pm c\hat{\sigma}\sqrt{\mathbf{x}^{T}(\boldsymbol{X}^{T}\boldsymbol{X})^{-1}\mathbf{x}},\mathbf{x}\in\mathcal{R}^{p-1}\}=1-\alpha.$$
 (1.7)

With P consistently defined, we have the probability on the left-hand side of (1.7) further equal to

$$P\{\sup_{\mathbf{x}\in\mathcal{R}^{p-1}} |\mathbf{x}^{T}(\boldsymbol{\beta}-\hat{\boldsymbol{\beta}})| \leq c\hat{\sigma}\sqrt{\mathbf{x}^{T}(X^{T}X)^{-1}\mathbf{x}}\}$$

$$= P\{\sup_{\mathbf{x}\in\mathcal{R}^{p-1}} |\mathbf{x}^{T}P^{T}(P^{-1})^{T}(\boldsymbol{\beta}-\hat{\boldsymbol{\beta}})| \leq c\hat{\sigma}\sqrt{\mathbf{x}^{T}P^{T}P\mathbf{x}}\}$$

$$= P\{\sup_{\mathbf{x}\in\mathcal{R}^{p-1}} |(P\mathbf{x})^{T} \cdot (P^{-1})^{T}(\boldsymbol{\beta}-\hat{\boldsymbol{\beta}})| \leq c\hat{\sigma}\sqrt{(P\mathbf{x})^{T}(P\mathbf{x})}\}$$

$$= P\{||P\mathbf{x}|| \cdot ||(P^{-1})^{T}(\boldsymbol{\beta}-\hat{\boldsymbol{\beta}})|| \leq c\hat{\sigma}||P\mathbf{x}||\}$$

$$= P\{[(P^{-1})^{T}(\boldsymbol{\beta}-\hat{\boldsymbol{\beta}})]^{T}[(P^{-1})^{T}(\boldsymbol{\beta}-\hat{\boldsymbol{\beta}})] \leq c^{2}\hat{\sigma}^{2}\}$$

$$= P\{(\boldsymbol{\beta}-\hat{\boldsymbol{\beta}})^{T}(P^{T}P)^{-1}(\boldsymbol{\beta}-\hat{\boldsymbol{\beta}}) \leq c^{2}\hat{\sigma}^{2}\}$$

$$= P\{(\boldsymbol{\beta}-\hat{\boldsymbol{\beta}})^{T}X^{T}X(\boldsymbol{\beta}-\hat{\boldsymbol{\beta}}) \leq c^{2}\hat{\sigma}^{2}\} = 1 - \alpha. \quad (1.8)$$



Figure 1.1: Simultaneous and individual confidence statements.

Therefore  $c^2 = pF_{p,\nu,1-\alpha}$ , and the link between (1.2) and (1.6) is obtained. For all  $\mathbf{x} \in \mathbb{R}^{p-1}$ , any point within the simultaneous confidence region for  $\beta$  in (1.6) one-to-one corresponds to a straight line which is completely inside the simultaneous confidence band for  $\mathbf{x}^T \boldsymbol{\beta}$  in (1.2).

Figure 1.1 indicates a possible situation that may arise when p = 2. The  $(1 - \alpha)$ -level simultaneous confidence region for  $(\beta_0, \beta_1)$  is displayed by the shin ellipse which encloses points of  $(\beta_0, \beta_1)$  that are considered as simultaneously appropriate for the true parameters. The individual  $(1 - \alpha)$ -level confidence intervals for  $\beta_0$  and  $\beta_1$  specify the ranges for the candidates of the true parameters separately irrespective with the value of the other parameter. Both ellipse and the rectangular region are centered at the point of the estimates of the two parameters  $(\hat{\beta}_0, \hat{\beta}_1)$ . Note that a point, for example, E lying inside the rectangular region but outside the ellipse illustrates that the coordinates of the point E are regarded as reasonable for parameters  $\beta_0$  and  $\beta_1$  by the individual confidence intervals but not so by the simultaneous confidence region. For details, see, e.g., Draper and Smith (1998, pages 142-146). This thesis focuses on the construction of hyperbolic-shape simultaneous confidence bands rather than bands of other shapes or pointwise confidence intervals.

1	x <sub>i</sub>	Уi
1	1.9	0.7
2	0.8	-1.0
3	1.1	-0.2
4	0.1	-1.2
5	-0,1	-0.1
6	4.4	3:4
7	4.6	0:0
8	1:6	0:8
9	5.5	3,7
10	3.4	2.0

Table 1.1: Observations for simple linear regression model

Next, we come to see two examples of constructing simultaneous confidence bands for a linear regression model. The first example is of one dimension, where we have 10 observations for the only predictor variable xand the response y respectively. These observations are given in Table 1.1. We fit this data using a simple linear regression model and construct a simultaneous confidence band over the restricted interval [-0.1, 5.5] with 95% confidence level. The critical value of the confidence band is 2.9201 compared with the critical value 2.3060 for the 95%-level pointwise confidence interval. The confidence band constructed is shown in Figure 1.2.

The second example is for two-dimensional case. Consider the acetylene data of Snee (1977) which was very popular in published papers and can be fitted by a bivariate linear regression model. We construct the 95%-level simultaneous confidence band over  $\mathcal{X} = [1100, 1300] \times [5.3, 23]$  and then picture it in Figure 1.3. The critical value of the confidence band is 3.1137 while that of the pointwise confidence interval is 2.1604.

A simultaneous confidence band provides useful information on whereabouts of the true regression function. Any regression function which lies completely inside the confidence band over the whole given region of the predictor variables is deemed by the band as a plausible candidate of the true function; any regression function that lies outside the confidence band for at least one point in the given region of the predictor space is not considered as



Figure 1.2: Confidence band for a simple linear regression



Figure 1.3: Confidence band for a bivariate linear regression

a potential candidate of the true function.

Specifically, a simultaneous confidence band can be used to test the following hypotheses

$$H_0: \beta = \beta_0$$
 against  $H_a: \beta \neq \beta_0$ 

in the following way

reject 
$$H_0$$
 if and only if  
 $\mathbf{x}^T \boldsymbol{\beta}_0$  is outside the band for at least one  $\mathbf{x} \in \mathcal{X}$ . (1.9)

This test is of size  $\alpha$  since the confidence band has a simultaneous confidence level  $1 - \alpha$ .

The problem of constructing simultaneous confidence bands has a history going back to Working and Hotelling (1929). Scheffé (1953) considered the whole predictor space as the given region of predictor variables which is equivalent to setting no constraint at all on predictor variables.

For p = 2, that is, there is only one predictor variable, Gafarian (1964) considered a two-sided constant-width confidence band with the only predictor variable restricted in an interval. His effort was followed by Bowden (1970) who considered two-sided confidence bands of other shapes by making use of Hölder's inequality. Piegorsch *et al.* (2000) considered the calculation of the critical values of a family of confidence bands from Bowden (1970). Wynn and Bloomfield (1971) and Uusipaikka (1983) provided exact two-sided hyperbolic-shape confidence bands, with the band width proportional to the standard error of the estimated regression function, when the only predictor variable is restricted in an interval or the union of disjoint intervals. Bohrer and Francis (1972) proposed exact one-sided confidence bands with the only predictor variable constrained to an interval.

For p > 2, there are at least two predictor variables in the model. In such a case, the (p-1)-dimensional region  $\mathcal{X}$  may have various forms. Construction of exact confidence bands becomes much harder. Bohrer (1967) considered a hyperbolic-shape confidence band when the predictor variables are all non-negative. Bohrer (1973) presented the construction of an exact one-sided confidence band over an ellipsoidal predictor region by evaluating a multivariate t probability. Halperin and Gurian (1968) provided conservative confidence bands over an ellipsoidal region. Wynn (1975) developed a general result on the calculation of the confidence levels for one-sided confidence bands in regression analysis. Casella and Strawderman (1980) proposed exact confidence bands over a region of the same shape. The most frequently used region is of rectangular shape, and it is given by

$$\mathcal{X}_R = \{(x_2,\ldots,x_p) : a_i \leq x_i \leq b_i, i = 2,\ldots,p\},\$$

where  $-\infty \leq a_i < b_i \leq \infty, i = 2, \dots, p$  are given constants. Knaff, Sacks and Ylvisaker (1985) obtained an approximate two-sided hyperbolic-shape confidence band when  $p \leq 3$  by using an up-crossing inequality. This approach was further developed in Faraway and Sun (1995), Sun and Loader (1994), and Sun, Loader and McCormick (2000) to produce approximate two-sided confidence bands for a more general regression model. However, multiple integrations are involved in the calculation of these approximations and the dimensionality of the integrations increases with p. Naiman (1986) discussed the construction of conservative simultaneous confidence bands for curvilinear regression functions by applying the tube volume theory. For the construction of confidence bands for a more general regression model, more references can be found in Johnstone and Siegmund (1989), Knowles and Siegmund (1989), Johansen and Johnstone (1990), and Sun, Loader and McCormick (2000). Recently, Liu, Jamshidian, Zhang and Donnelly (2005) proposed the simulation-based two-sided simultaneous confidence bands over a rectangular predictor space for generally p > 2, and the critical value based on this method can be as accurate as one expects if the number of simulations is set to be sufficiently large. Moreover, this simulation-based method can be adapted to the construction of one-sided confidence bands over a similar region. Liu, Jamshidian, Zhang and Bretz (2004) considered constructing two-sided constant-width confidence bands for a multiple regression model over a rectangular region by using both numerical integration and simulation. The existing literatures of the construction of simultaneous confidence bands for logistic regression models are very limited. The main contributions to this area are: Brand, Pinnock and Jackson (1973) which described a method of obtaining a confidence band for a simple logistic regression based on the large sample distribution of the maximum likelihood estimators, Hauck (1983) which further developed the previous work to the multiple case by applying the Cauchy-Schwartz inequality, Piegorsch and Casella (1988) which first discussed the confidence bands for a logistic regression with restricted predictor variables, and Sun, Loader and McCormick (2000) which developed their approximate method of Sun and Loader (1994) applicable to the generalized linear models.

### 1.2 The organization of this thesis

We continue to introduce some concepts and basic tools in the rest of this chapter on large sample theory, which include some important inequalities and theorems required in the subsequent chapters but without explicit proof here. In Chapter 2, we describe the generalized linear models, specially, the logistic regression model, involving the large sample asymptotic distribution of the estimators and related inferences. In Chapter 3, our attention is focused on the construction of exact one-sided and two-sided hyperbolic-shape simultaneous confidence bands for a simple linear regression model with restricted predictor variable based on three methods. Chapter 4 continues to talk about the construction of confidence bands using the same methods for a multiple linear regression over an ellipsoidal region. In Chapter 5, we consider the construction of simultaneous confidence bands for a regression model over a rectangular region based on several methods and then compare these methods in terms of critical values. In Chapter 6, we discuss the construction of simultaneous confidence bands for a logistic regression model and then give simulation studies to check the goodness of the considered bands. Finally, Chapter 7 provides some main conclusions and the future work.

#### 1.3 Concepts and basic tools

Definition 1.3.1 (Convergence in probability) A sequence  $\{T_n\}$  of random variables is said to converge in probability to a (possibly degenerate) random variable T, if for every positive numbers  $\varepsilon$  and  $\eta$ , there exists a positive integer  $n_0 = n_0(\varepsilon, \eta)$ , such that

$$P\{d(T_n, T) > \varepsilon\} < \eta, \quad n \ge n_0, \tag{1.10}$$

where  $d(\cdot)$  denotes a distance function (or norm). This mode of convergence is usually expressed by  $T_n - T \xrightarrow{P} 0$ . In the case where T is non-stochastic, we may write  $T_n \xrightarrow{P} T$ .

**Definition 1.3.2 (Convergence in distribution)** A sequence  $\{T_n\}$  of random variables with distribution functions  $F_n$  is said to converge in distribution (or in law) to a (possibly degenerate) random variable T with a distribution function F, if for every  $\varepsilon > 0$ , there exists an integer  $n_0 = n_0(\varepsilon)$ , such that at every point of continuity of F,

$$|F_n(x) - F(x)| < \varepsilon, \quad n \ge n_0. \tag{1.11}$$

This mode of convergence is denoted in this thesis by  $T_n \stackrel{\mathcal{D}}{\longrightarrow} T$ .

**Definition 1.3.3 (Almost sure convergence)** A sequence  $\{T_n\}$  of random variables is said to converge almost surely (a.s.) to a (possibly degenerate) random variable T, if for every positive  $\varepsilon$  and  $\eta$ , there exists a positive integer  $n_0 = n_0(\varepsilon, \eta)$ , such that

$$P\{d(T_N, T) > \varepsilon \quad for \ some \ N \ge n\} < \eta, \quad n \ge n_0. \tag{1.12}$$

In symbols, we write this as  $T_n - T \xrightarrow{a.s.} 0$ , and if T is non-stochastic, it may also be written as  $T_n \xrightarrow{a.s.} T$ .

**Theorem 1.3.1 (Chebyshev Inequality)** Let U be a non-negative random variable with a finite mean  $\mu = E(U)$ . Then for every t > 0,

$$P\{U > t\mu\} \le t^{-1}.$$
 (1.13)

Theorem 1.3.2 (Lindeberg-Feller) Let  $X_k, k \ge 1$ , be independent random variables such that  $E(X_k) = \mu_k$  and  $Var(X_k) = \sigma_k^2, k \ge 1$ ; also let  $T_n = \sum_{k=1}^n X_k, \ \xi_n = E(T_n) = \sum_{k=1}^n \mu_k, \ s_n^2 = Var(T_n) = \sum_{k=1}^n \sigma_k^2$  and  $Z_n = (T_n - \xi_n)/s_n = \sum_{k=1}^n Y_{nk}$  where  $Y_{nk} = (X_k - \mu_k)/s_n$ . Consider the following conditions:

A) Uniform asymptotic negligibility condition:

$$\max_{1 \le k \le n} \frac{\sigma_k^2}{s_n^2} \to 0 \quad as \quad n \to \infty.$$

B) Asymptotic normality condition:

$$\mathbb{P}\{Z_n \le z\} \to \frac{1}{\sqrt{2\pi}} \int_{-\infty}^z \exp\left(\frac{-t^2}{2}\right) dt = \Phi(z) \quad as \quad n \to \infty.$$

C) Lindeberg-Feller condition:

$$\forall \varepsilon > 0, \quad \frac{1}{s_n^2} \sum_{k=1}^n \mathbf{E} \Big[ (X_k - \mu_k)^2 I_{\{|X_k - \mu_k| > \varepsilon s_n\}} \Big] \to 0 \quad as \quad n \to \infty.$$

Then, (A) and (B) hold simultaneously if and only if (C) holds.

**Theorem 1.3.3 (Slutsky)** Let  $\{X_n\}$  and  $\{Y_n\}$  be sequences of random variables such that  $X_n \xrightarrow{\mathcal{D}} X$  and  $Y_n \xrightarrow{P} c$ , where c is a constant. Then, it follows that

i)  $X_n + Y_n \xrightarrow{\mathcal{D}} X + c$ , ii)  $Y_n X_n \xrightarrow{\mathcal{D}} cX$ , iii)  $X_n/Y_n \xrightarrow{\mathcal{D}} X/c$  if  $c \neq 0$ .

Theorem 1.3.4 (Khintchine Strong Law of Large Numbers) Let  $X_i, i \ge 1$  be independently identically distributed random variables. Then  $\bar{X}_n \xrightarrow{a.s.} c$ , and only if  $E(X_1)$  exists and  $c = E(X_1)$ .

**Theorem 1.3.5 (Delta Method)** Let  $\{\mathbf{T}_n\}$  be a sequence of random vectors such that  $\sqrt{n}(\mathbf{T}_n - \theta) \xrightarrow{\mathcal{D}} N(0, \Sigma)$  and consider a real-valued function  $g(\mathbf{T}_n)$  such that  $g'(\theta)$  is non-null and continuous in a neighborhood of  $\theta$ . Then

$$\sqrt{n}[g(\mathbf{T}_n) - g(\boldsymbol{\theta})] \xrightarrow{\mathcal{D}} N(0, \boldsymbol{\gamma}^2) \text{ with } \boldsymbol{\gamma}^2 = [g'(\boldsymbol{\theta})]^T \boldsymbol{\Sigma}[g'(\boldsymbol{\theta})].$$

# Chapter 2

# Generalized linear models and logistic regression model with binary data

### 2.1 Introduction

As we intend to construct simultaneous confidence bands for both linear and logistic regression models, it is motivated to introduce the generalized linear models first. The so-called generalized linear models, an extension of the classical linear modelling process that allows models to be fitted to data, can be analogously used in the following more general situations: first, the response variables have probability distributions other than the normal distribution, such as poisson, binomial, multinomial and etc; second, the relationship between the response and the predictor variables are not necessarily of the linear form. Also, generalized linear models relax the requirement of equality or constancy of variances that is required for hypothesis testing in traditional linear models. Generalized linear models include, as special cases, the linear regression and analysis of variance models, the log-linear models for categorical data, the product multinomial response models, the logistic model with binary data as well as some simple statistical models arising in survival analysis. In particular, the logistic regression model with a binary response variable is of our interest in this thesis.

In this chapter, we first specify the models, followed by the consideration of the parameter estimation based on the maximum likelihood and Newton-Raphson iterative method. Then, we focus on the asymptotic behavior of the estimators. Some related statistical inferences are considered after that specially for the logistic regression model.

## 2.2 Model specification

#### 2.2.1 Generalized linear models

Consider a single random variable Y whose probability distribution depends on a single parameter  $\theta$ . The distribution belongs to the exponential family if it can be written of the form given by

$$f(y,\theta) = \exp[a(y)b(\theta) + c(\theta) + d(y)], \qquad (2.1)$$

where a, b, c and d are known functions. Specially, if a(y) = y, the distribution is said to be in canonical form. If there are other parameters, in addition to the parameter of interest  $\theta$ , they are regarded as nuisance parameters forming parts of the functions a, b, c and d, and they are treated as though they are known. Many familiar distributions belong to the exponential family. For example, the poisson distribution, the normal distribution and the binomial distribution can all be written in the canonical form. Details can be found in, e.g., Dobson (2001).

The idea of a generalized linear model was introduced by Nelder and Wedderburn (1972) to demonstrate a unity of many statistical methods. This model is defined in terms of a set of independent random variables  $Y_1, \ldots, Y_N$  each with a distribution from the exponential family and has the following properties:

1. the distribution of each  $Y_i$  has the canonical form and depends on a

single parameter  $\theta_i$ , thus

$$f(y_i, \theta_i) = \exp[y_i b_i(\theta_i) + c_i(\theta_i) + d_i(y_i)]; \qquad (2.2)$$

2. the distribution of all  $Y_i$ 's are of the same form so that the subscripts on b, c, and d can all be ignored, thus the joint probability density function of  $Y_1, \ldots, Y_N$  is given by

$$f(y_1, \dots, y_N; \theta_1, \dots, \theta_N)$$

$$= \prod_{i=1}^N \exp[y_i b(\theta_i) + c(\theta_i) + d(y_i)]$$

$$= \exp\left[\sum_{i=1}^N y_i b(\theta_i) + \sum_{i=1}^N c(\theta_i) + \sum_{i=1}^N d(y_i)\right].$$
(2.3)

The parameters  $\theta_i$  and the observations of  $y_i, i = 1, ..., N$  may one-to-one correspond, which leads that  $\theta_i$ 's are typically not of direct interest. A smaller set of parameters  $\beta_1, ..., \beta_p$  (where p < N) are usually adopted. Suppose that  $E(Y_i) = \mu_i$  where  $\mu_i$  is some function of  $\theta_i$ . In a generalized linear model, a relationship between  $\mu_i$  and a linear combination  $\mathbf{x}_i^T \boldsymbol{\beta}$  is specified as

$$g(\mu_i) = \mathbf{x}_i^T \boldsymbol{\beta},\tag{2.4}$$

where g is a monotone and differentiable function called the link function,  $\mathbf{x}_i$  is a *p*-dimensional vector of the predictor variables and the *i*th column of the design matrix X as well, and  $\boldsymbol{\beta} = (\beta_1, \ldots, \beta_p)^T$  is the parameter vector of interest. Different link function determines different class of generalized linear models the considered model belongs to.

#### 2.2.2 Binary response and logistic regression model

In this subsection, we consider a generalized linear model in which the outcome variable is measured on a binary scale. 'Success' and 'failure' are usually used as generic terms of the two categories. Define the binary random variable

$$Z = \begin{cases} 1 & \text{if the outcome is a success,} \\ 0 & \text{if the outcome is a failure,} \end{cases}$$

with probabilities  $P\{Z = 1\} = \pi$  and  $P\{Z = 0\} = 1 - \pi$ . If there are *n* such random variables  $Z_1, \ldots, Z_n$  which are independent and with  $P\{Z_j = 1\} = \pi_j$ , then their joint probability is

$$\prod_{j=1}^{n} \pi_{j}^{z_{j}} (1-\pi_{j})^{1-z_{j}} = \exp\Big[\sum_{j=1}^{n} z_{j} \log\Big(\frac{\pi_{j}}{1-\pi_{j}}\Big) + \sum_{j=1}^{n} \log(1-\pi_{j})\Big], \quad (2.5)$$

which obviously is a member of the exponential family. For the case when  $\pi_j$ 's are all equal, a new random variable can be defined by

$$Y = \sum_{j=1}^{n} Z_j$$

so that Y is the number of successes in n 'trials'. Then Y has the binomial distribution with parameters n and  $\pi$ , and its probability distribution function is given by

$$P\{Y = y\} = {n \choose y} \pi^{y} (1 - \pi)^{n - y}, \qquad y = 0, 1, \dots, n.$$

Now consider m independent such random variables  $Y_1, \ldots, Y_m$  corresponding to the numbers of successes in m different subgroups. Each subgroup is of size  $n_i, i = 1, \ldots, m$  such that  $\sum_{i=1}^m n_i = N$ . Since  $Y_i \sim binomial(n_i, \pi_i)$ , the log-likelihood function is therefore given by

$$l(\pi_{1}, \dots, \pi_{m}; y_{1}, \dots, y_{m}) = \sum_{i=1}^{m} \left[ y_{i} \log \left( \frac{\pi_{i}}{1 - \pi_{i}} \right) + n_{i} \log(1 - \pi_{i}) + \log \left( \begin{array}{c} n_{i} \\ y_{i} \end{array} \right) \right]. \quad (2.6)$$

The proportion of the successes in each subgroup, i.e.,  $P_i = y_i/n_i$ ,  $i = 1, \ldots, m$ , is of interest. Note that  $E(Y_i) = n_i \pi_i$  implies  $E(P_i) = \pi_i$ . The probability  $\pi_i$  is linked with the parameters of interest by

$$g(\pi_i) = \mathbf{x}_i^T \boldsymbol{\beta}$$

where  $\mathbf{x}_i$  and  $\boldsymbol{\beta}$  are the same as before, g is the link function. Therefore, the general linear logistic regression model is defined by setting the link function

$$g = \log\left(\frac{\pi_i}{1 - \pi_i}\right) = \mathbf{x}_i^T \boldsymbol{\beta}, \quad i = 1, \dots, m,$$
(2.7)

where  $\log[\pi_i/(1-\pi_i)]$  is sometimes called the logit function.

### 2.3 Parameter estimation

To estimate parameters in a generalized linear model, we use a method based on the maximum likelihood. Although explicit mathematical expression can be obtained for the estimators of the parameters in some special cases, numerical method is usually needed which is typically iterative and based on the Newton-Raphson algorithm.

Consider the independent random variables  $Y_1, \ldots, Y_m$  that fulfil the requirements of a generalized linear model. We have  $E(Y_i) = \mu_i$  and  $g(\mu_i) = \mathbf{x}_i^T \boldsymbol{\beta} = \eta_i$ , where  $\mathbf{x}_i$  is the vector with the elements  $x_{ij}$ ,  $i = 1, \ldots, m$  indicating which subgroup the observation belongs to and  $j = 1, \ldots, p$  indicating which predictor variable is observed. For each  $Y_i$ , the likelihood function is

$$f(y_i, \theta_i) = \exp[y_i b(\theta_i) + c(\theta_i) + d(y_i)], \qquad (2.8)$$

where the functions b, c and d are known. In order to derive the score functions as well as the information matrix, expressions for the expected value and variance of  $Y_i$ 's are needed. The following method is used to find the score functions and the information matrix by changing the order of integration and differentiation provided a density function.

By the property that a probability density function integrates to 1, we have

$$\frac{\partial}{\partial \theta_i} \int f(y_i, \theta_i) \mathrm{d}y_i = \frac{\partial}{\partial \theta_i} \cdot 1 = 0.$$
(2.9)

Changing the order of the integration and differentiation, (2.9) becomes

$$\int \frac{\partial f(y_i, \theta_i)}{\partial \theta_i} \mathrm{d}y_i = 0.$$
(2.10)

Similarly, when the differentiation in (2.9) is of second order, then we have

. 1

$$\int \frac{\partial^2 f(y_i, \theta_i)}{\partial \theta_i^2} \mathrm{d}y_i = 0.$$
(2.11)

These results can be used to obtain the expectations and the variances of  $Y_i$ 's. (2.10) can be further written as

$$\int f(y_i, \theta_i) [y_i b'_i(\theta_i) + c'(\theta_i)]$$

$$= \int f(y_i, \theta_i) y_i b'(\theta_i) + \int f(y_i, \theta_i) c'(\theta_i)$$

$$= b'(\theta_i) \mu_i + c'(\theta_i) = 0$$

Thus, we have

$$E(Y_i) = \mu_i = -c'(\theta_i)/b'(\theta_i).$$
(2.12)

Similarly, we have

$$\operatorname{Var}(Y_{i}) = [b''(\theta_{i})c'(\theta_{i}) - c''(\theta_{i})b'(\theta_{i})]/[b'(\theta_{i})]^{3}.$$
(2.13)

Now we turn to derive the score function and the information matrix. The log-likelihood function for all the  $Y_i$ 's is

$$l = \sum_{i=1}^{m} l_i = \sum_{i=1}^{m} y_i b(\theta_i) + \sum_{i=1}^{m} c(\theta_i) + \sum_{i=1}^{m} d(y_i).$$
(2.14)

We use the chain rule for differentiation to obtain the score function which is given by

$$\frac{\partial l}{\partial \beta_j} = U_j = \sum_{i=1}^m \left( \frac{\partial l_i}{\partial \beta_j} \right) = \sum_{i=1}^m \left( \frac{\partial l_i}{\partial \theta_i} \cdot \frac{\partial \theta_i}{\partial \mu_i} \cdot \frac{\partial \mu_i}{\partial \beta_j} \right).$$
(2.15)

Consider each term on the right-hand side of (2.15) separately.  $\partial l_i/\partial \theta_i$  can be obtained from (2.14),  $\partial \theta_i/\partial \mu_i$  can be obtained from (2.12), and  $\partial \mu_i/\partial \beta_j$ can be obtained from the link function. Substituting these three individuals into (2.15) finally gives

$$U_j = \sum_{i=1}^m \left[ \frac{(y_i - \mu_i)}{\operatorname{Var}(Y_i)} x_{ij} \left( \frac{\partial \mu_i}{\partial \eta_i} \right) \right].$$
(2.16)

The variance-covariance matrix of  $U_i$  has the terms

$$J_{jk} = E(U_j U_k)$$
  
= 
$$\sum_{i=1}^{m} \left[ \frac{x_{ij} x_{ik}}{\operatorname{Var}(Y_i)} \left( \frac{\partial \mu_i}{\partial \eta_i} \right)^2 \right], \qquad (2.17)$$

where j, k = 1, ..., p.

An iterative procedure is usually adopted for parameter estimation. The most commonly used method is the following Newton-Raphson approximation. Suppose t is a function of x, Newton-Raphson method is the iterative process described by

$$x^{(r)} = x^{(r-1)} - \frac{t\left(x^{(r-1)}\right)}{t'\left(x^{(r-1)}\right)}$$
(2.18)

to find the value of x such that t(x) = 0. It starts with an initial guess  $x^{(1)}$  to obtain successive approximation until the iterative process converges.

By Newton-Raphson's formula, the *r*th approximation of the parameter vector  $\beta$  is given by

$$\mathbf{b}^{(r)} = \mathbf{b}^{(r-1)} - \left(\frac{\partial^2 l}{\partial \beta \partial \beta^T}\right)_{\beta = \mathbf{b}^{(r-1)}}^{-1} \mathbf{U}^{(r-1)}, \qquad (2.19)$$

where  $\mathbf{b}^{(r)}$  denotes the vector of the estimates of the parameter vector  $\boldsymbol{\beta}$ at the *r*th iteration,  $\mathbf{U}^{(r-1)}$  is the vector of the first order derivatives  $U_j$ 's evaluated at  $\boldsymbol{\beta} = \mathbf{b}^{(r-1)}$ . By the method of scoring which replaces the matrix of the second order derivatives in (2.19) by its expectation, and the fact that

$$J = -\mathrm{E}\Big(\frac{\partial^2 l}{\partial \beta \partial \beta^T}\Big),$$

we have (2.19) equal to

$$\mathbf{b}^{(r)} = \mathbf{b}^{(r-1)} + \left[ J^{(r-1)} \right]^{-1} \mathbf{U}^{(r-1)}, \qquad (2.20)$$

where  $[J^{(r-1)}]^{-1}$  is the inverse of the information matrix with the elements  $J_{jk}$  given by (2.17) all evaluated at  $\mathbf{b}^{(r-1)}$ . An alternative version gives

$$J^{(r-1)}\mathbf{b}^{(r)} = J^{(r-1)}\mathbf{b}^{(r-1)} + \mathbf{U}^{(r-1)}.$$
(2.21)

By (2.17) J can be written as

$$J = X^T W X,$$

where W is an  $m \times m$  diagonal matrix with the elements given by

$$w_{ii} = \frac{1}{\operatorname{Var}(Y_i)} \left(\frac{\partial \mu_i}{\partial \eta_i}\right)^2.$$
(2.22)

By (2.16) and (2.17), the right-hand side of the equation (2.21) can be written as  $X^T W \mathbf{z}$ , where  $\mathbf{z}$  has the elements

$$z_{i} = \sum_{j=1}^{p} x_{ij} b_{j}^{(r-1)} + (y_{i} - \mu_{i}) \left(\frac{\partial \eta_{i}}{\partial \mu_{i}}\right)$$
(2.23)

with  $\mu_i$  and  $\partial \eta_i / \partial \mu_i$  evaluated at  $\mathbf{b}^{(r-1)}$ . Hence the iterative equation (2.21) is equal to

$$X^{T} W^{(r-1)} X \mathbf{b}^{(r)} = X^{T} W^{(r-1)} \mathbf{z}^{(r-1)}$$
(2.24)

which has to be solved iteratively because, in general, z and W depend on b. Thus for generalized linear models, the maximum likelihood estimates are obtained by an iterative weighted procedure.

In particular for logistic regression model, we have the log-likelihood function given by

$$l(\boldsymbol{\pi}; \mathbf{y}) = \sum_{i=1}^{m} \left[ y_i \log \left( \frac{\pi_i}{1 - \pi_i} \right) + n_i \log(1 - \pi_i) + \log \left( \begin{array}{c} n_i \\ y_i \end{array} \right) \right],$$

where  $\pi = (\pi_1, \ldots, \pi_m)^T$  and  $\mathbf{y} = (y_1, \ldots, y_m)^T$ . Also, we have the link function

$$g(\pi_i) = \eta_i = \log\left(\frac{\pi_i}{1-\pi_i}\right) = \mathbf{x}_i^T \boldsymbol{\beta}.$$

Using the chain rule in (2.15), we have

$$\frac{\partial l}{\partial \beta_j} = \sum_{i=1}^m \left( \frac{\partial l_i}{\partial \pi_i} \cdot \frac{\partial \pi_i}{\partial \eta_i} \cdot \frac{\partial \eta_i}{\partial \beta_j} \right) = \sum_{i=1}^m (y_i - n_i \pi_i) x_{ij}$$

The fisher information for  $\beta$  is therefore

$$J_{jk} = -\mathbb{E}\left(\frac{\partial^2 l}{\partial \beta_j \partial \beta_k}\right) = \sum_{i=1}^m n_i \pi_i (1 - \pi_i) x_{ij} x_{ik} = \{X^T W X\}_{jk}$$

where j, k = 1, ..., p and W is a diagonal matrix of the weights given by

$$W = \operatorname{diag}\{n_i \pi_i (1 - \pi_i)\}.$$

Following the Newton-Raphson procedure, define  $\mathbf z$  with the elements given by

$$z_i = \hat{\eta}_i + \frac{y_i - n_i \hat{\pi}_i}{n_i} \cdot \frac{\partial \eta_i}{\partial \pi_i},$$

then the maximum likelihood estimates can be obtained from the equation (2.24).

Most statistical packages include the algorithm of estimation for generalized linear models. They begin by evaluating  $\mathbf{z}$  and W using some initial approximation  $\mathbf{b}^{(0)}$ , then solve the iterative equation (2.24) to obtain  $\mathbf{b}^{(1)}$ which in turn is used to get better approximations for  $\mathbf{z}$  and W, and so on until adequate convergence is reached. When the difference between the two successive approximations  $\mathbf{b}^{(r-1)}$  and  $\mathbf{b}^{(r)}$  is sufficiently small, then  $\mathbf{b}^{(r)}$  is taken as the maximum likelihood estimate of the parameter vector  $\boldsymbol{\beta}$ .

### 2.4 Asymptotic behavior of estimators

#### 2.4.1 Introduction

Since most distributional inferences on generalized linear models are valid based on large samples, there is a need to look into the large sample asymptotic theory so that some desired distributional properties for the estimators can be obtained. Specifically, the asymptotic normality of the maximum likelihood estimators is of interest.

Recall the specification of a generalized linear model in Section 2.2. Consider the vector of observations  $\mathbf{y} = (y_1, \ldots, y_m)^T$  corresponding to m independent random variables  $Y_i, i = 1, \ldots, m$ , each with a distribution in the exponential family. We have the density function for each  $Y_i$  given by

$$f(y_i, \theta_i, \phi) = c(y_i, \phi) \exp\{[y_i \theta_i - b(\theta_i)]/a(\phi)\}, \qquad (2.25)$$

where  $\theta_i$ 's are parameters,  $\phi > 0$  is a scale and  $a(\cdot)$ ,  $b(\cdot)$  and  $c(\cdot)$  are all known functions which are distinguishable from those appeared previously. Therefore the joint density function is

$$f(y_1, \dots, y_m; \theta_1, \dots, \theta_m; \phi)$$

$$= \prod_{i=1}^m f(y_i, \theta_i, \phi)$$

$$= c(\mathbf{y}, \phi) \exp\left\{\sum_{i=1}^m [y_i\theta_i - b(\theta_i)]/a(\phi)\right\},$$
(2.26)

where

$$c(\mathbf{y},\phi) = \prod_{i=1}^m c(y_i,\phi).$$

Review that

$$E(Y_i) = \mu_i(\theta_i) = b'(\theta_i), \qquad (2.27)$$

$$\operatorname{Var}(Y_i) = a(\phi)b''(\theta_i) = a(\phi)v_i[\mu_i(\theta_i)], \qquad (2.28)$$

where  $v_i[\mu_i(\theta_i)]$  is known as the variance function of  $\theta_i$  which depends solely on  $\mu_i(\theta_i)$  for  $1 \leq i \leq m$ . Furthermore, conceive of a transformation which provides the link between  $\mu_i$  and  $\mathbf{x}_i^T \boldsymbol{\beta}$  of the form

$$g[\mu(\theta_i)] = \mathbf{x}_i^T \boldsymbol{\beta}, \quad i = 1, \dots, m,$$
(2.29)

where  $g(\cdot)$  is a monotone and differentiable function and  $\beta = (\beta_1, \ldots, \beta_p)^T$  is the *p*-dimensional parameter vector. Alternatively, the link can be arranged in multi-dimensional version that

$$\mathbf{G} = \left(g(\mu_1), \dots, g(\mu_m)\right)^T = X\boldsymbol{\beta}, \qquad (2.30)$$

where  $X = (\mathbf{x}_1, \dots, \mathbf{x}_m)^T$  denotes a known  $m \times p$  matrix.

Now we turn to find the asymptotic distribution of  $\hat{\beta}$ , the maximum likelihood estimator of  $\beta$  in the generalized linear model. Usually it is assumed in the asymptotic sense that the total sample size  $N \to \infty$ , where  $N = \sum_{i=1}^{m} n_i$  with  $n_i$  being the sample size of the *i*th subgroup of observations. However, there may be another situation where for each *i*, the  $Y_i$  may be a statistic

given the subsample size  $n_i$ . In such a case, a second type of asymptotic might be considered where it is not crucial to have N large, provided the  $n_i$ 's are themselves large. In the rest of this section, we focus on the regular case first, where  $N \to \infty$ , and briefly talk about the second type of asymptotic after that.

#### 2.4.2 The first type of asymptotic

Define  $h(\cdot) = (g \circ \mu)^{-1}(\cdot)$  so that (2.29) is transformed to

$$\theta_i = h(\mathbf{x}_i^T \boldsymbol{\beta}), \quad i = 1, \dots, m, \tag{2.31}$$

where h is monotone and differentiable. The parameter vector  $\beta$  is of direct interest. By reviewing (2.25) and (2.26), we may note that the nuisance parameter  $\phi$  does not affect the estimation of  $\beta$  and it influences the information matrix J only by a multiplicative factor  $[a(\phi)]^{-2}$  which may be estimated consistently. Therefore, for the sake of simplicity and without loss of generality,  $a(\phi) \equiv 1$  is taken. Consider (2.31), the log-likelihood function in terms of  $\beta$  is given by

$$\log L_N(\boldsymbol{\beta}) = \sum_{i=1}^m \left\{ n_i y_i h(\mathbf{x}_i^T \boldsymbol{\beta}) - n_i b[h(\mathbf{x}_i^T \boldsymbol{\beta})] \right\} - \text{constant}, \quad (2.32)$$

where the constant term does not depend on  $\beta$ , the subscript of the likelihood, i.e., N, indicates that it is for the first type of asymptotic, and the quantities with such a subscript hereafter in this chapter are of the same meaning. Recall (2.27) and (2.28), then we have

$$\mu_i(\boldsymbol{\beta}) = \mu[h(\mathbf{x}_i^T \boldsymbol{\beta})] = b'[h(\mathbf{x}_i^T \boldsymbol{\beta})], \qquad (2.33)$$

$$v_i(\boldsymbol{\beta}) = v[h(\mathbf{x}_i^T \boldsymbol{\beta})] = b''[h(\mathbf{x}_i^T \boldsymbol{\beta})].$$
(2.34)

Thus, the score function of  $\beta$  is given by

$$\mathbf{U}_{N}(\boldsymbol{\beta}) = \frac{\partial}{\partial \boldsymbol{\beta}} \log L_{N}(\boldsymbol{\beta}) = \sum_{i=1}^{m} \frac{n_{i}[y_{i} - \mu_{i}(\boldsymbol{\beta})]}{\{g'[\mu_{i}(\boldsymbol{\beta})]v_{i}(\boldsymbol{\beta})\}} \mathbf{x}_{i}, \qquad (2.35)$$

from which it follows that whenever  $g'(\cdot)$  and  $v(\cdot) \equiv b''(\cdot)$  are both differentiable, then we have

$$-\frac{\partial^2}{\partial\beta\partial\beta^T}\log L_N(\beta) = J_N(\beta) + R_N(\beta), \qquad (2.36)$$

where

$$J_N(\beta) = \sum_{i=1}^m n_i \{ g'[\mu_i(\beta)] \}^{-2} [v_i(\beta)]^{-1} \mathbf{x}_i \mathbf{x}_i^T$$
(2.37)

and

$$R_{N}(\beta) = \sum_{i=1}^{m} n_{i}[y_{i} - \mu_{i}(\beta)] \\ \times \left\{ \frac{g''[\mu_{i}(\beta)]}{\{g'[\mu_{i}(\beta)]\}^{2}} + \frac{b'''[h(\mathbf{x}_{i}^{T}\beta)]}{\{g'[\mu_{i}(\beta)]\}^{2}[v_{i}(\beta)]^{3}} \right\} \mathbf{x}_{i} \mathbf{x}_{i}^{T}.$$
(2.38)

**Remark 2.4.1** Recall (2.31) that when  $g = \mu^{-1}$ ,  $g \circ \mu$  is the identity function, hence,  $\theta_i = \mathbf{x}_i^T \boldsymbol{\beta}$ . In such a case,  $g(\cdot)$  is termed a canonical link function. By (2.36)-(2.38), we have that for canonical link functions,  $R_N(\boldsymbol{\beta}) = 0$ .

*Proof.* For canonical link functions, we have  $h(\mathbf{x}_i^T \boldsymbol{\beta}) = \mathbf{x}_i^T \boldsymbol{\beta}$  and  $g = \mu^{-1}$ . Thus

$$b'[h(\mathbf{x}_{i}^{T}\boldsymbol{\beta})] = \mu(\mathbf{x}_{i}^{T}\boldsymbol{\beta}) = g^{-1}(\mathbf{x}_{i}^{T}\boldsymbol{\beta})$$
  

$$\Rightarrow g\{b'[h(\mathbf{x}_{i}^{T}\boldsymbol{\beta})]\} = \mathbf{x}_{i}^{T}\boldsymbol{\beta}$$
  

$$\Rightarrow g[b'(\mathbf{x}_{i}^{T}\boldsymbol{\beta})] = \mathbf{x}_{i}^{T}\boldsymbol{\beta}.$$
(2.39)

Differentiate the both sides of the last equality in (2.39) with respect to  $\beta$  and obtain

$$g'[b'(\mathbf{x}_i^T\boldsymbol{\beta})] \cdot b''(\mathbf{x}_i^T\boldsymbol{\beta}) \cdot \mathbf{x}_i = \mathbf{x}_i$$
(2.40)

which implies

$$b''(\mathbf{x}_i^T\boldsymbol{\beta}) = \{g'[b'(\mathbf{x}_i^T\boldsymbol{\beta})]\}^{-1}.$$
(2.41)

Differentiate twice and obtain

$$g''[b'(\mathbf{x}_i^T\boldsymbol{\beta})] \cdot [b''(\mathbf{x}_i^T\boldsymbol{\beta})]^2 \cdot \mathbf{x}_i \mathbf{x}_i^T + g'[b'(\mathbf{x}_i^T\boldsymbol{\beta})] \cdot b'''(\mathbf{x}_i^T\boldsymbol{\beta}) \cdot \mathbf{x}_i \mathbf{x}_i^T = 0 \quad (2.42)$$
23

which, in connection with (2.41), implies

ł

$$\left\{ \frac{g''[b'(\mathbf{x}_i^T\boldsymbol{\beta})]}{\{g'[b'(\mathbf{x}_i^T\boldsymbol{\beta})]\}^2} + \frac{b'''(\mathbf{x}_i^T\boldsymbol{\beta})}{g'[\mu_i(\boldsymbol{\beta})] \cdot [b''(\mathbf{x}_i^T\boldsymbol{\beta})]^2} \right\} \mathbf{x}_i \mathbf{x}_i^T \\
= \left\{ \frac{g''[b'(\mathbf{x}_i^T\boldsymbol{\beta})]}{\{g'[b'(\mathbf{x}_i^T\boldsymbol{\beta})]\}^2} + \frac{b'''(\mathbf{x}_i^T\boldsymbol{\beta})}{\{g'[\mu_i(\boldsymbol{\beta})]\}^2[b''(\mathbf{x}_i^T\boldsymbol{\beta})]^3} \right\} \mathbf{x}_i \mathbf{x}_i^T = 0. \quad (2.43)$$

We therefore simply obtain  $R_N(\beta) = 0. \ \#$ 

In order to obtain the asymptotic distribution of the estimator of  $\beta$  under the consistent setup, we need to discuss some required assumptions.

Assumption 2.4.1 Assume that

$$\lim_{N \to \infty} \frac{1}{N} J_N(\beta) = J(\beta), \text{ finite and positive definite.}$$
(2.44)

Assumption 2.4.2 Let

$$\mathbf{G}_{i} = \left\{ \frac{g''[\mu_{i}(\boldsymbol{\beta})]}{(g'[\mu_{i}(\boldsymbol{\beta})])^{2}} + \frac{b'''[h(\mathbf{x}_{i}^{T}\boldsymbol{\beta})]}{\{g'[\mu_{i}(\boldsymbol{\beta})]\}^{2}[v_{i}(\boldsymbol{\beta})]^{3}} \right\} \mathbf{x}_{i} \mathbf{x}_{i}^{T} = w_{i} \mathbf{x}_{i} \mathbf{x}_{i}^{T}, \qquad (2.45)$$

where

$$w_{i} = \left\{ \frac{g''[\mu_{i}(\boldsymbol{\beta})]}{\{g'[\mu_{i}(\boldsymbol{\beta})]\}^{2}} + \frac{b'''[h(\mathbf{x}_{i}^{T}\boldsymbol{\beta})]}{\{g'[\mu_{i}(\boldsymbol{\beta})]\}^{2}[v_{i}(\boldsymbol{\beta})]^{3}} \right\}, \quad i = 1, \dots, m,$$
(2.46)

and assume that

$$\lim_{N \to \infty} N^{-2} \sum_{i=1}^{m} n_i^2 v_i [\mu_i(\boldsymbol{\beta})] \operatorname{tr}(\mathbf{G}_i \mathbf{G}_i^T) = 0.$$
(2.47)

By directly applying Chebyshev Inequality (1.11) to (2.38) that for  $\forall \varepsilon > 0$ ,

$$P\{N^{-1}R_{N}(\boldsymbol{\beta}) > \varepsilon\}$$

$$= P\{[N^{-1}R_{N}(\boldsymbol{\beta})]^{2} > \varepsilon^{2}\}$$

$$\leq \frac{E[N^{-1}R_{N}(\boldsymbol{\beta})]^{2}}{\varepsilon^{2}}$$

$$= \frac{N^{-2}\sum_{i=1}^{m}n_{i}^{2}v_{i}[\mu_{i}(\boldsymbol{\beta})]\operatorname{tr}(\mathbf{G}_{i}\mathbf{G}_{i}^{T})}{\varepsilon^{2}}, \qquad (2.48)$$

in connection with Assumption 2.4.2, we can simply obtain  $N^{-1}R_N(\beta) \xrightarrow{P} 0$ . From (2.36), we have

$$\frac{1}{N} \left[ \frac{\partial^2}{\partial \beta \partial \beta^T} \log L_N(\beta) + J_N(\beta) \right] \xrightarrow{P} 0.$$
(2.49)

Next, we find the asymptotic normality of the score function given in (2.35). Observe that  $E[\mathbf{U}_N(\boldsymbol{\beta})] = 0$  and  $\operatorname{Var}[\mathbf{U}_N(\boldsymbol{\beta})] = J_N(\boldsymbol{\beta})$ . To apply Lindeberg-Feller Theorem to the independent but not necessarily identically distributed random vectors, it is needed to show the Lindeberg-Feller condition is satisfied. For  $\forall \varepsilon > 0$ , consider

$$J_N^{-1}(\boldsymbol{\beta}) \sum_{i=1}^m \mathrm{E}(\mathbf{t}_i \mathbf{t}_i^T) \mathrm{P}\{\|\mathbf{t}_i \mathbf{t}_i^T\| > \varepsilon \|J_N(\boldsymbol{\beta})\|\},$$
(2.50)

where  $\mathbf{t}_i$  is defined such that

$$\mathbf{U}_N(\boldsymbol{\beta}) = \sum_{i=1}^m \frac{n_i [y_i - \mu_i(\boldsymbol{\beta})]}{\{g'[\mu_i(\boldsymbol{\beta})] v_i(\boldsymbol{\beta})\}} \mathbf{x}_i = \sum_{i=1}^m \mathbf{t}_i.$$
 (2.51)

By applying Chebyshev Inequality, we have

$$J_{N}^{-1}(\boldsymbol{\beta}) \sum_{i=1}^{m} \mathbb{E}(\mathbf{t}_{i}\mathbf{t}_{i}^{T}) \mathbb{P}\{\|\mathbf{t}_{i}\mathbf{t}_{i}^{T}\| > \varepsilon \|J_{N}(\boldsymbol{\beta})\|\}$$

$$\leq J_{N}^{-1}(\boldsymbol{\beta}) \sum_{i=1}^{m} \mathbb{E}(\mathbf{t}_{i}\mathbf{t}_{i}^{T}) \frac{\mathbb{E}\|\mathbf{t}_{i}\mathbf{t}_{i}^{T}\|}{\varepsilon \|J_{N}(\boldsymbol{\beta})\|}$$
(2.52)

$$\leq \frac{\max(\mathbf{E} \|\mathbf{t}_i \mathbf{t}_i^T\|)}{\varepsilon \|J_N(\boldsymbol{\beta})\|} J_N^{-1}(\boldsymbol{\beta}) \sum_{i=1}^m \mathbf{E}(\mathbf{t}_i \mathbf{t}_i^T),$$
(2.53)

where  $\max(\mathbb{E}||\mathbf{t}_i \mathbf{t}_i^T||)$  is the maximum of  $\mathbb{E}||\mathbf{t}_i \mathbf{t}_i^T||$  as i = 1, 2, ..., m. Also it is known that  $J_N^{-1}(\boldsymbol{\beta}) \sum_{i=1}^m \mathbb{E}(\mathbf{t}_i \mathbf{t}_i^T)$  is equal to the identity matrix. From Assumption 2.4.1, we know that  $||J_N(\boldsymbol{\beta})|| \to \infty$  as  $N \to \infty$ . Thus, we have that the right-hand side of (2.53) converges to zero as  $N \to \infty$  so that (2.50) converges to zero as  $N \to \infty$ . Lindeberg-Feller condition is satisfied. By Lindeberg-Feller Theorem in connection with Assumption 2.4.1, we therefore have the asymptotic normality of  $\mathbf{U}_N(\boldsymbol{\beta})$  that

$$\frac{1}{\sqrt{N}}\mathbf{U}_{N}(\boldsymbol{\beta}) \xrightarrow{\mathcal{D}} N(0, J(\boldsymbol{\beta})).$$
(2.54)
Now we turn to our central work to show the asymptotic normality of the maximum likelihood estimator  $\hat{\beta}$ . Let  $\|\mathbf{u}\| < k, 0 < k < \infty$  and consider the Taylor Expansion of  $\log L_N(\boldsymbol{\beta} + N^{-\frac{1}{2}}\mathbf{u})$  around  $\log L_N(\boldsymbol{\beta})$ . Define

$$\lambda_{N}(\mathbf{u}) = \log L_{N}(\boldsymbol{\beta} + N^{-\frac{1}{2}}\mathbf{u}) - \log L_{N}(\boldsymbol{\beta})$$
  
$$= \frac{1}{\sqrt{N}}\mathbf{u}^{T}\mathbf{U}_{N}(\boldsymbol{\beta}) + \frac{1}{\sqrt{2N}}\mathbf{u}^{T}\frac{\partial^{2}}{\partial\boldsymbol{\beta}\partial\boldsymbol{\beta}^{T}}\log L_{N}(\boldsymbol{\beta})\Big|_{\boldsymbol{\beta}^{*}}\mathbf{u}, \quad (2.55)$$

where  $\beta^*$  is a point belonging to the line ended by  $\beta$  and  $(\beta + N^{-\frac{1}{2}}\mathbf{u})$  in the parameter space. Also, define

$$Z_{N}(\mathbf{u}) = \frac{1}{\sqrt{2N}} \left\{ \mathbf{u}^{T} \frac{\partial^{2}}{\partial \beta \partial \beta^{T}} \log L_{N}(\beta) \Big|_{\beta^{*}} \mathbf{u} - \mathbf{u}^{T} \frac{\partial^{2}}{\partial \beta \partial \beta^{T}} \log L_{N}(\beta) \Big|_{\beta} \mathbf{u} + \mathbf{u}^{T} \frac{\partial^{2}}{\partial \beta \partial \beta^{T}} \log L_{N}(\beta) \Big|_{\beta} \mathbf{u} + \mathbf{u}^{T} J_{N}(\beta) \mathbf{u} \right\}.$$
(2.56)

Then (2.55) can be alternatively written as

$$\lambda_N(\mathbf{u}) = \frac{1}{\sqrt{N}} \mathbf{u}^T \mathbf{U}_N(\boldsymbol{\beta}) - \frac{1}{\sqrt{2N}} \mathbf{u}^T J_N(\boldsymbol{\beta}) \mathbf{u} + Z_N(\mathbf{u}).$$
(2.57)

Observe that

$$\sup_{\|\mathbf{u}\| < k} \|Z_{N}(\mathbf{u})\| \leq \frac{1}{2} \sup_{\boldsymbol{\beta}^{*} \in \mathbf{B}(k/\sqrt{N})} \left\| \frac{1}{N} \frac{\partial^{2}}{\partial \boldsymbol{\beta} \partial \boldsymbol{\beta}^{T}} \log L_{N}(\boldsymbol{\beta}) \right\|_{\boldsymbol{\beta}^{*}} - \frac{1}{N} \frac{\partial^{2}}{\partial \boldsymbol{\beta} \partial \boldsymbol{\beta}^{T}} \log L_{N}(\boldsymbol{\beta}) \right\|_{\boldsymbol{\beta}} + \frac{k^{2}}{2} \left\| \frac{1}{N} \frac{\partial^{2}}{\partial \boldsymbol{\beta} \partial \boldsymbol{\beta}^{T}} \log L_{N}(\boldsymbol{\beta}) \right\|_{\boldsymbol{\beta}} + \frac{1}{N} J_{N}(\boldsymbol{\beta}) \right\|, \qquad (2.58)$$

where  $B(k/\sqrt{N})$  is defined in the following assumption. From (2.49), the second absolute value on the right-hand side of (2.58) converges to zero in probability as  $N \to \infty$ . Next we consider the first term on the right-hand side of (2.58).

Assumption 2.4.3 Suppose that  $\{g'[\mu_i(\beta^*)]\}^{-2}$ ,  $[v_i(\beta^*)]^{-3}$ ,  $g''[\mu_i(\beta^*)]$  and  $b'''[h(\mathbf{x}_i^T\beta^*)]$  are uniformly continuous in an infinitesimal neighborhood of the true  $\beta$ , i.e., in the set

$$B(\delta) = \{ \boldsymbol{\beta}^* \in \mathcal{R}^p : \| \boldsymbol{\beta}^* - \boldsymbol{\beta} \| < \delta \}, \quad \delta \downarrow 0.$$
(2.59)

Let

$$w_{1i}(\beta) = \{g'[\mu_i(\beta)]\}^{-2}[v_i(\beta)]^{-1}$$

and

$$w_{2i}(\boldsymbol{\beta}) = \mu_i(\boldsymbol{\beta}) w_i(\boldsymbol{\beta}),$$

where  $w_i(\beta)$  is defined in (2.46),  $i = 1, \ldots, m$ .

1. For k = 1, 2, as  $\delta \downarrow 0$ ,

$$\sup_{\boldsymbol{\beta}^* \in \mathbf{B}(\delta)} \| \{ w_{ki}(\boldsymbol{\beta}^*) - w_{ki}(\boldsymbol{\beta}) \} \mathbf{x}_i \mathbf{x}_i^T \| \to 0.$$
 (2.60)

2. As  $\delta \downarrow 0$ ,

$$\mathbb{E}_{\boldsymbol{\beta}}\{\sup_{\boldsymbol{\beta}^* \in \mathbb{B}(\delta)} |y_i| \| w_i(\boldsymbol{\beta})^* - w_i(\boldsymbol{\beta}) \mathbf{x}_i \mathbf{x}_i^T \| \} = \psi \to 0, \qquad (2.61)$$

where  $\psi$  is a scale.

Observe according to (2.36)-(2.38) that

$$E_{\beta} \left\{ \sup_{\beta^{*} \in B(k/\sqrt{N})} \left\| \frac{\partial^{2}}{\partial \beta \partial \beta^{T}} \log f(y_{i}; \beta) \right|_{\beta^{*}} - \frac{\partial^{2}}{\partial \beta \partial \beta^{T}} \log f(y_{i}; \beta) \Big|_{\beta} \right\| \right\}$$

$$= E_{\beta} \left\{ \sup_{\beta^{*} \in B(k/\sqrt{N})} \left\| \{w_{1i} + [y_{i} - \mu_{i}(\beta)]w_{i}\}\mathbf{x}_{i}\mathbf{x}_{i}^{T} \right|_{\beta^{*}} - \{w_{1i} + [y_{i} - \mu_{i}(\beta)]w_{i}\}\mathbf{x}_{i}\mathbf{x}_{i}^{T} \Big|_{\beta} \right\| \right\}$$

$$\leq \sup_{\beta^{*} \in B(k/\sqrt{N})} \left\| [w_{1i}(\beta^{*}) - w_{1i}(\beta)]\mathbf{x}_{i}\mathbf{x}_{i}^{T} \right\|$$
(2.62)

$$+ \sup_{\boldsymbol{\beta}^* \in \mathcal{B}(k/\sqrt{N})} \| [w_{2i}(\boldsymbol{\beta}^*) - w_{2i}(\boldsymbol{\beta})] \mathbf{x}_i \mathbf{x}_i^T \|$$
(2.63)

By Assumption 2.4.3, (2.62)-(2.64) converge to zero separately as  $k/\sqrt{N} \to 0$ , which implies that the left-hand side of the above inequality converges to zero as  $k/\sqrt{N} \to 0$ . In addition, observe that

$$\frac{1}{2} \sup_{\beta^{\star} \in B(k/\sqrt{N})} \left\| \frac{1}{N} \frac{\partial^{2}}{\partial \beta \partial \beta^{T}} \log L_{N}(\beta) \right|_{\beta^{\star}} - \frac{1}{N} \frac{\partial^{2}}{\partial \beta \partial \beta^{T}} \log L_{N}(\beta) \Big|_{\beta} \right\|$$

$$\leq \frac{1}{2N} \sum_{i=1}^{m} n_{i} \sup_{\beta^{\star} \in B(k/\sqrt{N})} \left\| \frac{\partial^{2}}{\partial \beta \partial \beta^{T}} \log f(y_{i};\beta) \right|_{\beta^{\star}} - \frac{\partial^{2}}{\partial \beta \partial \beta^{T}} \log f(y_{i};\beta) \Big|_{\beta} \right\|.$$
(2.65)

27

By the Khintehine Strong Law of Large Numbers, since

$$\mathbb{E}_{\boldsymbol{\beta}} \left\{ \sup_{\boldsymbol{\beta}^{*} \in \mathbb{B}(k/\sqrt{N})} \left\| \frac{\partial^{2}}{\partial \boldsymbol{\beta} \partial \boldsymbol{\beta}^{T}} \log f(y_{i}; \boldsymbol{\beta}) \right|_{\boldsymbol{\beta}^{*}} - \frac{\partial^{2}}{\partial \boldsymbol{\beta} \partial \boldsymbol{\beta}^{T}} \log f(y_{i}; \boldsymbol{\beta}) \Big|_{\boldsymbol{\beta}} \right\| \right\} \to 0$$

as  $k/\sqrt{N} \to 0$ , we have the right-hand side of the inequality (2.65) converges to zero almost surely. And this implies the left-hand side of (2.65), which is the same as the first term on the right-hand side of (2.58), converges to zero almost surely. Consequently, from (2.58), we have

$$\sup_{\|\mathbf{u}\| < k} \|Z_N(\mathbf{u})\| \xrightarrow{a.s.} 0.$$
 (2.66)

Rewrite (2.57) as

$$\lambda_N(\mathbf{u}) = \frac{1}{\sqrt{N}} \mathbf{u}^T \mathbf{U}_N(\boldsymbol{\beta}) - \frac{1}{2N} \mathbf{u}^T J_N(\boldsymbol{\beta}) \mathbf{u} + o_p(1).$$
(2.67)

By Assumption 2.4.1, (2.67) is equal to

$$\lambda_N(\mathbf{u}) = \frac{1}{\sqrt{N}} \mathbf{u}^T \mathbf{U}_N(\boldsymbol{\beta}) - \frac{1}{2} \mathbf{u}^T J(\boldsymbol{\beta}) \mathbf{u} + o_p(1),$$

when  $N \to \infty$ . Maximize  $\lambda_N(\mathbf{u})$  by solving  $\partial \lambda_N(\mathbf{u}) / \partial \mathbf{u} = 0$ , and then obtain

$$\hat{\mathbf{u}} = \frac{1}{\sqrt{N}} J^{-1}(\boldsymbol{\beta}) \mathbf{U}_N(\boldsymbol{\beta}) + o_p(1)$$

By the definition of  $\lambda_N(\mathbf{u})$  in (2.55), it is clear that  $\hat{\mathbf{u}}$  makes  $L_N(\boldsymbol{\beta} + N^{-1/2}\mathbf{u})$  maximal, and the maximum of which is obtained at  $\hat{\boldsymbol{\beta}}$ . Therefore, we have

$$\hat{\boldsymbol{\beta}} = \boldsymbol{\beta} + N^{-1/2} \hat{\mathbf{u}} + o_p(N^{-1/2}) = \boldsymbol{\beta} + N^{-1} J^{-1}(\boldsymbol{\beta}) \mathbf{U}_N(\boldsymbol{\beta}) + o_p(N^{-1/2}), \qquad (2.68)$$

which implies

$$\sqrt{N}(\hat{\boldsymbol{\beta}}-\boldsymbol{\beta}) = rac{1}{\sqrt{N}}J^{-1}(\boldsymbol{\beta})\mathbf{U}_N(\boldsymbol{\beta}) + o_p(1).$$

Apply Slutsky Theorem in connection with (2.54) and then obtain

$$\sqrt{N}(\hat{\boldsymbol{\beta}} - \boldsymbol{\beta}) \xrightarrow{\mathcal{D}} N_p(0, J^{-1}(\boldsymbol{\beta})).$$
(2.69)

The idea of how to obtain (2.69) for the first type of asymptotic comes from Sen and Singer (1993).

¢.

In particular, consider a logistic regression model. For the sake of simplicity, we assume that there is only one predictor variable and no intercept term is included in the model, i.e., p = 1. To avoid a degenerate binomial distribution, take  $x_i \neq 0$ . The canonical link function is given by

$$g(\pi) = \log\left(\frac{\pi}{1-\pi}\right).$$

Accordingly, we have

$$g'(\pi) = \frac{1}{\pi(1-\pi)}$$
 and  $v_i(\beta) = \frac{\exp(2\beta x_i)}{[1+\exp(\beta x_i)]^2} x_i^2$ .

By Assumption 2.4.3, we have

$$w_{1i}(\beta) = \left\{ \frac{[1 + \exp(\beta x_i)]^2}{\exp(\beta x_i)} \right\}^{-2} \cdot \left\{ \frac{\exp(2\beta x_i)}{[1 + \exp(\beta x_i)]^2} x_i^2 \right\}^{-1} \\ = \left\{ [1 + \exp(\beta x_i)]^2 x_i^2 \right\}^{-1}.$$

Considering Remark 2.4.1, the assumptions required for obtaining the asymptotic normality of the maximum likelihood estimator  $\hat{\beta}$  reduce to

1. Assume that

$$\lim_{N \to \infty} \frac{1}{N} \sum_{i=1}^{m} n_i [1 + \exp(\beta x_i)]^{-2} = J(\beta) < \infty.$$

2. For some k:  $0 < k < \infty$ , as  $N \to \infty$ 

$$\sup_{\substack{|h| \le k/\sqrt{N}}} \left| \{1 + \exp[(\beta + h)x_i]\}^{-2} - [1 + \exp(\beta x_i)]^{-2} \right|$$
  
=  $\left| \{1 + \exp[(\beta + k/\sqrt{N})x_i]\}^{-2} - [1 + \exp(\beta x_i)]^{-2} \right| \to 0$ 

If we suppose the only predictor variable is bounded, then both conditions hold. Thus, we have

$$\sqrt{N}(\hat{\beta}-\beta) \xrightarrow{\mathcal{D}} N(0, J^{-1}(\beta)).$$

In this case, the design matrix X reduces to the m-dimensional vector  ${\bf x}$  such that

$$J(\beta) = \mathbf{x}^T W \mathbf{x},$$

where W is the diagonal weight matrix with the elements given by

$$w_{ii} = \frac{\exp(\beta x_i)}{[1 + \exp(\beta x_i)]^2} \quad i = 1, \dots, m,$$

 $x_i$  is the *i*-th element of **x**.

#### 2.4.3 The second type of asymptotic

We considered the first type of asymptotic behavior of  $\beta$  in last subsection, i.e., set the total sample size N large. As for the second type of asymptotic, we do not necessarily set N large and may consider the subsample sizes  $n_i, i = 1, \ldots, m$  are themselves large.

Take the case of m = 2 for example. Consider the independent binary variables  $z_{ij}$ ,  $i = 1, 2, j = 1, \ldots, n_i$ , which have the Bernoulli distribution and are defined by

$$z_{ij} = \begin{cases} 1 & \text{with probability} \quad \pi_i, \\ 0 & \text{with probability} \quad 1 - \pi_i. \end{cases}$$

Then, we have  $E(z_{ij}) = \pi_i$  and  $Var(z_{ij}) = \pi_i(1 - \pi_i)$ . Define a random vector **Y** such that

$$Y_i = \sum_{j=1}^{n_i} \frac{z_{ij}}{n_i} \qquad i = 1, 2.$$
(2.70)

Then  $\mathbf{Y}$  can be viewed as the vector of the frequencies of the independent binomial random variables.

Consider the second type of asymptotic, i.e., set the subsample sizes  $n_i \rightarrow \infty$  for i = 1, 2. A common subsample size  $n \rightarrow \infty$  is introduced to replace the individuals. Then by Classical Central Limit Theorem, the asymptotic normality of the random vector **Y** can be simply obtained as

$$\sqrt{n}(\mathbf{Y}-\boldsymbol{\mu}) \xrightarrow{\mathcal{D}} N_2(\mathbf{0},\boldsymbol{\Sigma})$$
 (2.71)

where  $\mu = (\pi_1, \pi_2)^T$  is the mean vector of Y, and  $\Sigma$  is the asymptotic variance-covariance matrix given by

$$\Sigma = \begin{pmatrix} \pi_1(1-\pi_1) & 0\\ 0 & \pi_2(1-\pi_2) \end{pmatrix}.$$
 (2.72)

If the parameter vector  $\beta$  is of direct interest, therefore, it is specified by a generalized linear model with a link to a linear combination that

$$g(\boldsymbol{\mu}) = X\boldsymbol{\beta},\tag{2.73}$$

where g satisfies the properties of a link function, X is the design matrix with specific entries. Then Delta Method may be applied appropriately to (2.71) to obtain the asymptotic normality of  $\hat{\beta}$  given by

$$\sqrt{n}(\hat{\boldsymbol{\beta}} - \boldsymbol{\beta}) \xrightarrow{\mathcal{D}} N(0, J^{-1}(\boldsymbol{\beta})),$$
 (2.74)

where

$$J(\boldsymbol{\beta}) = X^T W X,$$

W is the diagonal weight matrix with the elements given by

$$w_{ii} = \frac{\exp(\mathbf{x}_i^T \boldsymbol{\beta})}{[1 + \exp(\mathbf{x}_i^T \boldsymbol{\beta})]^2} \quad i = 1, 2,$$

and  $\mathbf{x}_i$  is the *i*-th row of the design matrix.

# 2.5 Goodness of fit statistics

#### 2.5.1 Deviance

One way of assessing the adequacy of a model is to compare it with a more general model, called a saturated model, with the maximum number of parameters that can be estimated. It is a generalized linear model with the same distribution and link function as the model of interest.

Let k denote the maximum number of parameters that can be estimated for the saturated model. Then k is equal to the number of potentially different linear components, which may be less than the number of observations N. Let  $\beta_{\max}$  denote the parameter vector for the saturated model and  $\hat{\beta}_{\max}$  denote the maximum likelihood estimator of  $\beta_{\max}$ . The likelihood function for the saturated model evaluated at  $\hat{\beta}_{\max}$ , noted by  $L(\hat{\beta}_{\max}; \mathbf{y})$ , will be larger than any other likelihood function for these observations with the same assumed distribution and link function. That is because it provides the most complete description of the data. Also, denote  $L(\hat{\beta}; \mathbf{y})$  the maximum value of the likelihood function for the model of interest. Therefore, the likelihood ratio

$$\lambda = \frac{L(\hat{\boldsymbol{\beta}}_{\max}; \mathbf{y})}{L(\hat{\boldsymbol{\beta}}; \mathbf{y})}$$
(2.75)

provides a way of assessing the goodness of fit for the model. In practice, the logarithm of  $\lambda$ , which stands for the difference between the log-likelihood functions

$$\log \lambda = l(\hat{\boldsymbol{\beta}}_{\max}; \mathbf{y}) - l(\hat{\boldsymbol{\beta}}; \mathbf{y})$$

is used. Large values of  $\log \lambda$  suggest that the model of interest is a poor fit of the data relative to the saturated model.

In next section, the sampling distributions will be discussed. Then we may notice that  $2 \log \lambda$  rather than  $\log \lambda$  is the most commonly used statistic and is referred to as the deviance termed by Nelder and Wedderburn (1972). In particular, for linear logistic regression, it is given by

$$D = 2\sum_{i=1}^{m} \left[ y_i \log\left(\frac{y_i}{n_i \hat{\pi}_i}\right) + (n_i - y_i) \log\left(\frac{n_i - y_i}{n_i - n_i \hat{\pi}_i}\right) \right].$$
 (2.76)

#### 2.5.2 Pearson chi-squared statistic

Instead of using maximum likelihood estimation we could estimate the parameters by minimizing the Pearson chi-squared statistic

$$X^2 = \sum \frac{(o-e)^2}{e},$$

where o represents the observed frequencies and e represents the expected frequencies. In particular, for linear logistic regression, the Pearson chisquared statistic evaluated at the estimated expected frequencies is given by

$$X^{2} = \sum_{i=1}^{m} \frac{(y_{i} - n_{i}\hat{\pi}_{i})^{2}}{n_{i}\hat{\pi}_{i}(1 - \hat{\pi}_{i})}.$$
(2.77)

#### 2.5.3 Equivalence

The Taylor Expansion of  $s \log(s/t)$  about s = t is given by

$$s \log \frac{s}{t} = (s-t) + \frac{1}{2} \frac{(s-t)^2}{t} + \cdots$$

By applying the above expansion to (2.76), we have

$$D = 2\sum_{i=1}^{m} \left\{ (y_i - n_i \hat{\pi}_i) + \frac{1}{2} \frac{(y_i - n_i \hat{\pi}_i)^2}{n_i \hat{\pi}_i} + [(n_i - y_i) - (n_i - n_i \hat{\pi}_i)] + \frac{1}{2} \frac{[(n_i - y_i) - (n_i - n_i \hat{\pi}_i)]^2}{n_i - n_i \hat{\pi}_i} + \cdots \right\}$$
$$\cong \sum_{i=1}^{m} \frac{(y_i - n_i \hat{\pi}_i)^2}{n_i \hat{\pi}_i (1 - \hat{\pi}_i)} = X^2.$$
(2.78)

Thus, it is that the deviance in (2.76) is asymptotically equivalent to the Pearson chi-squared statistic in (2.77).

# 2.6 Sampling distributions of statistics

We write the first three terms of the Taylor Expansion of the log-likelihood at  $\beta = \hat{\beta}$  as

$$l(\boldsymbol{\beta}) = l(\hat{\boldsymbol{\beta}}) + (\boldsymbol{\beta} - \hat{\boldsymbol{\beta}})^T \mathbf{U}(\hat{\boldsymbol{\beta}}) - \frac{1}{2} (\boldsymbol{\beta} - \hat{\boldsymbol{\beta}})^T \mathbf{U}'(\hat{\boldsymbol{\beta}}) (\boldsymbol{\beta} - \hat{\boldsymbol{\beta}}), \qquad (2.79)$$

where  $U(\hat{\beta})$  is the score vector evaluated at  $\beta = \hat{\beta}$  and  $U'(\hat{\beta})$  is the derivative of U with respect to  $\beta$  at  $\beta = \hat{\beta}$ .

Note that  $\mathbf{U}(\hat{\boldsymbol{\beta}}) = 0$  in (2.79) is due to the maximum likelihood estimation. If  $\mathbf{U}'(\hat{\boldsymbol{\beta}})$  is approximated by its expected value  $\mathbf{E}(\mathbf{U}') = J$ , (2.79) is therefore equal to

$$l(\boldsymbol{\beta}) - l(\hat{\boldsymbol{\beta}}) = -\frac{1}{2} (\boldsymbol{\beta} - \hat{\boldsymbol{\beta}})^T J(\hat{\boldsymbol{\beta}}) (\boldsymbol{\beta} - \hat{\boldsymbol{\beta}}), \qquad (2.80)$$

where  $J(\hat{\beta})$  is the information matrix evaluated at  $\beta = \hat{\beta}$ . Therefore, we have

$$2[l(\hat{\boldsymbol{\beta}};\mathbf{y}) - l(\boldsymbol{\beta};\mathbf{y})] = (\boldsymbol{\beta} - \hat{\boldsymbol{\beta}})^T J(\hat{\boldsymbol{\beta}})(\boldsymbol{\beta} - \hat{\boldsymbol{\beta}}).$$
(2.81)

From the asymptotic distribution of  $\hat{\beta}$ , we have

$$(\boldsymbol{\beta} - \hat{\boldsymbol{\beta}})^T J(\hat{\boldsymbol{\beta}})(\boldsymbol{\beta} - \hat{\boldsymbol{\beta}}) \sim \chi_p^2,$$

where  $\chi_p^2$  stands for the Chi-square distribution with p degrees of freedom, and p here is also the dimensionality of  $\beta$ .

Thus, the sampling distribution for the deviance can be derived. Observe that

$$D = 2[l(\hat{\boldsymbol{\beta}}_{\max}; \mathbf{y}) - l(\hat{\boldsymbol{\beta}}; \mathbf{y})]$$
  
= 2[l( $\hat{\boldsymbol{\beta}}_{\max}; \mathbf{y}$ ) - l( $\boldsymbol{\beta}_{\max}; \mathbf{y}$ )]  
-2[l( $\hat{\boldsymbol{\beta}}; \mathbf{y}$ ) - l( $\boldsymbol{\beta}; \mathbf{y}$ )] + 2[l( $\boldsymbol{\beta}_{\max}; \mathbf{y}$ ) - l( $\boldsymbol{\beta}; \mathbf{y}$ )]. (2.82)

The first term on the right-hand side of (2.82) has the  $\chi_k^2$  distribution where k is the number of parameters in the saturated model. The second term has the  $\chi_p^2$  distribution where p is the number of parameters in the model of interest. The third term,  $v = 2[l(\beta_{\max}; \mathbf{y}) - l(\beta; \mathbf{y})]$ , is a positive constant which will be near zero if the model of interest fits the data almost as well as the saturated model. Consequently, the sampling distribution of the deviance is, approximately,  $\chi_{k-p,v}^2$ , where v is the non-central parameter.

For logistic regression, considering the equivalence between the deviance and the Pearson chi-squared statistic, we have approximately  $X^2 \sim \chi^2_{m-p}$ . The choice between D and  $X^2$  depends on the adequacy of the approximation to the  $\chi^2_{m-p}$  distribution. D has a general advantage as a measure of discrepancy in that it is additive for nested sets of models if maximum likelihood estimates are used, whereas  $X^2$  in general is not. However, there is some evidence to suggest that  $X^2$  is often better than D because D is unduly influenced by very small frequencies (see Cressie and Read, 1989). Both of them are likely to be poor when the expected frequencies are too small.

# 2.7 Residual analysis

Measures of agreements between observations on a response variable and the corresponding fitted values are known as residuals. These quantities, and summary statistics derived from them, can provide much information about the adequacy of the fitted model.

For logistic regression there are two main forms of residuals corresponding to the goodness of fit measures D and  $X^2$  respectively. Let m denote the number of observations of Y,  $Y_i$  denote the number of successes,  $n_i$  denote the number of trials in subgroups and  $\hat{\pi}_i$  denote the estimated probability of being success for the *i*th subgroup of samples. Then the Pearson residual is defined by

$$X_{i} = \frac{(y_{i} - n_{i}\hat{\pi}_{i})}{\sqrt{n_{i}\hat{\pi}_{i}(1 - \hat{\pi}_{i})}}, i = 1, \dots, m.$$
(2.83)

From (2.77),  $\sum_{i=1}^{m} X_i^2 = X^2$ , the Pearson chi-squared goodness of fit statistic. The standardization used in the construction of the Pearson residuals does not yield residuals that have even approximate unit variance, since no allowance has been made for the inherent variation in the fitted values of the response  $n_i \hat{\pi}_i$ . A better procedure is to divide the raw residuals  $y_i - n_i \hat{\pi}_i$  by their standard error. This standard error is quite complicated to derive, but it is found to be given by

s.e. = 
$$\sqrt{\hat{v}_i(1-h_i)}$$
,

where  $\hat{v}_i = n_i \hat{\pi}_i (1 - \hat{\pi}_i)$ ,  $h_i$  is the *i*th element on the diagonal of the hat matrix  $H = X(X^T X)^{-1} X^T$  and the quantities  $h_i$  can be easily found through many statistical packages. So the resulting standardized residuals are

$$r_{Pi} = \frac{X_i}{\sqrt{1 - h_i}}.\tag{2.84}$$

Another type of residual can be constructed from the deviance, given by

$$d_{i} = \operatorname{sign}(y_{i} - n_{i}\hat{\pi}_{i}) \left\{ 2 \left[ y_{i} \log \left( \frac{y_{i}}{n_{i}\hat{\pi}_{i}} \right) + (n_{i} - y_{i}) \log \left( \frac{n_{i} - y_{i}}{n_{i} - n_{i}\hat{\pi}_{i}} \right) \right] \right\}^{\frac{1}{2}}, \quad (2.85)$$

where the term  $\operatorname{sign}(y_i - n_i \hat{\pi}_i)$  ensures that  $d_i$  has the same sign as  $X_i$ . From (2.76),  $\sum_{i=1}^{m} d_i^2 = D$ , the deviance. Also standardized deviance residuals are defined by

$$r_{Di} = \frac{d_i}{\sqrt{1 - h_i}}.\tag{2.86}$$

These residuals can be used for checking the adequacy of a model. For instance, they should be plotted against each covariate in the model to check whether the assumption of linearity is appropriate. They should be plotted in the order of the measurements, if applicable, to check for serial correlation. Normal probability plots can also be adopted, since the standardized residuals should approximately have a standard normal distribution provided the numbers of observations for each covariate are not too small.

In the case that the data are binary or  $n_i$  is small for most covariate patterns, there are few distinct values of the residuals and, consequently, the plots may be less informative. Under this situation, the aggregated goodness of fit statistics  $X^2$  and D may be necessary to be considered.

Sections 2.5-2.7 take Dobson (2001) for main reference.

# Chapter 3

# Exact simultaneous confidence bands for a simple linear regression with restricted predictor variable

In following two chapters, we consider the construction of exact hyperbolicshape simultaneous confidence bands for a linear regression model. This chapter focuses on the construction of exact one-sided and two-sided confidence bands for a simple linear regression model with constrained predictor variable using the following three methods: the method following the idea of Bohrer (1973), the algebraical method and the tubular neighborhood method. The equivalence of the computational formulae based on these three methods is given for both one-sided and two-sided cases.

# 3.1 Exact one-sided confidence bands

Bohrer and Francis (1972) considered an one-sided confidence bound of hyperbolic shape for a simple linear regression model

$$y_i = f_i(x; \beta) + \varepsilon_i \tag{3.1}$$

with

$$f_i(x;\boldsymbol{\beta}) = \beta_1 + \beta_2(x_i - \bar{x}), i = 1, \dots, n,$$

where  $y_i$ 's are the observations of the response, the differences between the observations of the only predictor variable and their mean value  $(x_i - \bar{x})$ 's are restricted in a given interval  $[a, b], \beta = (\beta_1, \beta_2)^T$  is the vector of unknown regression coefficients,  $\varepsilon_i$ 's are independent and identically distributed normal random errors with mean 0 and unknown variance  $\sigma^2$ . If we define  $S_x = \sum (x_i - \bar{x})^2$  and  $S_{xy} = \sum (x_i - \bar{x})y_i$ , then the least squares estimator of  $\beta$  and the usual unbiased estimator of  $\sigma^2$  are given by  $\hat{\beta} = (\sum y_i/n, S_{xy}/S_x)^T$  and  $\hat{\sigma}^2 = \sum (y_i - \hat{\beta}_1 - \hat{\beta}_2(x_i - \bar{x}))/(n-2)$  respectively, which are independent by studying least squares theory and have the following distributions

$$\hat{\boldsymbol{\beta}} \sim N_2 \left( \begin{pmatrix} \beta_1 \\ \beta_2 \end{pmatrix}, \begin{pmatrix} n^{-1}\sigma^2 & 0 \\ 0 & S_x^{-1}\sigma^2 \end{pmatrix} \right),$$
$$(n-2)\hat{\sigma}^2/\sigma^2 \sim \chi^2_{n-2}.$$

An one-sided hyperbolic-shape simultaneous confidence band for the mean responses

$$f(x;\beta) = \beta_1 + \beta_2(x - \bar{x})$$

is centered by  $f(x; \hat{\beta})$  and with band width proportional to the standard deviation of  $f(x; \hat{\beta})$ . Specifically, the band, e.g., with upper bound, is given by

$$f(x;\beta) \le f(x;\hat{\beta}) + c\hat{\sigma}H(x;\hat{\beta}), \text{ for all } x - \bar{x} \in [a,b],$$

where c is a critical value and

$$H(x;\hat{\beta}) = [\operatorname{Var} f(x;\hat{\beta})]^{\frac{1}{2}} / \sigma = n^{-1} + S_x^{-1} (x - \bar{x})^2.$$

The key of constructing a simultaneous confidence band is to find an appropriate critical value c such that the band has the coverage probability defined by

$$P(c) = P\{f(x; \boldsymbol{\beta}) \le f(x; \hat{\boldsymbol{\beta}}) + c\hat{\sigma}H(x; \hat{\boldsymbol{\beta}}), x - \bar{x} \in [a, b]\}$$
(3.2)

equal to a preassigned confidence level  $1 - \alpha$ .

Let  $\mathbf{z} = (n^{-1/2}, (x - \bar{x})S_x^{-1/2})^T$  and  $\mathbf{N} = ((\beta_1 - \hat{\beta}_1)n^{1/2}, (\beta_2 - \hat{\beta}_2)S_x^{1/2})^T$ . Note that since  $\hat{\boldsymbol{\beta}} = (\hat{\beta}_1, \hat{\beta}_2)^T$  is independent of  $\hat{\sigma}$ , so is  $\mathbf{N}$ . Let  $\mathbf{t} = \mathbf{N}/\hat{\sigma}$ , then we have

$$\begin{aligned} \beta_1 + \beta_2 (x - \bar{x}) &\leq \hat{\beta}_1 + \hat{\beta}_2 (x - \bar{x}) + c\hat{\sigma} [n^{-1} + S_x^{-1} (x - \bar{x})^2] \\ \Leftrightarrow \quad (\beta_1 - \hat{\beta}_1) + (\beta_2 - \hat{\beta}_2) (x - \bar{x}) \leq c\hat{\sigma} [n^{-1} + S_x^{-1} (x - \bar{x})^2] \\ \Leftrightarrow \quad (n^{-\frac{1}{2}}, (x - \bar{x}) S_x^{-\frac{1}{2}})^T \Big[ \Big( (\beta_1 - \hat{\beta}_1) n^{\frac{1}{2}}, (\beta_2 - \hat{\beta}_2) S_x^{\frac{1}{2}} \Big) / \hat{\sigma} \Big] \\ \leq c \| (n^{-\frac{1}{2}}, (x - \bar{x}) S_x^{-\frac{1}{2}}) \|. \end{aligned}$$

Consequently, the confidence level of the band in (3.2) is equal to

$$P(c) = P\{\mathbf{z}^T \mathbf{t} \le c \|\mathbf{z}\|, \text{ for } x - \bar{x} \in [a, b]\},$$
(3.3)

where  $x - \bar{x} \in [a, b]$  determines a restricted region for  $\mathbf{z}$  in terms of a and b. From the definition of  $\mathbf{z}$ , it is clear that  $\mathbf{z}$  has the fixed first coordinate and the second coordinate bounded by an interval as  $S_x^{-1/2}$  is known. This implies that  $\mathbf{z}$  varies within a circular cone  $\mathcal{Z} = \{\mathbf{z} : z_1 \ge q ||\mathbf{z}||\}$ , where  $z_1$  is the first coordinate of  $\mathbf{z}$  and q is a constant which will be explicitly given in the following text when needed. Therefore, P(c) is equal to  $P\{\mathbf{t} \in R\}$ , where

$$R = \{ \mathbf{t} : \mathbf{z}^T \mathbf{t} \le c \| \mathbf{z} \|, \text{ all } \mathbf{z} \in \mathcal{Z} \}.$$
(3.4)

This is the starting point of the following three methods we are going to discuss.

#### 3.1.1 Method following the idea of Bohrer (1973)

Let  $\mathbf{a} = (n^{-1/2}, aS_x^{-1/2})^T$  and  $\mathbf{b} = (n^{-1/2}, bS_x^{-1/2})^T$  be the boundaries of  $\mathcal{Z}$ , and  $\phi^* \in [0, \pi]$  be the angle between  $\mathbf{a}$  and  $\mathbf{b}$ . Set up a coordinates system such that the horizontal axis has the same direction as  $\mathbf{a}$ . Let  $\phi_t$  be the angle of  $\mathbf{t}$  turned moving anti-clockwise from  $\mathbf{a}$  to  $\mathbf{t}$ .

**Lemma 3.1.1** Under the notations of t,  $\phi^*$  and  $\phi_t$ , R in (3.4) can be par-



Figure 3.1: For the method following Bohrer (1973) in one-sided case

titioned into four disjoint parts according to the location of t:

$$R_1 = \{\mathbf{t} : \|\mathbf{t}\| \le c, 0 < \phi_{\mathbf{t}} < \phi^*\}, \tag{3.5}$$

$$R_2 = \{\mathbf{t} : 0 \le \mathbf{b}^T \mathbf{t} \le c \|\mathbf{b}\|, \phi^* \le \phi_{\mathbf{t}} < \phi^* + \frac{1}{2}\pi\},$$
(3.6)

$$R_3 = \{\mathbf{t}: \phi^* + \frac{1}{2}\pi \le \phi_{\mathbf{t}} < \frac{3}{2}\pi\},$$
(3.7)

$$R_4 = \{\mathbf{t} : 0 \le \mathbf{a}^T \mathbf{t} \le c \|\mathbf{a}\|, \frac{3}{2}\pi \le \phi_{\mathbf{t}} \le 2\pi\}.$$
(3.8)

Proof. When  $\mathbf{t} \in R_1$ , then  $\mathbf{t} \in \mathcal{Z}$ . We have  $\|\mathbf{t}\|^2 \leq c\|\mathbf{t}\|$  from (3.5), and further  $\mathbf{t}^T \mathbf{t} \leq c\|\mathbf{t}\|$  which implies  $\mathbf{t} \in R$  by studying (3.4). When  $\mathbf{t} \in R_2$ , since  $\mathbf{b} \in \mathcal{Z}$ , obviously  $\mathbf{t} \in R$ . Similarly, when  $\mathbf{t} \in R_4$ ,  $\mathbf{t} \in R$ . Finally when  $\mathbf{t} \in R_3$ , since  $\mathbf{z} \in \mathcal{Z}$ , we have  $\pi/2 \leq \phi_{\mathbf{t}} - \phi_{\mathbf{z}} \leq 3\pi/2$ . Hence  $\mathbf{z}^T \mathbf{t} \leq 0$  which implies  $\mathbf{t} \in R$ . Therefore,  $\bigcup_{i=1}^4 R_i \subset R$ .

Conversely, when  $\mathbf{t} \in R$  and  $0 < \phi_{\mathbf{t}} < \phi^*$ , we have  $\mathbf{t} \in \mathbb{Z}$  from the definition of  $\phi^*$ . Then  $\mathbf{t}^T \mathbf{t} \leq c \|\mathbf{t}\|$  implies  $\|\mathbf{t}\| \leq c$  which is equivalent to  $\mathbf{t} \in R_1$ . Consider  $\mathbf{t} \in R$  and  $\phi^* \leq \phi_{\mathbf{t}} < \phi^* + \pi/2$ , only  $\mathbf{b} \in \mathbb{Z}$  in this case, so we have  $\mathbf{b}^T \mathbf{t} \leq c \|\mathbf{b}\|$  which implies  $\mathbf{t} \in R_2$ . Similarly, when  $\mathbf{t} \in R$  and  $3\pi/2 \leq \phi_{\mathbf{t}} \leq 2\pi$ , we have  $\mathbf{a}^T \mathbf{t} \leq c \|\mathbf{a}\|$  which implies  $\mathbf{t} \in R_4$ . As for the case

when  $\mathbf{t} \in R$  and  $\phi^* + \pi/2 \leq \phi_{\mathbf{t}} < 3\pi/2$ ,  $\mathbf{z}^T \mathbf{t} \leq 0$  for all  $\mathbf{z} \in \mathcal{Z}$ , we therefore have  $\mathbf{t} \in R_3$ . Consequently,  $R \subset \bigcup_{i=1}^4 R_i$ . Overall,  $\bigcup_{i=1}^4 R_i = R$ . #

By applying Lemma 3.1.1 to  $P\{t \in R\}$  with R defined in (3.4), we have the confidence level of the band based on this method equal to

$$P_B(c) = \sum_{i=1}^{4} P\{t \in R_i\},$$
(3.9)

where the four individual probabilities on the right-hand side of (3.9) can be evaluated separately. Define the polar coordinates of t in terms of  $(R_t, \phi_t)$ that  $\mathbf{t} = (R_t \cos \phi_t, R_t \sin \phi_t)$ . Note that t can be written in terms of the polar coordinates of N as  $((R_N/\hat{\sigma}) \cos \phi_N, (R_N/\hat{\sigma}) \sin \phi_N)$ . Note that  $\phi_N$ and  $\phi_t$  denote the same angle because  $\mathbf{N}/\hat{\sigma}$  does not change the location of N. As we know that N has a bivariate standard normal distribution, one may find the joint density function of  $R_N$  and  $\phi_N$  via the transformation of random variables. By finding the individual marginal density functions of  $R_N$  and  $\phi_N$ , we have that the joint density is equal to the product of the individual marginal densities. And this implies that  $R_N$ is independent of  $\phi_N$ . Accordingly,  $R_t$  is independent of  $\phi_t$ . In addition,  $\|\mathbf{t}\|^2/2 = (\|\mathbf{N}\|^2/2)/\hat{\sigma}^2 = (\|\mathbf{N}/\sigma\|^2/2)/(\hat{\sigma}^2/\sigma^2)$  has the  $F_{2,\nu}$  distribution, and  $\phi_t$  has the uniform marginal distribution.

Now, we turn to evaluate the probabilities on the right-hand side of (3.9) individually. Specifically, we have

$$P\{\mathbf{t} \in R_{1}\} = P\{\|\mathbf{t}\| \leq c, 0 < \phi_{\mathbf{t}} < \phi^{*}\}$$

$$= P\{\|\mathbf{t}\| \leq c\} \cdot P\{0 < \phi_{\mathbf{t}} < \phi^{*}\}$$

$$= P\{\|\mathbf{t}\|^{2}/2 \leq c^{2}/2\} \cdot \frac{\phi^{*}}{2\pi}$$

$$= \frac{\phi^{*}}{2\pi} F_{2,\nu}(\frac{c^{2}}{2}), \qquad (3.10)$$

$$P\{\mathbf{t} \in R_{3}\} = P\{\phi^{*} + \frac{1}{2}\pi \leq \phi_{\mathbf{t}} < \frac{3}{2}\pi\}$$

$$= [\frac{3}{2}\pi - (\phi^{*} + \frac{1}{2}\pi)]/2\pi$$

$$= \frac{1}{2} - \frac{\phi^{*}}{2\pi}, \qquad (3.11)$$

where  $F_{2,\nu}$  stands for the F cumulative distribution function with 2 and  $\nu$  degrees of freedom. As for the other two probabilities, take the case of  $\mathbf{t} \in R_2$  for example. From (3.6),  $\mathbf{b}^T \mathbf{t} \leq c ||\mathbf{b}||$  implies  $||\mathbf{t}|| \cos[\phi_{\mathbf{t}} - \phi(\mathbf{b})] \leq c$ . If we rotate the coordinates system such that the horizontal axis has the same direction as  $\mathbf{b}$ , then  $||\mathbf{t}|| \cos[\phi_{\mathbf{t}} - \phi(\mathbf{b})]$  can be thought as the projection of  $\mathbf{t}$  on the horizontal axis, namely, the first coordinate of  $\mathbf{t}$ . Doing this does not change the probability. Thus we have

$$P\{\mathbf{t} \in R_2\} = P\{0 < t_1 \le c\} \cdot P\{\phi^* \le \phi_{\mathbf{t}} < \phi^* + \frac{\pi}{2}\}$$
$$= P\{\|t_1\|^2 \le c^2\} \cdot (\phi^* + \frac{\pi}{2} - \phi^*)/2\pi$$
$$= \frac{1}{4}F_{1,\nu}(c^2).$$
(3.12)

Similarly,

$$\mathbb{P}\{\mathbf{t} \in R_4\} = \frac{1}{4}F_{1,\nu}(c^2).$$

Overall,

$$P_B(c) = \frac{\phi^*}{2\pi} F_{2,\nu}(\frac{c^2}{2}) + \frac{1}{2} F_{1,\nu}(c^2) + (\frac{1}{2} - \frac{\phi^*}{2\pi}).$$
(3.13)

#### 3.1.2 Algebraical method

From (3.3) and (3.4), the confidence level can be alternatively written as

$$P(c) = P\left\{\sup_{\mathbf{z}\in\mathcal{Z}}\frac{\mathbf{z}^{T}\mathbf{t}}{\|\mathbf{z}\|} \le c\right\}.$$
(3.14)

The key idea of the algebraical method is to find the explicit form of the supreme in (3.14).

**Lemma 3.1.2** Rotating the coordinates such that the horizontal axis reaches the central direction of  $\mathcal{Z}$ . Let  $\theta^* = (1/2)\phi^*$  be the angle between the horizontal axis and one of the boundaries of  $\mathcal{Z}$ , say, **b**. Also, let  $\theta_t$  denote the angle between the horizontal axis and **t**. Then we have

$$\sup_{\mathbf{z}\in\mathcal{Z}} \frac{\mathbf{z}^T \mathbf{t}}{\|\mathbf{z}\|} = \begin{cases} \|\mathbf{t}\| & \text{if } -\theta^* \le \theta_{\mathbf{t}} \le \theta^*, \\ \|\mathbf{t}\| \cos(\theta_{\mathbf{t}} - \theta^*) & \text{if } \theta^* < \theta_{\mathbf{t}} < \pi, \\ \|\mathbf{t}\| \cos(2\pi - \theta_{\mathbf{t}} - \theta^*) & \text{if } \pi < \theta_{\mathbf{t}} < 2\pi - \theta^*. \end{cases}$$



Figure 3.2: For the algebraical method in one-sided case

*Proof.* When  $-\theta^* \leq \theta_t \leq \theta^*$ ,  $t \in \mathbb{Z}$  which implies the supreme is equal to  $t^T t/||t|| = ||t||$ . When  $\theta^* < \theta_t < \pi$ , the supreme is equal to  $||t|| \cos(\theta_t - \theta^*)$  since  $\cos \theta$  decreases with  $\theta$ . Similarly, the supreme is equal to  $||t|| \cos(2\pi - \theta_t - \theta^*)$  when  $\pi < \theta_t < 2\pi - \theta^*$ . #

Applying Lemma 3.1.2, the confidence level (3.14) based on the algebraical method becomes

$$P_{A}(c) = P\left\{\sup_{\mathbf{z}\in\mathcal{Z}}\frac{\mathbf{z}^{T}\mathbf{t}}{\|\mathbf{z}\|} \leq c\right\}$$
  
$$= P\{\|\mathbf{t}\| \leq c, -\theta^{*} \leq \theta_{\mathbf{t}} \leq \theta^{*}\}$$
  
$$+ P\{\|\mathbf{t}\| \cos(\theta_{\mathbf{t}} - \theta^{*}) \leq c, \theta^{*} < \theta_{\mathbf{t}} < \pi\}$$
  
$$+ P\{\|\mathbf{t}\| \cos(2\pi - \theta_{\mathbf{t}} - \theta^{*}) \leq c, \pi < \theta_{\mathbf{t}} < 2\pi - \theta^{*}\}. (3.15)$$

Note that the second and the third terms on the right-hand side of (3.15) are in fact the same because the regions of t corresponding to these two cases are graphically symmetric. Therefore, (3.15) is further equal to

$$\begin{aligned} P_{A}(c) &= P\{||\mathbf{t}|| \leq c, -\theta^{*} \leq \theta_{t} \leq \theta^{*}\} \\ &+ 2P\{||\mathbf{t}|| \cos(\theta_{t} - \theta^{*}) \leq c, \theta^{*} < \theta_{t} < \pi\} \\ &= P\{||\mathbf{t}|| \leq c, -\theta^{*} \leq \theta_{t} \leq \theta^{*}\} \\ &+ 2\left(P\{0 \leq ||\mathbf{t}|| \cos(\theta_{t} - \theta^{*}) \leq c, \theta^{*} < \theta_{t} < \theta^{*} + \frac{\pi}{2}\} \right) \\ &+ P\{||\mathbf{t}|| \cos(\theta_{t} - \theta^{*}) < 0, \theta^{*} + \frac{\pi}{2} < \theta_{t} < \pi\} \right) \\ &= P\{\frac{||\mathbf{t}||^{2}}{2} \leq \frac{c^{2}}{2}\} \cdot P\{-\theta^{*} \leq \theta_{t} \leq \theta^{*}\} \\ &+ 2\left(P\{\frac{||\mathbf{t}||^{2}}{2} \leq \frac{c^{2}}{2\cos^{2}(\theta_{t} - \theta^{*})}\} \cdot P\{\theta^{*} < \theta_{t} < \theta^{*} + \frac{\pi}{2}\} \right) \\ &+ P\{\theta^{*} + \frac{\pi}{2} < \theta_{t} < \pi\} \right) \\ &= \frac{2\theta^{*}}{2\pi} F_{2,\nu}(\frac{c^{2}}{2}) + 2\left(\int_{\theta^{*}}^{\theta^{*} + \frac{\pi}{2}} \frac{1}{2\pi} F_{2,\nu}\left(\frac{c^{2}}{2\cos^{2}(\theta - \theta^{*})}\right) d\theta + \frac{\pi/2 - \theta^{*}}{2\pi}\right) \\ &= \frac{\theta^{*}}{\pi} F_{2,\nu}(\frac{c^{2}}{2}) + \frac{1}{\pi} \int_{0}^{\frac{\pi}{2}} F_{2,\nu}(\frac{c^{2}}{2\cos^{2}\theta}) d\theta + (\frac{1}{2} - \frac{\theta^{*}}{\pi}), \end{aligned}$$
(3.16)

where  $F_{2,\nu}$  denotes the cumulative distribution function of  $F_{2,\nu}$  distribution.

# 3.1.3 Tubular neighborhood method

The idea of this method seems similar to the thoughts in Naiman (1986, 1990), Sun and Loader (1994). Here, the exact volume of the tubular neighborhood of a circular cone is calculated to evaluate the coverage probability of the one-sided confidence band.

From (3.14), the confidence level is given by the alternative form

$$P(c) = P\left\{\sup_{\mathbf{z}\in\mathcal{Z}}\frac{\mathbf{z}^{T}\mathbf{t}}{\|\mathbf{z}\|\|\mathbf{t}\|} \le \frac{c}{\|\mathbf{t}\|}\right\}.$$
(3.17)

Note that t/||t|| is independent of ||t|| and so is c/||t||. And the supreme in



Figure 3.3: For the tubular neighborhood method in one-sided case

(3.17) is no larger than one. Then (3.17) is further equal to

$$1 - P\left\{\sup_{\mathbf{z}\in\mathcal{Z}} \frac{\mathbf{z}^{T}\mathbf{t}}{\|\mathbf{z}\|\|\mathbf{t}\|} > \frac{c}{\|\mathbf{t}\|}\right\}$$

$$= 1 - \int_{0}^{\infty} P\left\{\sup_{\mathbf{z}\in\mathcal{Z}} \frac{\mathbf{z}^{T}\mathbf{t}}{\|\mathbf{z}\|\|\mathbf{t}\|} > \frac{c}{\sqrt{2w}}\right\} \cdot dF_{2,\nu}(w)$$

$$= 1 - \int_{\frac{c^{2}}{2}}^{\infty} P\left\{\sup_{\mathbf{z}\in\mathcal{Z}} \frac{\mathbf{z}^{T}\mathbf{t}}{\|\mathbf{z}\|\|\mathbf{t}\|} > \frac{c}{\sqrt{2w}}\right\} \cdot dF_{2,\nu}(w). \quad (3.18)$$

Let  $0 < h = c/\sqrt{2w} < 1$ . The set

$$\mathbf{E}(h) = \left\{ \mathbf{t} : \sup_{\mathbf{z} \in \mathcal{Z}} \frac{\mathbf{z}^T \mathbf{t}}{\|\mathbf{z}\| \|\mathbf{t}\|} > h \right\}$$

contains all possible t's with the angle between t and z being at largest  $\cos^{-1} h$ . So E(h) is in fact a fan with vertex at the origin, symmetrically containing the region of Z, and has the angle  $\cos^{-1} h$  between one of its bound and the nearest bound of Z. Therefore,  $P\{t \in E(h)\}$  is equal to

 $2P\{0 \le \theta_t \le \theta^* + \cos^{-1} h\}$ . Consequently, (3.18) becomes

$$1 - \int_{\frac{c^2}{2}}^{\infty} 2 \cdot \frac{\theta^* + \cos^{-1}(c/\sqrt{2w})}{2\pi} \cdot dF_{2,\nu}(w)$$
  
=  $1 - \int_{\frac{c^2}{2}}^{\infty} \frac{\theta^* + \cos^{-1}(c/\sqrt{2w})}{\pi} \cdot dF_{2,\nu}(w).$  (3.19)

#### 3.1.4 Equivalence of the formulae

It is of natural interest to compare the three computational formulae (3.13), (3.16) and (3.19) corresponding to the three methods respectively. Formula (3.13) comes from the original paper of Bohrer and Francis (1972). We first derive the equivalent formula of (3.13) by rotating the coordinates system.

Rotating the coordinates system such that the central direction of Z is given by  $z_1$  axis. In this case, by defining  $\theta^* = \phi^*/2$  and  $\theta_t$  as the angle between  $z_1$  axis and the vector  $\mathbf{t}$ , the confidence level based on the first method is then  $P_B(c) = \sum_{i=1}^4 P\{\mathbf{t} \in R'_i\}$ , where

$$R'_{1} = \{\mathbf{t} : \|\mathbf{t}\| \le c, -\theta^{*} < \theta_{\mathbf{t}} < \theta^{*}\},\$$

$$R'_{2} = \{\mathbf{t} : \|\mathbf{t}\| \cos(\theta_{\mathbf{t}} - \theta^{*}) \le c, \theta^{*} < \theta_{\mathbf{t}} < \theta^{*} + \frac{\pi}{2}\},\$$

$$R'_{3} = \{\mathbf{t} : \theta^{*} + \frac{\pi}{2} < \theta_{\mathbf{t}} < \frac{3\pi}{2} - \theta^{*}\},\$$

$$R'_{4} = \{\mathbf{t} : \|\mathbf{t}\| \cos(\theta_{\mathbf{t}} - \theta^{*}) \le c, \frac{3\pi}{2} - \theta^{*} < \theta_{\mathbf{t}} < 2\pi\}.$$
(3.20)

So we have

$$P_{B}(c) = \int_{-\theta^{*}}^{\theta^{*}} \frac{1}{2\pi} P\{\|\mathbf{t}\| \le c\} d\theta + 2 \int_{\theta^{*}}^{\theta^{*} + \frac{\pi}{2}} \frac{1}{2\pi} P\{\|\mathbf{t}\| \le \frac{c}{\cos(\theta - \theta^{*})}\} d\theta + \int_{\theta^{*} + \frac{\pi}{2}}^{\frac{3\pi}{2} - \theta^{*}} \frac{1}{2\pi} d\theta = \frac{\theta^{*}}{\pi} F_{2,\nu}(\frac{c^{2}}{2}) + \frac{1}{\pi} \int_{0}^{\frac{\pi}{2}} F_{2,\nu}(\frac{c^{2}}{2\cos^{2}\theta}) d\theta + \frac{\pi - 2\theta^{*}}{2\pi}$$
(3.21)  
$$= \frac{\theta^{*}}{\pi} F_{2,\nu}(\frac{c^{2}}{2}) + \frac{1}{\pi} \int_{0}^{\frac{\pi}{2}} d\theta \int_{0}^{\frac{c^{2}}{2\cos^{2}\theta}} dF_{2,\nu}(w) + \frac{\pi - 2\theta^{*}}{2\pi}.$$
(3.22)



Figure 3.4: Picture obtained by rotating the coordinates system

Note that (3.21) is the same as (3.16) which implies that the method following the idea of Bohrer (1973) can have the same formula as the algebraical method. The second term of (3.22) is further equal to

$$\frac{1}{\pi} \left( \int_{0}^{\frac{\pi}{2}} d\theta \int_{0}^{\frac{c^{2}}{2}} dF_{2,\nu}(w) + \int_{0}^{\frac{\pi}{2}} d\theta \int_{\frac{c^{2}}{2\cos^{2}\theta}}^{\frac{c^{2}}{2\cos^{2}\theta}} dF_{2,\nu}(w) \right)$$

$$= \frac{1}{2} F_{2,\nu}(\frac{c^{2}}{2}) + \frac{1}{\pi} \int_{\frac{c^{2}}{2}}^{\infty} \int_{\cos^{-1}(\frac{c}{\sqrt{2w}})}^{\frac{\pi}{2}} d\theta \cdot dF_{2,\nu}(w). \quad (3.23)$$

By substituting (3.23) into (3.22), we have

$$P_B(c) = \left(\frac{\theta^*}{\pi} + \frac{1}{2}\right) F_{2,\nu}\left(\frac{c^2}{2}\right) + \frac{\pi - 2\theta^*}{2\pi} + \frac{1}{\pi} \int_{\frac{c^2}{2}}^{\infty} \int_{\cos^{-1}\left(\frac{c}{\sqrt{2w}}\right)}^{\frac{\pi}{2}} d\theta \cdot dF_{2,\nu}(w).$$
(3.24)

Now consider formula (3.19). It can be further written as

$$1 - \int_{\frac{c^2}{2}}^{\infty} \frac{\theta^*}{\pi} dF_{2,\nu}(w) - \int_{\frac{c^2}{2}}^{\infty} \frac{\cos^{-1}(c/\sqrt{2w})}{\pi} dF_{2,\nu}(w)$$

$$= 1 - \frac{\theta^*}{\pi} F_{2,\nu}(w > \frac{c^2}{2}) - \frac{1}{\pi} \int_{\frac{c^2}{2}}^{\infty} \int_{0}^{\cos^{-1}(\frac{c}{\sqrt{2w}})} d\theta \cdot dF_{2,\nu}(w)$$

$$= \frac{\theta^*}{\pi} F_{2,\nu}(\frac{c^2}{2}) + \frac{\pi - \theta^*}{\pi} - \frac{1}{\pi} \int_{\frac{c^2}{2}}^{\infty} \left(\int_{0}^{\frac{\pi}{2}} - \int_{\cos^{-1}(\frac{c}{\sqrt{2w}})}^{\frac{\pi}{2}}\right) d\theta \cdot dF_{2,\nu}(w)$$

$$= \frac{\theta^*}{\pi} F_{2,\nu}(\frac{c^2}{2}) + \frac{\pi - \theta^*}{\pi} - \frac{1}{2} F_{2,\nu}(w > \frac{c^2}{2}) + \frac{1}{\pi} \int_{\frac{c^2}{2}}^{\infty} \int_{\cos^{-1}(\frac{c}{\sqrt{2w}})}^{\frac{\pi}{2}} d\theta \cdot dF_{2,\nu}(w)$$

$$= (\frac{\theta^*}{\pi} + \frac{1}{2}) F_{2,\nu}(\frac{c^2}{2}) + \frac{\pi - 2\theta^*}{2\pi} + \frac{1}{\pi} \int_{\frac{c^2}{2}}^{\infty} \int_{\cos^{-1}(\frac{c}{\sqrt{2w}})}^{\frac{\pi}{2}} d\theta \cdot dF_{2,\nu}(w), \quad (3.25)$$

which is equivalent to (3.24).

Hence, it can be concluded that the three methods of constructing onesided confidence bands for a simple linear regression model give the same result mathematically. Clearly, (3.13) is relatively simple compared with (3.16) and (3.19) since both (3.16) and (3.19) involve an integration.

# 3.2 Exact two-sided confidence bands

It is also of interest to think about constructing exact two-sided simultaneous confidence bands for a simple linear regression. Recall (3.4), we have the following setting corresponding to the two-sided case that

$$R = \{ \mathbf{t} : |\mathbf{z}^T \mathbf{t}| \le c ||\mathbf{z}||, \text{ all } \mathbf{z} \in \mathcal{Z} \},$$
(3.26)

where  $\mathbf{t} = \mathbf{N}/\hat{\sigma}$ , N has the  $N_2(\mathbf{0}, \sigma^2 I)$  distribution,  $\hat{\sigma}$  is the usual unbiased estimator of unknown  $\sigma$  and has the  $\sigma \sqrt{\chi_{\nu}^2/\nu}$  distribution with  $\nu$  degrees of freedom, c is a critical value, and

$$\mathcal{Z} = \{ \mathbf{z} : |z_1| \ge q ||\mathbf{z}|| \},\tag{3.27}$$

where q is a non-negative constant.



Figure 3.5: For the method following Bohrer (1973) in two-sided case

# 3.2.1 Method following the idea of Bohrer (1973)

R is shown in Figure 3.5. Since R has a symmetric structure, the probability  $P\{t \in R\}$  equals four times the summation of the probabilities  $P\{t \in R_1\}$  and  $P\{t \in R_2\}$ , where

$$\begin{aligned}
\theta^{*} &= \cos^{-1} q, \\
R_{1} &= \{ \mathbf{t} : \|\mathbf{t}\| \le c, 0 < \theta_{\mathbf{t}} < \theta^{*} \}, \\
R_{2} &= \{ \mathbf{t} : \|\mathbf{t}\| \cos(\theta_{\mathbf{t}} - \theta^{*}) \le c, \theta^{*} < \theta_{\mathbf{t}} < \frac{\pi}{2} \}, \end{aligned}$$
(3.28)

 $\theta_t$  is the angle between t and the  $z_1$  axis.

Note that  $||\mathbf{N}||$  is independent of  $\hat{\sigma}$  by studying the least squares theory and  $||\mathbf{t}||^2/2$  has the *F* distribution with 2 and  $\nu$  degrees of freedom. Also, note that  $||\mathbf{t}||$  is independent of  $\theta_t$ , which has been shown previously. Therefore, we have

$$P_{B}\{\mathbf{t} \in R\} = 4\left(P\{\mathbf{t} \in R_{1}\} + P\{\mathbf{t} \in R_{2}\}\right)$$

$$= 4\left(P\{\|\mathbf{t}\| \le c, 0 < \theta_{\mathbf{t}} < \theta^{*}\} + P\{\|\mathbf{t}\| \cos(\theta_{\mathbf{t}} - \theta^{*}) \le c, \theta^{*} < \theta_{\mathbf{t}} < \frac{\pi}{2}\}\right)$$

$$= 4\left(\frac{\theta^{*}}{2\pi}F_{2,\nu}(\frac{c^{2}}{2}) + \int_{\theta^{*}}^{\frac{\pi}{2}}\frac{1}{2\pi}F_{2,\nu}(\frac{c^{2}}{2\cos^{2}(\theta - \theta^{*})})d\theta\right)$$

$$= \frac{2\theta^{*}}{\pi}F_{2,\nu}(\frac{c^{2}}{2}) + \frac{2}{\pi}\int_{0}^{\frac{\pi}{2}-\theta^{*}}F_{2,\nu}(\frac{c^{2}}{2\cos^{2}\theta})d\theta.$$
(3.29)

)

Note that this method agrees with that of Wynn and Bloomfield (1971).

# 3.2.2 Algebraical method

According to (3.26) and (3.27), R has the alternative form

$$R = \left\{ \mathbf{t} : \sup_{\mathbf{z} \in \mathcal{Z}} \frac{|\mathbf{z}^T \mathbf{t}|}{||\mathbf{z}||} \le c \right\},\tag{3.30}$$

where the supreme can be found directly and explicitly.

Lemma 3.2.1 Under the notations of  $\theta_t$  and  $\theta^*,$  we have

$$\sup_{\mathbf{z}\in\mathcal{Z}}\frac{|\mathbf{z}^T\mathbf{t}|}{\|\mathbf{z}\|} = \begin{cases} \|\mathbf{t}\| & \text{if } \theta_{\mathbf{t}}\in[0,\theta^*]\cup[\pi-\theta^*,\pi+\theta^*] \\ & \cup[2\pi-\theta^*,2\pi], \\ \|\mathbf{t}\||\cos(\theta_{\mathbf{t}}-\theta^*)| & \text{if } \theta_{\mathbf{t}}\in[\theta^*,\frac{\pi}{2}]\cup[\pi+\theta^*,\frac{3\pi}{2}], \\ \|\mathbf{t}\||\cos(\pi-\theta_{\mathbf{t}}-\theta^*)| & \text{if } \theta_{\mathbf{t}}\in[\frac{\pi}{2},\pi-\theta^*]\cup[\frac{3\pi}{2},2\pi-\theta^*]. \end{cases}$$

The proof of Lemma 3.2.1 is very similar with that of Lemma 3.1.2. #

By applying Lemma 3.2.1, we have

1

$$P_{A}\{t \in R\} = 2 \cdot \frac{2\theta^{*}}{2\pi} P\{\|t\| \le c\} + \int_{\theta^{*}}^{\frac{\pi}{2}} \frac{1}{2\pi} P\{\|t\| \| \cos(\theta - \theta^{*})\| \le c\} d\theta + \int_{\pi + \theta^{*}}^{\frac{3\pi}{2}} \frac{1}{2\pi} P\{\|t\| \| \cos(\theta - \pi - \theta^{*})\| \le c\} d\theta + \int_{\pi + \theta^{*}}^{\pi - \theta^{*}} \frac{1}{2\pi} P\{\|t\| \| \cos(\pi - \theta - \theta^{*})\| \le c\} d\theta + \int_{\frac{3\pi}{2}}^{2\pi - \theta^{*}} \frac{1}{2\pi} P\{\|t\| | \cos(2\pi - \theta - \theta^{*})\| \le c\} d\theta$$
(3.31)  
$$= \frac{2\theta^{*}}{\pi} F_{2,\nu}(\frac{c^{2}}{2}) + 2 \int_{0}^{\frac{\pi}{2} - \theta^{*}} \frac{1}{2\pi} F_{2,\nu}(\frac{c^{2}}{2\cos^{2}\theta}) d\theta - 2 \int_{\frac{\pi}{2} - \theta^{*}}^{0} \frac{1}{2\pi} F_{2,\nu}(\frac{c^{2}}{2\cos^{2}\theta}) d\theta = \frac{2\theta^{*}}{\pi} F_{2,\nu}(\frac{c^{2}}{2}) + \frac{2}{\pi} \int_{0}^{\frac{\pi}{2} - \theta^{*}} F_{2,\nu}(\frac{c^{2}}{2\cos^{2}\theta}) d\theta.$$
(3.32)

# 3.2.3 Tubular neighborhood method

R in (3.30) can be further written as

$$R = \left\{ \mathbf{t} : \sup_{\mathbf{z} \in \mathcal{Z}} \frac{|\mathbf{z}^T \mathbf{t}|}{\|\mathbf{z}\| \|\mathbf{t}\|} \le \frac{c}{\|\mathbf{t}\|} \right\}.$$
 (3.33)

Then the confidence level is equal to

$$P_{TN} \{ \mathbf{t} \in R \}$$

$$= 1 - P \left\{ \sup_{\mathbf{z} \in \mathcal{Z}} \frac{|\mathbf{z}^T \mathbf{t}|}{\|\mathbf{z}\| \|\mathbf{t}\|} > \frac{c}{\|\mathbf{t}\|} \right\}$$

$$= 1 - \int_{\frac{c^2}{2}}^{\infty} P \left\{ \sup_{\mathbf{z} \in \mathcal{Z}} \frac{|\mathbf{z}^T \mathbf{t}|}{\|\mathbf{z}\| \|\mathbf{t}\|} > \frac{c}{\sqrt{2w}} \right\} \cdot dF_{2,\nu}(w). \quad (3.34)$$

Note that the supreme in (3.34) can not be larger than one. Let  $0 < h = c/\sqrt{2w} < 1$  such that  $\cos^{-1} h \in (0, \pi/2)$ . The set

$$\mathbf{E}(h) = \left\{ \mathbf{t} : \sup_{\mathbf{z} \in \mathcal{Z}} \frac{|\mathbf{z}^T \mathbf{t}|}{\|\mathbf{z}\| \|\mathbf{t}\|} > h \right\}$$



Figure 3.6: For the tubular neighborhood method in two-sided case

consists of two opposite circular cones in  $\mathcal{R}^2$  with their common vertex at the origin, symmetrically containing the smaller cones graphically produced by  $\mathcal{Z}$  with the angle  $\cos^{-1} h$  between the boundaries. So we have E(h) equal to

$$\begin{aligned} \{ \mathbf{t} : \theta_{\mathbf{t}} \in [0, \theta^* + \cos^{-1} h] \cup [\pi - \theta^* - \cos^{-1} h] & \text{if} \quad \theta^* + \cos^{-1} h < \frac{\pi}{2}, \\ \cup [\pi + \theta^* + \cos^{-1} h] \cup [2\pi - \theta^* - \cos^{-1} h] \} \\ & \{ \mathbf{t} : \theta_{\mathbf{t}} \in [0, 2\pi] \} & \text{if} \quad \theta^* + \cos^{-1} h \ge \frac{\pi}{2}. \end{aligned}$$

Note that

$$\theta^* + \cos^{-1}(\frac{c}{\sqrt{2w}}) < \frac{\pi}{2} \iff w < \frac{c^2}{2b^2},$$

where  $b = \sqrt{1-q^2}$ . Since  $\theta_t$  was proven to be uniformly distributed in Section 3.1, we have, for  $c^2/2 \le w < c^2/(2b^2)$ ,

$$P\{t \in E(h)\} = P\{\theta_{t} \in [0, \theta^{*} + \cos^{-1}(\frac{c}{\sqrt{2w}})] \cup [\pi - \theta^{*} - \cos^{-1}(\frac{c}{\sqrt{2w}})] \cup [\pi + \theta^{*} + \cos^{-1}(\frac{c}{\sqrt{2w}})] \cup [2\pi - \theta^{*} - \cos^{-1}(\frac{c}{\sqrt{2w}})]\} = 4 \int_{0}^{\theta^{*} + \cos^{-1}(\frac{c}{\sqrt{2w}})} \frac{1}{2\pi} d\theta, \qquad (3.35)$$

52

and, for  $w \ge c^2/(2b^2)$ ,

$$P\{t \in E(h)\} = P\{\theta_t \in [0, 2\pi]\} = 1.$$
(3.36)

In connection with (3.34), the confidence level is equal to

$$1 \quad - \quad \int_{\frac{c^2}{2b^2}}^{\frac{c^2}{2b^2}} \int_{0}^{\theta^* + \cos^{-1}(\frac{c}{\sqrt{2w}})} \frac{4}{2\pi} d\theta \cdot dF_{2,\nu}(w) - \int_{\frac{c^2}{2b^2}}^{\infty} 1 \cdot dF_{2,\nu}(w). \quad (3.37)$$

#### 3.2.4 Equivalence of the formulae

We are also interested in finding the equivalence of the formulae (3.29), (3.32) and (3.37) corresponding to the three methods respectively. Obviously (3.29) and (3.32) are the same. So our attention moves to show that (3.32) is equivalent to (3.37).

Consider the double integral in (3.37). It is further equal to

$$\int_{\frac{c^2}{2b^2}}^{\frac{c^2}{2b^2}} \frac{2}{\pi} \Big[ \theta^* + \cos^{-1}(\frac{c}{\sqrt{2w}}) \Big] dF_{2,\nu}(w)$$

$$= \frac{2\theta^*}{\pi} \Big[ F_{2,\nu}(\frac{c^2}{2b^2}) - F_{2,\nu}(\frac{c^2}{2}) \Big]$$

$$+ \frac{2}{\pi} \int_{\frac{c^2}{2}}^{\frac{c^2}{2b^2}} \int_{0}^{\cos^{-1}(\frac{c}{\sqrt{2w}})} d\theta \cdot dF_{2,\nu}(w).$$
(3.38)

Note that  $\theta^* = \cos^{-1} q$  and  $b = \sqrt{1 - q^2}$  imply  $\cos^{-1} b = \pi/2 - \theta^*$ . Thus, the last term on the right-hand side in (3.38) can be further written by changing the order of the integrations as

$$\frac{2}{\pi} \int_{0}^{\cos^{-1}b} \int_{\frac{c^{2}}{2\cos^{2}\theta}}^{\frac{c^{2}}{2b^{2}}} dF_{2,\nu}(w) \cdot d\theta$$

$$= \frac{2}{\pi} \int_{0}^{\frac{\pi}{2} - \theta^{*}} \left[ F_{2,\nu}(\frac{c^{2}}{2b^{2}}) - F_{2,\nu}(\frac{c^{2}}{2\cos^{2}\theta}) \right] d\theta$$

$$= (1 - \frac{2\theta^{*}}{\pi}) F_{2,\nu}(\frac{c^{2}}{2b^{2}}) - \frac{2}{\pi} \int_{0}^{\frac{\pi}{2} - \theta^{*}} F_{2,\nu}(\frac{c^{2}}{2\cos^{2}\theta}) d\theta. \quad (3.39)$$

Substitute (3.39) into (3.38), and then we have (3.38) further equal to

$$F_{2,\nu}(\frac{c^2}{2b^2}) - \frac{2\theta^*}{\pi} F_{2,\nu}(\frac{c^2}{2}) - \frac{2}{\pi} \int_0^{\frac{\pi}{2} - \theta^*} F_{2,\nu}(\frac{c^2}{2\cos^2\theta}) d\theta.$$
(3.40)

By replacing the double integral in (3.37) by (3.40), in connection with that

$$1 - \int_{\frac{c^2}{2b^2}}^{\infty} 1 \cdot dF_{2,\nu}(w) = F_{2,\nu}(\frac{c^2}{2b^2}),$$

we have (3.37) equal to

$$\frac{2\theta^*}{\pi}F_{2,\nu}(\frac{c^2}{2}) + \frac{2}{\pi}\int_0^{\frac{\pi}{2}-\theta^*}F_{2,\nu}(\frac{c^2}{2\cos^2\theta})d\theta, \qquad (3.41)$$

which is the same as (3.29) and (3.32). Consequently, the equivalence of the three computational formulae is obtained.

# Chapter 4

# Exact simultaneous confidence bands for a multiple linear regression over an ellipsoidal region

This chapter continues to discuss the construction of exact one-sided and twosided hyperbolic-shape simultaneous confidence bands for a multiple linear regression model over an ellipsoid that is centered at the point of the means of the predictor variables using the same methods as shown in last chapter. Also, the equivalence of the computational formulae of the methods is given for both one-sided and two-sided cases at last.

### 4.1 Exact one-sided confidence bands

Bohrer (1973) presented a method of constructing an exact one-sided confidence band for a multiple linear regression model by evaluating a multivariate t probability.

Consider an one-sided hyperbolic-shape simultaneous confidence band e.g., with upper bound, for a classical normal-error multiple linear regression model

$$\mathbf{x}^{T}\boldsymbol{\beta} \leq \mathbf{x}^{T}\hat{\boldsymbol{\beta}} + r\hat{\sigma}\sqrt{\mathbf{x}^{T}(\boldsymbol{X}^{T}\boldsymbol{X})^{-1}\mathbf{x}} \qquad \mathbf{x} \in \mathcal{X},$$
(4.1)

where  $\hat{\boldsymbol{\beta}}$  is the maximum likelihood estimator of the *p*-dimensional parameter vector  $\boldsymbol{\beta}, \hat{\sigma}$  is the usual unbiased estimator of  $\sigma$  which is the standard variance of the independent and identically distributed random errors in the linear regression model, the  $n \times p$  design matrix X can be expressed by  $X = (\mathbf{1}, X_{(1)})$ , where  $\mathbf{1}$  is the vector containing n ones,  $X_{(1)}$  is the  $n \times (p-1)$  matrix containing the observed predictor variables, and r is a non-negative critical value.

Consider the restricted region of the predictor space,  $\mathcal{X}$ , which has the form given by

$$\mathcal{X} = \{ \mathbf{x} : \mathbf{x}^T V \mathbf{u} (\mathbf{u}^T V \mathbf{u})^{-1} \mathbf{u}^T V \mathbf{x} \ge c^2 \mathbf{x}^T V \mathbf{x} \},$$
(4.2)

where  $V = (X^T X)^{-1}$ , **u** is a *p*-dimensional vector such that  $\mathbf{u}^T V \mathbf{u} = 1$ , *c* is a non-negative constant. Define  $\bar{x}_{.j} = \frac{1}{n} \sum_{i=1}^n x_{ij}, j = 2, \ldots, p$  and  $\bar{\mathbf{x}}_{(1)} = (\bar{x}_{.2}, \ldots, \bar{x}_{.p})$ . Then  $\bar{\mathbf{x}}_{(1)}$  is the mean vector of the observed predictor variables. And, we have

$$X^T X = \begin{pmatrix} n & n \bar{\mathbf{x}}_{(1)}^T \\ n \bar{\mathbf{x}}_{(1)} & X_{(1)}^T X_{(1)} \end{pmatrix}$$

Furthermore, the inverse is given by

$$V = (X^T X)^{-1} = \begin{pmatrix} \frac{1}{n} (1 + \bar{\mathbf{x}}_{(1)}^T S^{-1} \bar{\mathbf{x}}_{(1)}) & -\frac{1}{n} \bar{\mathbf{x}}_{(1)}^T S^{-1} \\ -\frac{1}{n} S^{-1} \bar{\mathbf{x}}_{(1)} & \frac{1}{n} S^{-1} \end{pmatrix},$$

where

$$nS = (X_{(1)}^T - \bar{\mathbf{x}}_{(1)} \mathbf{1}^T) (X_{(1)} - \mathbf{1} \bar{\mathbf{x}}_{(1)}^T)$$
  
=  $X_{(1)}^T X_{(1)} - n \bar{\mathbf{x}}_{(1)} \bar{\mathbf{x}}_{(1)}^T.$ 

Let  $\mathbf{u} = \sqrt{n}(1, \bar{\mathbf{x}}_{(1)}^T)^T$  so that  $\mathbf{u}^T V \mathbf{u} = 1$  and  $\mathbf{u}^T V \mathbf{x} = 1/\sqrt{n}$ . In addition,

$$\mathbf{x}^{T} V \mathbf{x} = 1 + (\mathbf{x}_{(1)} - \bar{\mathbf{x}}_{(1)})^{T} S^{-1} (\mathbf{x}_{(1)} - \bar{\mathbf{x}}_{(1)}),$$

where  $\mathbf{x}_{(1)}$  is defined such that  $\mathbf{x} = (1, \mathbf{x}_{(1)}^T)^T$ . Hence, (4.2) can be further written as

$$\begin{aligned} \mathcal{X} &= \left\{ \mathbf{x} : c^{2} [1 + (\mathbf{x}_{(1)} - \bar{\mathbf{x}}_{(1)})^{T} S^{-1} (\mathbf{x}_{(1)} - \bar{\mathbf{x}}_{(1)})] \le 1 \right\} \\ &= \left\{ \mathbf{x} : (\mathbf{x}_{(1)} - \bar{\mathbf{x}}_{(1)})^{T} S^{-1} (\mathbf{x}_{(1)} - \bar{\mathbf{x}}_{(1)}) \le \frac{1 - c^{2}}{c^{2}} \right\}, \end{aligned}$$
(4.3)

which is, in fact, an  $\bar{\mathbf{x}}_{(1)}$ -centered ellipsoid in the predictor space, and whose size can be controlled by  $(1 - c^2)/c^2$ .

Next, we transform the ellipsoidal region  $\mathcal{X}$  to a corresponding region of our interest. For a **u**, there exists a  $p \times (p-1)$  matrix U such that  $U^T VU = I_{p-1}$  and  $\mathbf{u}^T VU = 0$ . So **u** and the columns of U, which are linearly independent, form an orthogonal basis of the *p*-dimensional predictor space. Define

$$\mathbf{z} = \begin{pmatrix} z_1 \\ \mathbf{z}_{(1)} \end{pmatrix} = \begin{pmatrix} \mathbf{u}^T \\ U^T \end{pmatrix} V \mathbf{x}.$$
(4.4)

We have

$$\mathbf{x}^{T} V \mathbf{x} = \mathbf{x}^{T} V(\mathbf{u} \ U)(\mathbf{u} \ U)^{-1} V^{-1} [(\mathbf{u} \ U)^{T}]^{-1} (\mathbf{u} \ U)^{T} V \mathbf{x}$$
$$= \left[ \begin{pmatrix} \mathbf{u}^{T} \\ U^{T} \end{pmatrix} V \mathbf{x} \right]^{T} \left[ (\mathbf{u} \ U)^{T} V(\mathbf{u} \ U) \right]^{-1} \begin{pmatrix} \mathbf{u}^{T} \\ U^{T} \end{pmatrix} V \mathbf{x}$$
$$= \begin{pmatrix} z_{1} \\ \mathbf{z}_{(1)} \end{pmatrix}^{T} \begin{pmatrix} z_{1} \\ \mathbf{z}_{(1)} \end{pmatrix} = \|\mathbf{z}\|^{2}.$$
(4.5)

Since  $z_1 = \mathbf{u}^T V \mathbf{x} = 1/\sqrt{n} > 0$  and  $\mathbf{u}^T V \mathbf{u} = 1$ , therefore, the region  $\mathcal{X}$  given in (4.2) can be transformed to the following region

$$E(c) = \{ \mathbf{z} : z_1 \ge c \| \mathbf{z} \| \}.$$
(4.6)

Consequently, any  $\mathbf{x}$  belonging to  $\mathcal{X}$  definitely has a corresponding  $\mathbf{z}$  belonging to  $\mathbf{E}(c)$ ; conversely any  $\mathbf{z} \in \mathbf{E}(c)$  corresponds to an  $\mathbf{x} \in \mathcal{X}$  as well.

Now, we consider the one-sided confidence band given in (4.1). It has the coverage probability given by

$$\mathbf{P}\Big\{\sup_{\mathbf{x}\in\mathcal{X}}\frac{\mathbf{x}^{T}(\boldsymbol{\beta}-\hat{\boldsymbol{\beta}})}{\hat{\sigma}\sqrt{\mathbf{x}^{T}(\boldsymbol{X}^{T}\boldsymbol{X})^{-1}\mathbf{x}}}\leq r\Big\},\$$

which is equal to

$$\mathbb{P}\Big\{\sup_{\mathbf{x}\in\mathcal{X}}\frac{\mathbf{x}^T V(\mathbf{u}\ U)(\mathbf{u}\ U)^{-1}V^{-1}(\boldsymbol{\beta}-\hat{\boldsymbol{\beta}})}{\hat{\sigma}(\mathbf{x}^T V \mathbf{x})^{1/2}} \leq r\Big\}.$$

By recalling the definition of  $\mathbf{z}$  in (4.4) and the derivation in (4.5), in connection with the fact that an  $\mathbf{x} \in \mathcal{X}$  one-to-one corresponds to a  $\mathbf{z} \in E(c)$ , then above probability is equivalent to

$$\mathbf{\tilde{P}}\Big\{\sup_{\mathbf{z}\in\mathbf{E}(c)}\frac{\mathbf{z}^{T}\mathbf{t}}{\|\mathbf{z}\|}\leq r\Big\},$$
(4.7)

where  $\mathbf{t} = \mathbf{N}/\hat{\sigma}$  with  $\mathbf{N} = (\mathbf{u} \ U)^{-1} V^{-1} (\boldsymbol{\beta} - \hat{\boldsymbol{\beta}}) = (\mathbf{u} \ U)^T (\boldsymbol{\beta} - \hat{\boldsymbol{\beta}})$ . Note that N has the  $N_p(\mathbf{0}, \sigma^2 I)$  distribution,  $\hat{\sigma}$  has the  $\sigma \sqrt{\chi_{\nu}^2/\nu}$  distribution, and they are independent by studying the least squares theory. Thus,  $\mathbf{t}$  has a so-called multivariate t distribution with  $\nu = n - p$  degrees of freedom. This is the starting point of the three methods given in the rest of this section.

### 4.1.1 Method of Bohrer (1973)

Define a *p*-dimensional vector  $\mathbf{v}$  in terms of the polar coordinates  $R_{\mathbf{v}}$  and  $\boldsymbol{\theta}_{\mathbf{v}} = (\theta_{\mathbf{v}1}, \dots, \theta_{\mathbf{v}, p-1})$  by

$$\begin{cases} v_1 = R_{\mathbf{v}} \cos \theta_{\mathbf{v}1}, \\ v_2 = R_{\mathbf{v}} \sin \theta_{\mathbf{v}1} \cos \theta_{\mathbf{v}2}, \\ v_3 = R_{\mathbf{v}} \sin \theta_{\mathbf{v}1} \sin \theta_{\mathbf{v}2} \cos \theta_{\mathbf{v}3}, \\ \cdots \\ v_{p-1} = R_{\mathbf{v}} \sin \theta_{\mathbf{v}1} \sin \theta_{\mathbf{v}2} \cdots \sin \theta_{\mathbf{v},p-2} \cos \theta_{\mathbf{v},p-1}, \\ v_p = R_{\mathbf{v}} \sin \theta_{\mathbf{v}1} \sin \theta_{\mathbf{v}2} \cdots \sin \theta_{\mathbf{v},p-2} \sin \theta_{\mathbf{v},p-1}, \end{cases}$$

where

$$\begin{cases} 0 \le \theta_{\mathbf{v}1} \le \pi, \\ 0 \le \theta_{\mathbf{v}2} \le \pi, \\ \dots \\ 0 \le \theta_{\mathbf{v},p-2} \le \pi, \\ 0 \le \theta_{\mathbf{v},p-1} \le 2\pi, \\ R_{\mathbf{v}} \ge 0. \end{cases}$$

Furthermore, the Jacobian of the transformation from  $\mathbf{v}$  to the polar coordinates is

$$J| = R_{\mathbf{v}}^{p-1} \sin^{p-2} \theta_{\mathbf{v}1} \sin^{p-3} \theta_{\mathbf{v}2} \cdots \sin \theta_{\mathbf{v},p-2}.$$

Also, note that

$$\mathbf{z}^T \mathbf{t} = R_{\mathbf{z}} R_{\mathbf{t}} f_{p-1}, \tag{4.8}$$

where  $f_1 = \cos(\theta_{\mathbf{z},p-1} - \theta_{\mathbf{t},p-1})$  and

$$f_j = \cos \theta_{\mathbf{z}, p-j} \cos \theta_{\mathbf{t}, p-j} + f_{j-1} \sin \theta_{\mathbf{z}, p-j} \sin \theta_{\mathbf{t}, p-j}$$

for j = 2, ..., p - 1.

The probability in (4.7) can be alternatively written as  $P\{t \in A_r(c)\}$ , where

$$A_r = A_r(c) = \{ \mathbf{t} : \mathbf{z}^T \mathbf{t} \le r \| \mathbf{z} \|, \text{ all } \mathbf{z} \text{ in } \mathbf{E}(c) \}$$

$$(4.9)$$

with E(c) defined in (4.6) which is a spherical cone with the vertex at the origin.  $A_{\tau}(c)$  and E(c) are graphically shown in Figure 4.1.

**Lemma 4.1.1** Define  $\theta^* = \cos^{-1} c$ , then  $A_r$  is partitioned by the following three disjoint sets:

$$T_{1} = \{ \mathbf{t} : 0 \le \theta_{t1} \le \theta^{*}, R_{t} \le r \},$$

$$T_{2} = \{ \mathbf{t} : \theta_{t1} - \theta^{*} \in (0, \frac{\pi}{2}], R_{t} \cos(\theta_{t1} - \theta^{*}) \le r \},$$

$$T_{3} = \{ \mathbf{t} : \theta^{*} + \frac{\pi}{2} < \theta_{t1} \le \pi \}.$$
(4.10)

*Proof.* When  $\mathbf{t} \in T_1$ , then  $t_1 = R_t \cos \theta_{t1} \ge R_t \cos \theta^* = c \|\mathbf{t}\|$  so that  $\mathbf{t} \in \mathbf{E}(c)$ , which in connection with the fact that  $R_t^T R_t \le r \|\mathbf{t}\|$  implies  $\mathbf{t} \in A_r(c)$ . When  $\mathbf{t} \in T_2$ , since  $\mathbf{z} \in \mathbf{E}(c)$ , then  $0 \le \theta_{\mathbf{z}1} \le \theta^*$  so that  $R_\mathbf{z}R_\mathbf{t}\cos(\theta_{\mathbf{t}1}-\theta_{\mathbf{z}1}) \le R_\mathbf{z}R_\mathbf{t}\cos(\theta_{\mathbf{t}1}-\theta^*) \le r \|\mathbf{z}\|$ , which implies that  $\mathbf{t} \in A_r(c)$ . When  $\mathbf{t} \in T_3$ , obviously  $\cos(\theta_{\mathbf{t}1}-\theta_{\mathbf{z}1}) < 0$  which implies  $\mathbf{t} \in A_r(c)$ . Hence  $\cup_{j=1}^3 T_j \subset A_r$ .

Conversely, when  $\mathbf{t} \in A_r \cap {\mathbf{t} : 0 \le \theta_{t1} \le \theta^*}$ , then  $t_1 = R_t \cos \theta_{t1} \ge c \|\mathbf{t}\|$ so that  $\mathbf{t} \in \mathbf{E}(c)$  and hence we obtain  $R_t \le r$  from  $\mathbf{t}^T \mathbf{t} \le r \|\mathbf{t}\|$ . Therefore,  $\mathbf{t} \in T_1$ . When  $\mathbf{t} \in A_r \cap {\mathbf{t} : \theta_{t1} - \theta^* \in (0, \pi/2)}$ , since  $\mathbf{z} \in \mathbf{E}(c)$ , we have



Figure 4.1: For the method of Bohrer (1973)

 $R_{\mathbf{t}}\cos(\theta_{\mathbf{t}1}-\theta^*) \leq r$ . So  $\mathbf{t} \in T_2$ . And finally  $\mathbf{t} \in A_r \cap \{\mathbf{t}: \theta^* + \pi/2 < \theta_{\mathbf{t}1} \leq \pi\}$ obviously implies  $\mathbf{t} \in T_3$ . Hence  $A_r \subset \cup_{j=1}^3 T_j$ . Overall,  $A_r$  is composed of  $T_j, j = 1, 2, 3$ . #

Applying Lemma 4.1.1, we have

$$P\{\mathbf{t} \in A_r\} = \sum_{j=1}^{3} P\{\mathbf{t} \in T_j\}.$$
(4.11)

Recall that  $\mathbf{t} = \mathbf{N}/\hat{\sigma}$ , where  $\mathbf{N} \sim N_p(\mathbf{0}, \sigma^2 I)$ , and  $\hat{\sigma} \sim \sigma \sqrt{\chi_{\nu}^2/\nu}$ . Moreover, **N** is independent of  $\hat{\sigma}$ . Thus  $\|\mathbf{t}\|^2/p = (\|\mathbf{N}/\sigma\|^2/p)/(\hat{\sigma}^2/\sigma^2) \sim F_{p,\nu}$ , where  $F_{p,\nu}$  is the F distribution with p and  $\nu$  degrees of freedom. Also  $\mathbf{t}$  can be expressed in terms of the polar coordinates  $R_{\mathbf{t}}$  and  $\theta_{\mathbf{t}} = (\theta_{\mathbf{t}1}, \ldots, \theta_{\mathbf{t},p-1})$ , and **N** can be expressed in terms of  $R_{\mathbf{N}}$  and  $\theta_{\mathbf{N}} = (\theta_{\mathbf{N}1}, \ldots, \theta_{\mathbf{N},p-1})$ . Note that  $\theta_{\mathbf{t}1}, \ldots, \theta_{\mathbf{t},p-1}$  and  $\theta_{\mathbf{N}1}, \ldots, \theta_{\mathbf{N},p-1}$  denote the same p-1 angles because  $\mathbf{N}/\hat{\sigma}$ does not change the location of  $\mathbf{N}$ . One can easily find the joint density function of  $R_{\mathbf{N}}$  and  $\theta_{\mathbf{N}}$  via the transformation of random variables in connection with the fact that  $\mathbf{N}$  has a p-variate standard normal distribution. By finding the individual marginal density functions, we find that the joint density is equal to the product of the individual marginal densities which implies  $R_{\mathbf{N}}$  is independent of  $\theta_{\mathbf{N}j}, j = 1, \ldots, p-1$ . Thus, the independence between  $R_t$  and  $\theta_{tj}, j = 1, \dots, p-1$  can be obtained. In particular,  $\theta_{t1}$  has the marginal density function

$$f_1(\theta_{t1}) = k_1 \sin^{p-2} \theta_{t1}, \tag{4.12}$$

where  $k_1$  is normalizing constant such that  $\int_0^{\pi} k_1 \sin^{p-2} \theta d\theta = 1$ .

Based on the analysis above, we have

$$P\{\mathbf{t} \in T_1\} = P\{0 \le \theta_{\mathbf{t}1} \le \theta^*, R_{\mathbf{t}} \le r\}$$
$$= \int_0^{\theta^*} k_1 \sin^{p-2} \theta d\theta \cdot P\{R_{\mathbf{t}} \le r\}$$
$$= \int_0^{\theta^*} k_1 \sin^{p-2} \theta d\theta \cdot F_{p,\nu}(\frac{r^2}{p}), \qquad (4.13)$$
$$P\{\mathbf{t} \in T_2\} = P\{\theta^* + \frac{\pi}{r} < \theta_{\mathbf{t}1} \le \pi\}$$

$$= \int_{\theta^* + \frac{\pi}{2}}^{\pi} k_1 \sin^{p-2} \theta d\theta$$
$$= \int_{0}^{\frac{\pi}{2} - \theta^*} k_1 \sin^{p-2} \theta d\theta, \qquad (4.14)$$
$$P\{t \in T_0\} = P\{0 < \theta_0 - \theta^* \le \frac{\pi}{2}, R_{\rm e} \cos(\theta_0 - \theta^*) \le r\}$$

$$P\{\mathbf{t} \in T_2\} = P\{0 < \theta_{t1} - \theta^* \le \frac{\pi}{2}, R_t \cos(\theta_{t1} - \theta^*) \le r\}$$
$$= \int_{\theta^*}^{\theta^* + \frac{\pi}{2}} k_1 \sin^{p-2} \theta \cdot P\{R_t \cos(\theta - \theta^*) \le r\} d\theta$$
$$= \int_0^{\frac{\pi}{2}} k_1 \sin^{p-2}(\theta + \theta^*) \cdot F_{p,\nu}(\frac{r^2}{p \cos^2 \theta}) d\theta, \qquad (4.15)$$

where  $F_{p,\nu}$  stands for the F cumulative distribution function with p and  $\nu$  degrees of freedom.

Consequently, by (4.11), the confidence level of the one-sided confidence band based on the method of Bohrer (1973) is given by

$$P_{B} = \int_{0}^{\theta^{*}} k_{1} \sin^{p-2}\theta d\theta \cdot F_{p,\nu}(\frac{r^{2}}{p}) + \int_{0}^{\frac{\pi}{2}-\theta^{*}} k_{1} \sin^{p-2}\theta d\theta + \int_{0}^{\frac{\pi}{2}} k_{1} \sin^{p-2}(\theta + \theta^{*}) \cdot F_{p,\nu}(\frac{r^{2}}{p \cos^{2}\theta}) d\theta.$$
(4.16)
## 4.1.2 Algebraical method

ç

Recalling (4.7), the confidence level of the band has the form

$$P\Big\{\sup_{\mathbf{z}\in E(c)}\frac{\mathbf{z}^{T}\mathbf{t}}{\|\mathbf{z}\|} \le r\Big\},\tag{4.17}$$

where r is a critical value, and

$$E(c) = \{ \mathbf{z} : z_1 \ge c \| \mathbf{z} \| \}$$
 (4.18)

with c non-negative.

**Lemma 4.1.2** Let  $t_1$  be the first element of  $\mathbf{t}$ ,  $\mathbf{t}_{(1)}$  be the (p-1)-dimensional vector containing the rest elements of  $\mathbf{t}$  in order. Then we have

$$\sup_{\mathbf{z}\in E(c)} \frac{\mathbf{z}^T \mathbf{t}}{\|\mathbf{z}\|} = \begin{cases} \|\mathbf{t}\| & \text{if } \mathbf{t}\in E(c), \\ \frac{t_1 + \frac{1}{q}\|\mathbf{t}_{(1)}\|}{\sqrt{1 + \frac{1}{q^2}}} & \text{if } \mathbf{t}\notin E(c), \end{cases}$$

where  $q = \sqrt{c^2/(1-c^2)}$ .

*Proof.* Note that it is obvious when  $\mathbf{t} \in \mathbf{E}(c)$ . So our attention focuses on the case when  $\mathbf{t} \notin \mathbf{E}(c)$ . Define  $\mathbf{z} = (z_1, \mathbf{z}_{(1)}^T)^T$  such that

$$E(c) = \{ \mathbf{z} : z_1 > 0, z_1^2 \ge c^2 z_1^2 + c^2 \| \mathbf{z}_{(1)} \|^2 \}$$
  
=  $\{ \mathbf{z} : z_1 \ge q \| \mathbf{z}_{(1)} \| \},$  (4.19)

where q is defined in Lemma 4.1.2.

Consider  $t \notin E(c)$  which leads that  $t_1 < q ||\mathbf{t}_{(1)}||$  from (4.19). For  $t_1 \neq 0$ , define

$$\mathbf{z}^* = \begin{pmatrix} 1\\ \frac{\mathbf{t}_{(1)}/|t_1|}{q||\mathbf{t}_{(1)}/|t_1||} \end{pmatrix},$$

then  $z_1^* = 1$  and  $q \|\mathbf{z}_{(1)}^*\| = 1$  so that  $\mathbf{z}^* \in \mathbf{E}(c)$ . So generally we consider  $\mathbf{z} \in \mathbf{E}(c)$  has the similar form with  $\mathbf{z}^*$  that  $\mathbf{z} = (1, \mathbf{z}_{(1)}^T)^T$  and  $1 \ge q \|\mathbf{z}_{(1)}\|$ . Therefore, we have

$$\frac{\mathbf{z}^{T}\mathbf{t}}{\|\mathbf{z}\|} = \frac{t_{1} + \mathbf{z}_{(1)}^{T}\mathbf{t}_{(1)}}{\sqrt{1 + \|\mathbf{z}_{(1)}\|^{2}}} \\
\leq \frac{t_{1} + \|\mathbf{z}_{(1)}\| \|\mathbf{t}_{(1)}\|}{\sqrt{1 + \|\mathbf{z}_{(1)}\|^{2}}} \\
= \phi t_{1} + \sqrt{1 - \phi^{2}} \|\mathbf{t}_{(1)}\| = f(\phi), \quad (4.20)$$



Figure 4.2: For the algebraical method in one-sided case

where

$$\phi = \frac{1}{\sqrt{1 + \|\mathbf{z}_{(1)}\|^2}} \ge \frac{1}{\sqrt{1 + 1/q^2}}$$

Also, from  $t_1 < q \|\mathbf{t}_{(1)}\|$ , we have

$$t_1 < \frac{1/\sqrt{1+1/q^2}}{\sqrt{1-1/(1+1/q^2)}} \|\mathbf{t}_{(1)}\| \le \frac{\phi}{\sqrt{1-\phi^2}} \|\mathbf{t}_{(1)}\|.$$
(4.21)

So it is clear that  $f(\phi)$  is monotonously decreasing because, by (4.20) and (4.21), we have

$$f'(\phi) = t_1 - \frac{1}{2}(1 - \phi^2)^{-\frac{1}{2}} \cdot 2\phi \|\mathbf{t}_{(1)}\| \le 0.$$

Consequently,

$$f(\phi) \le f(\frac{1}{\sqrt{1+1/q^2}}) = \frac{t_1 + (1/q) \|\mathbf{t}_{(1)}\|}{\sqrt{1+1/q^2}}.$$
 # (4.22)

The probability in (4.17), therefore, can be evaluated straightforward by applying Lemma 4.1.2. We have

$$P\left\{\sup_{\mathbf{z}\in E(c)} \frac{\mathbf{z}^{T}\mathbf{t}}{\|\mathbf{z}\|} \leq r\right\}$$

$$= P\left\{\mathbf{t}\in E(c), \|\mathbf{t}\| \leq r\right\} + P\left\{\mathbf{t}\notin E(c), \frac{qt_{1} + \|\mathbf{t}_{(1)}\|}{\sqrt{q^{2}+1}} \leq r\right\}$$

$$= P\left\{t_{1} \geq q\|\mathbf{t}_{(1)}\|, \|t_{1}\|^{2} + \|\mathbf{t}_{(1)}\|^{2} \leq r^{2}\right\} + P\left\{t_{1} < q\|\mathbf{t}_{(1)}\|, \frac{qt_{1} + \|\mathbf{t}_{(1)}\|}{\sqrt{q^{2}+1}} \leq r\right\}$$

$$= P\left\{R_{\mathbf{t}}^{2} \leq r^{2}\right\} + P\left\{r^{2} < R_{\mathbf{t}}^{2} < \infty, w = \frac{t_{1}}{\|\mathbf{t}_{(1)}\|} \in \left(-\infty, \frac{ar - b\sqrt{R_{\mathbf{t}}^{2} - r^{2}}}{br + a\sqrt{R_{\mathbf{t}}^{2} - r^{2}}}\right)\right\}, \quad (4.23)$$

where  $R_t^2 = t_1^2 + ||\mathbf{t}_{(1)}||^2$ ,  $a = q/\sqrt{q^2 + 1}$ ,  $b = 1/\sqrt{q^2 + 1}$ , and the upper bound of w is obtained by solving the equation set formed by  $||t_1||^2 + ||\mathbf{t}_{(1)}||^2 = r^2$ and  $(qt_1 + ||\mathbf{t}_{(1)}||)/\sqrt{q^2 + 1} = r$ . The accomplishment of the last equality in (4.23) is graphically because the total area of the light shadowed region and the dark shadowed region is equal to the total area of the half circle and the rest light shadowed part in the left top corner. The first probability on the right-hand side of the last equality in (4.23) equals  $F_{p,\nu}(r^2/p)$  which is the F cumulative distribution function with p and  $\nu$  degrees of freedom, and the second probability is further equal to

$$\int_{\frac{\pi^2}{p}}^{\infty} g(w) dF_{p,\nu}(w), \qquad (4.24)$$

where

$$g(w) = \mathbf{P}\Big\{\frac{t_1}{\|\mathbf{t}_{(1)}\|} \le \frac{ar - b\sqrt{pw - r^2}}{br + a\sqrt{pw - r^2}}\Big\}.$$

To evaluate g(w), note that

$$ar - b\sqrt{pw - r^2} \le 0 \iff w \ge r^2/pb^2.$$

For 
$$w \in (r^2/p, r^2/pb^2)$$
,  $(ar - b\sqrt{pw - r^2})/(br + a\sqrt{pw - r^2}) \ge 0$ , then  

$$g(w) = P\{t_1 \le 0\} + P\left\{0 \le \frac{t_1}{\|\mathbf{t}_{(1)}\|} \le \frac{ar - b\sqrt{pw - r^2}}{br + a\sqrt{pw - r^2}}\right\}$$

$$= \frac{1}{2} + \frac{1}{2}P\left\{\frac{\cdot t_1^2}{\|\mathbf{t}_{(1)}\|^2/(p-1)} \le (p-1)\left(\frac{ar - b\sqrt{pw - r^2}}{br + a\sqrt{pw - r^2}}\right)^2\right\}$$

$$= \frac{1}{2} + \frac{1}{2}F_{1,p-1}\left\{(p-1)\left(\frac{ar - b\sqrt{pw - r^2}}{br + a\sqrt{pw - r^2}}\right)^2\right\};$$
(4.25)

r

for  $w \in (r^2/pb^2, \infty)$ ,  $(ar - b\sqrt{pw - r^2})/(br + a\sqrt{pw - r^2}) \le 0$ , then

$$g(w) = P\left\{\frac{t_1^2}{\|\mathbf{t}_{(1)}\|^2} \ge \left(\frac{ar - b\sqrt{pw - r^2}}{br + a\sqrt{pw - r^2}}\right)^2\right\}$$
  
=  $\frac{1}{2} - \frac{1}{2}P\left\{\frac{t_1^2}{\|\mathbf{t}_{(1)}\|^2/(p-1)} \le (p-1)\left(\frac{ar - b\sqrt{pw - r^2}}{br + a\sqrt{pw - r^2}}\right)^2\right\}$   
=  $\frac{1}{2} - \frac{1}{2}F_{1,p-1}\left\{(p-1)\left(\frac{ar - b\sqrt{pw - r^2}}{br + a\sqrt{pw - r^2}}\right)^2\right\},$  (4.26)

where  $a = q/\sqrt{q^2 + 1} = c$ ,  $b = 1/\sqrt{q^2 + 1} = \sqrt{1 - c^2}$ .

## 4.1.3 Tubular neighborhood method

Again from (4.7), the confidence level of the one-sided confidence band can be further written as

$$\begin{aligned}
& P\left\{\sup_{\mathbf{z}\in E(c)}\frac{\mathbf{z}^{T}\mathbf{t}}{\|\mathbf{z}\|} \leq r\right\} \\
&= 1 - \int_{0}^{\infty} P\left\{\sup_{\mathbf{z}\in E(c)}\frac{\mathbf{z}^{T}\mathbf{t}}{\|\mathbf{z}\|\|\mathbf{t}\|} > \frac{r}{\sqrt{pw}}\right\} dF_{p,\nu}(w) \\
&= 1 - \int_{\frac{r^{2}}{p}}^{\infty} P\left\{\sup_{\mathbf{z}\in E(c)}\frac{\mathbf{z}^{T}\mathbf{t}}{\|\mathbf{z}\|\|\mathbf{t}\|} > \frac{r}{\sqrt{pw}}\right\} dF_{p,\nu}(w).
\end{aligned} \tag{4.27}$$

Note that the supreme on the right-hand side of the last equality in (4.27) is no larger than one. Let  $0 < h = r/\sqrt{pw} < 1$  such that  $\cos^{-1} h \in (0, \pi/2)$ , the set

$$\mathbf{E}(h) = \left\{ \mathbf{t} : \sup_{\mathbf{z} \in \mathbf{E}(c)} \frac{\mathbf{z}^T \mathbf{t}}{\|\mathbf{z}\| \|\mathbf{t}\|} > h \right\}$$
(4.28)



Figure 4.3: For the tubular neighborhood method in one-sided case

graphically is a spherical cone with the vertex at the origin and has the angle  $\cos^{-1} h$  between a ray of E(h) and the nearest ray from E(c). By the definition of the polar coordinates,  $P\{t \in E(h)\}$  is equal to  $P\{0 < \theta_{t,1} \le \theta^* + \cos^{-1} h\}$ , and  $||t|| = R_t$  is independent of  $\theta_{t1}$ . Therefore, (4.27) is further equal to

$$1 - \int_{\frac{r^2}{p}}^{\infty} P\{0 < \theta_{t,1} \le \theta^* + \cos^{-1}(\frac{r}{\sqrt{pw}})\} dF_{p,\nu}(w)$$
  
=  $1 - \int_{\frac{r^2}{p}}^{\infty} \int_{0}^{\theta^* + \cos^{-1}(\frac{r}{\sqrt{pw}})} k_1 \sin^{p-2}\theta d\theta \cdot dF_{p,\nu}(w),$  (4.29)

where

$$k_1 = \frac{1}{\int_0^\pi \sin^{p-2}\theta d\theta} \tag{4.30}$$

is the normalizing constant.

## 4.1.4 Equivalence of the formulae

It is of interest to show the equivalence of (4.16), (4.29) and that based on the algebraical method. First, we come to show (4.29) is equivalent to (4.16).

Further write (4.29) as

$$1 - \int_{\frac{r^{2}}{p}}^{\infty} \left( \int_{0}^{\theta^{*}} + \int_{\theta^{*}}^{\theta^{*} + \cos^{-1}(\frac{r}{\sqrt{pw}})} \right) k_{1} \sin^{p-2} \theta d\theta \cdot dF_{p,\nu}(w)$$

$$= 1 - \int_{\frac{r^{2}}{p}}^{\infty} dF_{p,\nu}(w) \int_{0}^{\theta^{*}} k_{1} \sin^{p-2} \theta d\theta$$

$$- \int_{\frac{r^{2}}{p}}^{\infty} \int_{0}^{\cos^{-1}(\frac{r}{\sqrt{pw}})} k_{1} \sin^{p-2}(\theta + \theta^{*}) d\theta \cdot dF_{p,\nu}(w)$$

$$= \left( 1 - \int_{0}^{\theta^{*}} k_{1} \sin^{p-2} \theta d\theta \right) + \int_{0}^{\theta^{*}} k_{1} \sin^{p-2} \theta d\theta \cdot F_{p,\nu}(\frac{r^{2}}{p})$$

$$- \int_{0}^{\frac{\pi}{2}} \int_{\frac{r^{2}}{p\cos^{2}\theta}}^{\infty} k_{1} \sin^{p-2}(\theta + \theta^{*}) dF_{p,\nu}(w) \cdot d\theta$$

$$= \int_{0}^{\theta^{*}} k_{1} \sin^{p-2} \theta d\theta \cdot F_{p,\nu}(\frac{r^{2}}{p}) + \int_{0}^{\frac{\pi}{2}} k_{1} \sin^{p-2}(\theta + \theta^{*}) F_{p,\nu}(\frac{r^{2}}{p\cos^{2}\theta}) d\theta$$

$$+ \left( 1 - \int_{0}^{\theta^{*}} k_{1} \sin^{p-2} \theta d\theta - \int_{0}^{\frac{\pi}{2}} k_{1} \sin^{p-2}(\theta + \theta^{*}) d\theta \right).$$
(4.31)

ŧ

The terms in the big bracket on the right-hand side of the last equality in (4.31) together as a whole is further equal to

$$\left(\int_0^{\pi} -\int_0^{\theta^*} -\int_{\theta^*}^{\theta^* + \frac{\pi}{2}}\right) k_1 \sin^{p-2}\theta d\theta = \int_0^{\frac{\pi}{2} - \theta^*} k_1 \sin^{p-2}\theta d\theta.$$
(4.32)

Substituting (4.32) into (4.31) gives the same formula as (4.16).

Next, we turn to find the equivalence between (4.16) and that got from the algebraical method. Recall (4.23), with  $\theta^*$  defined consistently, the last equality is equal to

$$P\{R_{t}^{2} \leq r^{2}, \theta_{t1} \in [0, \theta^{*}]\} + P\{R_{t} \cos(\theta_{t1} - \theta^{*}) \leq r, \theta_{t1} \in (\theta^{*}, \pi]\}$$

$$= P\{R_{t}^{2} \leq r^{2}, \theta_{t1} \in [0, \theta^{*}]\} + P\{0 \leq R_{t} \cos(\theta_{t1} - \theta^{*}) \leq r, \theta_{t1} \in (\theta^{*}, \pi]\}$$

$$+ P\{R_{t} \cos(\theta_{t1} - \theta^{*}) < 0, \theta_{t1} \in (\theta^{*}, \pi]\}$$

$$= P\{R_{t}^{2} \leq r^{2}, \theta_{t1} \in [0, \theta^{*}]\} + P\{0 \leq R_{t} \cos(\theta_{t1} - \theta^{*}) \leq r, \theta_{t1} \in (\theta^{*}, \theta^{*} + \frac{\pi}{2}]\}$$

$$+ P\{R_{t} \cos(\theta_{t1} - \theta^{*}) < 0, \theta_{t1} \in (\theta^{*} + \frac{\pi}{2}, \pi]\}$$

$$= \int_{0}^{\theta^{*}} k_{1} \sin^{p-2}\theta d\theta \cdot F_{p,\nu}(\frac{r^{2}}{p}) + \int_{\theta^{*}}^{\theta^{*} + \frac{\pi}{2}} k_{1} \sin^{p-2}\theta \cdot F_{p,\nu}(\frac{r^{2}}{p \cos^{2}(\theta - \theta^{*})}) d\theta$$

$$+ \int_{\theta^{*} + \frac{\pi}{2}}^{\pi} k_{1} \sin^{p-2}\theta d\theta \cdot F_{p,\nu}(\frac{r^{2}}{p}) + \int_{0}^{\frac{\pi}{2}} k_{1} \sin^{p-2}(\theta + \theta^{*}) \cdot F_{p,\nu}(\frac{r^{2}}{p \cos^{2}\theta}) d\theta$$

$$+ \int_{0}^{\frac{\pi}{2} - \theta^{*}} k_{1} \sin^{p-2}\theta d\theta. \qquad (4.33)$$

Obviously, (4.33) is the same as (4.16). So a conclusion can be drawn that the three methods give the same computational formulae.

## 4.2 Exact two-sided confidence bands

In this section, we consider exact two-sided simultaneous confidence bands for a multiple linear regression over an ellipsoidal region based on the same methods.

## 4.2.1 Method following the idea of Bohrer (1973)

Recall (4.6) and (4.9). We change E(c) and  $A_r(c)$  slightly to make them correspond to the two-sided case. Therefore, we have for two-sided confidence bands

$$A_r = \{ \mathbf{t} : |\mathbf{z}^T \mathbf{t}| \le r \|\mathbf{z}\|, \text{ all } \mathbf{z} \text{ in } \mathbf{E}(c) \},$$

$$(4.34)$$

where

$$\mathbb{E}(c) = \{\mathbf{z} : |z_1| \ge c \|\mathbf{z}\|\}$$



Figure 4.4: For the method following Bohrer (1973) in two-sided case

Recall the definitions of the polar coordinates  $(R_t, \theta_{t1}, \ldots, \theta_{t,p-1})$ , where  $\theta_{tj} \in [0, \pi], j = 1, \ldots, p-2$  and  $\theta_{t,p-1} \in [0, 2\pi]$ . Note that when we consider  $\theta_{t1}$  moving throughout  $[0, \pi], A_r$  actually looks like the full region rather than just the upper half due to the effects of other angles  $\theta_{tj}, j = 2, \ldots, p-1$ . Also, note that  $A_r$  has a graphically symmetric shape for the two-sided case as shown in Figure 4.4. So we only need to consider the region produced by  $\theta_{t1}$  moving throughout  $[0, \pi/2]$ .

Define

$$\theta^{*} = \cos^{-1} c, 
T_{1} = \{ \mathbf{t} : 0 \le \theta_{\mathbf{t},1} \le \theta^{*}, R_{\mathbf{t}} \le r \}, 
T_{2} = \{ \mathbf{t} : \theta^{*} \le \theta_{\mathbf{t},1} \le \frac{\pi}{2}, R_{\mathbf{t}} \cos(\theta_{\mathbf{t},1} - \theta^{*}_{\perp}) \le r \}.$$
(4.35)

We have the confidence level of the two-sided band simply equal to

$$P\{\mathbf{t} \in A_r\} = 2\Big(P\{\mathbf{t} \in T_1\} + P\{\mathbf{t} \in T_2\}\Big).$$

$$(4.36)$$

Recall that  $\theta_{t1}$  has the density function given by

$$f(\theta) = k_1 \sin^{p-2}\theta \tag{4.37}$$

with  $k_1$  being the normalizing constant,  $R_t^2/p$  has the  $F_{p,\nu}$  distribution and is independent of  $\theta_{t1}$ . Thus, we obtain

$$P\{\mathbf{t} \in T_1\} = P\{0 \le \theta_{t1} \le \theta^*, R_t \le r\}$$

$$= \int_0^{\theta^*} k_1 \sin^{p-2} \theta d\theta \cdot P\{R_t \le r\}$$

$$= \int_0^{\theta^*} k_1 \sin^{p-2} \theta d\theta \cdot F_{p,\nu}(\frac{r^2}{p}), \qquad (4.38)$$

$$P\{\mathbf{t} \in T_2\} = P\{\theta^* \le \theta_{t1} \le \frac{\pi}{2}, R_t \cos(\theta_{t1} - \theta^*) \le r\}$$

$$= \int_{\theta^*}^{\frac{\pi}{2}} k_1 \sin^{p-2} \theta d\theta \cdot P\{R_t \cos(\theta_{t1} - \theta^*) \le r\}$$

$$= \int_0^{\frac{\pi}{2} - \theta^*} k_1 \sin^{p-2}(\theta + \theta^*) d\theta \cdot P\{R_t \le \frac{r}{\cos \theta}\}$$

$$= \int_0^{\frac{\pi}{2} - \theta^*} k_1 \sin^{p-2}(\theta + \theta^*) \cdot F_{p,\nu}(\frac{r^2/p}{\cos^2 \theta}) d\theta. \qquad (4.39)$$

Overall, the two-sided simultaneous confidence band can be constructed with the confidence level given by

$$\int_{0}^{\theta^{*}} 2k_{1} \sin^{p-2}\theta d\theta \cdot F_{p,\nu}(\frac{r^{2}}{p}) + \int_{0}^{\frac{\pi}{2}-\theta^{*}} 2k_{1} \sin^{p-2}(\theta+\theta^{*}) \cdot F_{p,\nu}(\frac{r^{2}/p}{\cos^{2}\theta}) d\theta.$$
(4.40)

## 4.2.2 Algebraical method

Casella and Strawderman (1980) considered the construction of a two-sided hyperbolic-shape confidence band over an ellipsoidal region  $\mathcal{X}$ . And the structure of this  $\mathcal{X}$  can be transformed as

$$\mathbf{E}(q) = \{ \mathbf{z} : \sum_{i=1}^{m} z_i^2 \ge q^2 \sum_{i=m+1}^{p} z_i^2 \}.$$

Specially when m = 1, E(q) becomes the structure of our interest that

$$\mathbf{E}(q) = \{ \mathbf{z} : |z_1| \ge \frac{q}{\sqrt{1+q^2}} \|\mathbf{z}\| \},\$$

where q > 0 is a fixed constant.

From the result of Casella and Strawderman (1980), it is that the twosided confidence band of hyperbolic shape

$$\mathbf{x}^{T}\boldsymbol{\beta} \in \mathbf{x}^{T}\hat{\boldsymbol{\beta}} \pm r\hat{\sigma}\sqrt{\mathbf{x}^{T}(\boldsymbol{X}^{T}\boldsymbol{X})^{-1}\mathbf{x}} \quad \mathbf{x} \in \mathcal{X},$$
(4.41)

where r is a critical value, has its simultaneous confidence level given by

$$F_{p,\nu}(\frac{r^2}{p}) + \int_{r^2/p}^{r^2/(b^2p)} F_{1,p-1}\left\{(p-1)\left(\frac{cr-b\sqrt{pw-r^2}}{br+c\sqrt{pw-r^2}}\right)^2\right\} dF_{p,\nu}(w), \quad (4.42)$$
  
here  $c = a/\sqrt{1+a^2}$  and  $b = 1/\sqrt{1+a^2}$ 

where  $c = q/\sqrt{1+q^2}$  and  $b = 1/\sqrt{1+q^2}$ .

## 4.2.3 Tubular neighborhood method

Recall (4.7), the confidence level of the two-sided band is alternatively given by

$$\mathbf{P}\Big\{\sup_{\mathbf{z}\in\mathbf{E}(c)}\frac{|\mathbf{z}^{T}\mathbf{t}|}{\|\mathbf{z}\|\|\mathbf{t}\|} \leq \frac{r}{\|\mathbf{t}\|}\Big\}.$$
(4.43)

Note that t/||t|| is independent of ||t||, the supreme in (4.43) is no larger than one, and

$$r/\sqrt{pw} < 1 \iff w > r^2/p.$$

Therefore, (4.43) is further equal to

2

$$1 - \int_{0}^{\infty} \mathbf{P} \Big\{ \sup_{\mathbf{y} \in \mathbf{E}(c)} \frac{|\mathbf{y}^{T}\mathbf{t}|}{\|\mathbf{y}\|\|\mathbf{t}\|} > \frac{r}{\sqrt{pw}} \Big\} dF_{p,\nu}(w)$$
  
= 
$$1 - \int_{r^{2}/p}^{\infty} \mathbf{P} \Big\{ \sup_{\mathbf{y} \in \mathbf{E}(c)} \frac{|\mathbf{y}^{T}\mathbf{t}|}{\|\mathbf{y}\|\|\mathbf{t}\|} > \frac{r}{\sqrt{pw}} \Big\} dF_{p,\nu}(w).$$
(4.44)

Let  $0 < h = r/\sqrt{pw} < 1$  such that  $\cos^{-1}h \in (0, \pi/2)$ . The set

$$\mathbb{E}(h) = \left\{ \mathbf{t} : \sup_{\mathbf{z} \in \mathbb{E}(c)} \frac{|\mathbf{z}^T \mathbf{t}|}{\|\mathbf{z}\| \|\mathbf{t}\|} > h \right\}$$

consists of two opposite spherical cones in  $\mathcal{R}^p$ . One cone,  $\mathcal{C}$ , has its vertex at the origin and its central direction given by  $z_1$ -axis, symmetrically and centrally containing one smaller cone with the angle  $\cos^{-1} h$  between a ray on its surface and the nearest ray from the smaller cone. The other cone is



Figure 4.5: For the tubular neighborhood method in two-sided case

simply  $-\mathcal{C}$ . The two smaller cones are produced by E(c). Then, in connection with the definition of the polar coordinates, we have E(h) equal to

$$\{ \mathbf{t} : \theta_{t1} \in [0, \theta^* + \cos^{-1} h] \cup [\pi - \theta^* - \cos^{-1} h, \pi] \} \quad \text{if} \quad \theta^* + \cos^{-1} h < \frac{\pi}{2}, \\ \{ \mathbf{t} : \theta_{t1} \in [0, \pi] \} \qquad \qquad \text{if} \quad \theta^* + \cos^{-1} h \ge \frac{\pi}{2}.$$

Note that

$$\theta^* + \cos^{-1}(r/\sqrt{pw}) < \frac{\pi}{2} \iff w < \frac{r^2}{b^2p}$$

and the density function of  $\theta_{t,1}$  is given by (4.37), we therefore have, for  $r^2/p \le w < r^2/(b^2p)$ ,

$$P\{\mathbf{t} \in E(h)\}$$

$$= P\{\theta_{\mathbf{t},1} \in [0, \theta^* + \cos^{-1}(r/\sqrt{pw})] \cup [\pi - \theta^* - \cos^{-1}(r/\sqrt{pw}), \pi]\}$$

$$= \int_0^{\theta^* + \cos^{-1}(r/\sqrt{pw})} 2k_1 \sin^{p-2}\theta d\theta;$$

and, for  $w \ge r^2/(b^2p)$ ,

$$P\{\mathbf{t} \in E(h)\} = P\{\theta_{t,1} \in [0,\pi]\} = 1.$$

Consequently, the confidence level (4.44) is equal to

$$1 - \int_{r^{2}/p}^{r^{2}/(b^{2}p)} \int_{0}^{\theta^{*} + \cos^{-1}(r/\sqrt{pw})} 2k_{1} \sin^{p-2}\theta d\theta dF_{p,\nu}(w) - \int_{r^{2}/(b^{2}p)}^{\infty} 1dF_{p,\nu}(w).$$
(4.45)

## 4.2.4 Equivalence of the formulae

By changing the order of integrations, the double integral in (4.45) simplifies as

$$\int_{0}^{\theta^{\star}} 2k_{1} \sin^{p-1}\theta d\theta \{F_{p,\nu}(\frac{r^{2}}{b^{2}p}) - F_{p,\nu}(\frac{r^{2}}{p})\} + \int_{\theta^{\star}}^{\frac{\pi}{2}} 2k_{1} \sin^{p-1}\theta \Big\{F_{p,\nu}(\frac{r^{2}}{b^{2}p}) - F_{p,\nu}\Big(\frac{r^{2}}{p\cos^{2}(\theta-\theta^{\star})}\Big)\Big\} d\theta. \quad (4.46)$$

Substitute (4.46) into (4.45) and note that

$$\int_0^{\frac{\pi}{2}} 2k_1 \sin^{p-1}\theta d\theta \cdot F_{p,\nu}(\frac{r^2}{b^2 p}) = \int_0^{r^2/(b^2 p)} dF_{p,\nu}(w).$$

We finally have that the confidence level based on the tubular neighborhood method is equivalent to the expression given in (4.40).

Change (4.23) slightly to make it corresponding to the two-sided case. We therefore have the confidence level of the two-sided band is

$$P\{R_{t}^{2} \leq r^{2}\} + P\left\{r^{2} < R_{t}^{2} \leq \frac{r^{2}}{b^{2}}, w = \frac{t_{1}}{\|\mathbf{t}_{(1)}\|} \\ \in \left(-\frac{ar - b\sqrt{R_{t}^{2} - r^{2}}}{br + a\sqrt{R_{t}^{2} - r^{2}}}, \frac{ar - b\sqrt{R_{t}^{2} - r^{2}}}{br + a\sqrt{R_{t}^{2} - r^{2}}}\right)\right\},$$
(4.47)

where  $a = q/\sqrt{1+q^2}$  and  $b = 1/\sqrt{1+q^2}$ . The first probability is simply equal to  $F_{p,\nu}(r^2/p)$ , and the second one is further equal to

$$\int_{\frac{r^2}{p}}^{\frac{r^2}{b^2p}} \mathbb{P}\Big\{\frac{|t_1|}{\|\mathbf{t}_{(1)}\|} \le \frac{ar - b\sqrt{pw - r^2}}{br + a\sqrt{pw - r^2}}\Big\} dF_{p,\nu}(w)$$

$$= \int_{\frac{r^2}{p}}^{\frac{r^2}{b^2p}} F_{1,p-1}\Big\{(p-1)\Big(\frac{ar - b\sqrt{pw - r^2}}{br + a\sqrt{pw - r^2}}\Big)^2\Big\} dF_{p,\nu}(w). \quad (4.48)$$

It can be found that (4.47) is equivalent to (4.42). On the other hand, we can write (4.47) according to the location of the vector t. It is that (4.47) can be evaluated in terms of the regions  $\theta_{t1}$  belongs to, as

ŕ

$$P\{R_{t}^{2} \leq r^{2}, \theta_{t1} \in [0, \theta^{*}] \cup [\pi - \theta^{*}, \pi]\} + P\{R_{t} \cos(\theta_{t1} - \theta^{*}) \leq r, \theta_{t1} \in (\theta^{*}, \pi - \theta^{*})\}$$

$$= \int_{0}^{\theta^{*}} k_{1} \sin^{p-2}\theta d\theta \cdot F_{p,\nu}(\frac{r^{2}}{p}) + \int_{\pi - \theta^{*}}^{\pi} k_{1} \sin^{p-2}\theta d\theta \cdot F_{p,\nu}(\frac{r^{2}}{p}) + \int_{\theta^{*}}^{\pi - \theta^{*}} k_{1} \sin^{p-2}\theta \cdot F_{p,\nu}(\frac{r^{2}}{p \cos^{2}(\theta - \theta^{*})}) d\theta$$

$$= \int_{0}^{\theta^{*}} 2k_{1} \sin^{p-2}\theta d\theta \cdot F_{p,\nu}(\frac{r^{2}}{p}) + \int_{0}^{\frac{\pi}{2} - \theta^{*}} 2k_{1} \sin^{p-2}(\theta + \theta^{*}) \cdot F_{p,\nu}(\frac{r^{2}}{p \cos^{2}\theta}) d\theta, \qquad (4.49)$$

which is the same as (4.40). Consequently, we obtain the equivalence of the three formulae corresponding to the three methods respectively.

## Chapter 5

## Simultaneous confidence bands for a regression model over a rectangular region and comparisons

1

In last two chapters, we discussed the construction of exact simultaneous confidence bands with the predictor variables restricted in an ellipsoidal region. In this chapter, we turn to consider the construction of two-sided simultaneous confidence bands over the most popular rectangular region of the predictor space based on several methods, including Naiman (1986)'s conservative method by applying the tube volume theory, the approximate method proposed by Sun and Loader (1994) presenting an approximation to the tube formula to construct confidence bands for a parametric or nonparametric regression function, and the simulation-based method of Liu, Wynn and Hayter (2005) and Liu, Jamshidian, Zhang and Donnelly (2005) to construct confidence bands for these methods are given in terms of critical values. All critical values are calculated by running programmes on MATLAB 7 platform. Conclusions are drawn in the end.

## 5.1 Conservative confidence bands

Naiman (1986) presented a method of constructing conservative hyperbolicshape simultaneous confidence bands for an one-dimensional curvilinear regression over finite intervals. This method is, by using a geometric inequality, to obtain an upper bound for the volume of a tube with a fixed distance from an arbitrary path which is piecewise differentiable and has a finite length on the surface  $S^{p-1}$  of the unit sphere in *p*-dimensional real space.

Consider the regression model

$$y = \mathbf{f}(x)^T \boldsymbol{\beta} + \boldsymbol{\varepsilon},\tag{5.1}$$

where y is the response,  $\mathbf{f}(x)$  is the p-dimensional vector of known functions of the only predictor variable x,  $\boldsymbol{\beta}$  is the p-dimensional vector of unknown regression coefficients,  $\varepsilon$  is the random error which is normally distributed with mean 0 and unknown variance  $\sigma^2$ . For a special case when  $\mathbf{f}(x) =$  $(1, x, x^2, \ldots, x^{p-1})^T$ , (5.1) is the usual polynomial regression model of p-1degrees. Let  $\mathcal{X} \subset \mathcal{R}$  be a restricted interval containing all possible values of x. Denote  $\hat{\boldsymbol{\beta}}$  and  $\hat{\sigma}^2$  the maximum likelihood estimator of  $\boldsymbol{\beta}$  and the usual unbiased estimator of  $\sigma^2$  respectively. Also, assume the design matrix is of full rank so that  $\hat{\boldsymbol{\beta}} \sim N_p(\boldsymbol{\beta}, \sigma^2 \boldsymbol{\Sigma})$  for some known positive definite matrix  $\boldsymbol{\Sigma}$ . And  $\nu \hat{\sigma}^2 / \sigma^2 \sim \chi^2_{\nu}$  with  $\nu$  degrees of freedom. Let P be a  $p \times p$  non-singular matrix such that  $P^T P = \boldsymbol{\Sigma}$ .

A two-sided hyperbolic-shape simultaneous confidence band for the mean regression function  $\mathbf{f}(x)^T \boldsymbol{\beta}$  over the restricted predictor space is given by

$$\mathbf{f}(x)^T \boldsymbol{\beta} \in \mathbf{f}(x)^T \hat{\boldsymbol{\beta}} \pm c \hat{\sigma} p(x) \quad \text{all } x \in \mathcal{X},$$
(5.2)

where  $p(x) = {\mathbf{f}(x)^T \Sigma \mathbf{f}(x)}^{1/2} = ||P\mathbf{f}(x)||$ , and  $c \ge 0$  is a critical value. Define  $\mathbf{N} = (P^{-1})^T (\boldsymbol{\beta} - \hat{\boldsymbol{\beta}}) / \sigma$  which in fact has a *p*-variate standard normal distribution by studying the least squares theory. Then the confidence band (5.2) has the confidence level given by

$$P\left\{\sup_{x\in\mathcal{X}}\frac{|\mathbf{f}(x)^{T}(\boldsymbol{\beta}-\hat{\boldsymbol{\beta}})|}{p(x)} \leq c\hat{\sigma}\right\}$$

$$= P\left\{\sup_{x\in\mathcal{X}}\frac{|[P\mathbf{f}(x)]^{T}(P^{T})^{-1}(\boldsymbol{\beta}-\hat{\boldsymbol{\beta}})/\sigma|}{\|P\mathbf{f}(x)\|} \leq \frac{c\hat{\sigma}}{\sigma}\right\}$$

$$= P\left\{\sup_{x\in\mathcal{X}}\frac{|[P\mathbf{f}(x)]^{T}\mathbf{N}|}{\|P\mathbf{f}(x)\|\|\mathbf{N}\|} \leq \frac{c\hat{\sigma}/\sigma}{\|\mathbf{N}\|}\right\}$$

$$= 1 - P\left\{\sup_{x\in\mathcal{X}}\frac{|[P\mathbf{f}(x)]^{T}\mathbf{N}|}{\|P\mathbf{f}(x)\|\|\mathbf{N}\|} > \frac{c\hat{\sigma}/\sigma}{\|\mathbf{N}\|}\right\}.$$
(5.3)

Define

$$\gamma(x) = \frac{P\mathbf{f}(x)}{\|P\mathbf{f}(x)\|} \quad \text{for } x \in \mathcal{X},$$
(5.4)

which is a path in  $S^{p-1}$ , the surface of the unit sphere centered at the origin in  $\mathcal{R}^p$ . And assume the length of the path given by  $\Lambda(\gamma) = \int_{\mathcal{X}} \|\gamma'(x)\| dx$  is finite. Also, define the random vector  $\mathbf{U} = \mathbf{N}/\|\mathbf{N}\|$ . Consider N in terms of the polar coordinates  $R_{\mathbf{N}} = \|\mathbf{N}\|$  and  $\boldsymbol{\theta}_{\mathbf{N}}$ . Then U only depends on  $\boldsymbol{\theta}_{\mathbf{N}}$ . Since N has the *p*-variate standard normal distribution, one may directly find the joint density function of  $\|\mathbf{N}\|$  and  $\boldsymbol{\theta}_{\mathbf{N}}$ . Furthermore, by finding the individual marginal density functions, we obtain that the joint density is equal to the product of the individual marginal densities, which implies that  $\|\mathbf{N}\|$  and  $\boldsymbol{\theta}_{\mathbf{N}}$  are statistically independent. So are U and  $\|\mathbf{N}\|$ .

If  $\Gamma(\gamma)$  and  $\mu$  are used to denote the image of the path and the uniform probability measure on  $S^{p-1}$  respectively, define for  $r \in [0, 1]$ 

$$\Gamma(\boldsymbol{\gamma})_{(r)} = \{ u \in S^{p-1} : \sup(u^T v) > r \text{ for } v \in \Gamma(\boldsymbol{\gamma}) \}.$$
(5.5)

Recall (5.3). Since the supreme is no larger than one, we have  $0 \leq (\hat{\sigma}/\sigma)/||\mathbf{N}|| \leq 1/c$ . Hence (5.3) is further equal to

$$1 - \int_0^{1/c} \mu\{[\Gamma(\boldsymbol{\gamma}) \cup -\Gamma(\boldsymbol{\gamma})]_{(ct)}\} f_T(t) dt, \qquad (5.6)$$

where  $f_T$  denotes the density function of  $T = (\hat{\sigma}/\sigma)/||\mathbf{N}||$  such that  $pT^2 \sim F_{\nu,p}$ , the F distribution with  $\nu$  and p degrees of freedom.



Figure 5.1: Tubular neighborhood of a path

The central part of Naiman (1986) is to find an upper bound of  $\mu\{\Gamma(\gamma)_{(r)}\}$ so as to construct a conservative confidence band. Consider the case when  $\Gamma(\gamma)$  can be piecewise approximated by great circular arcs using geometric inequalities. The great circular curve obtained after approximation can then be replaced by a curve of the same length on a single great circle by straightening out the curve at each point where the circular arcs are joined. Equivalently, if  $\gamma$  is replaced by  $\gamma^*$ , a path of equal length but whose image lies on a great circle, then the bound may be thought of as  $\mu\{\Gamma(\gamma^*)_{(r)}\}$ . Thus, a bound is obtained which depends only on the length of the path and consists of two terms. The first term is proportional to the length of the path corresponding to the points in the middle tubular part of  $\Gamma(\gamma^*)_{(r)}$ . The second term is the sum of the measures of two half spherical caps of angular radius  $\cos^{-1} r$  corresponding to the points in the two half spherical ends of the tube  $\Gamma(\gamma^*)_{(r)}$ . Hence, the upper bound of  $\mu\{\Gamma(\gamma)_{(r)}\}$  is given by

$$\mu\{\Gamma(\boldsymbol{\gamma})_{(r)}\} \leq \min\{F_{p-2,2}[2(r^{-2}-1)/(p-2)] \times \Lambda(\boldsymbol{\gamma})/(2\pi) + F_{p-1,1}[(r^{-2}-1)/(p-1)]/2, 1\}.$$
(5.7)

The minimum used here is to avoid overlapping.

From (5.7), a lower bound for the coverage probability of the confidence band (5.2) is obtained as

$$1 - \int_{0}^{\frac{1}{c}} \min\{F_{p-2,2}[2((ct)^{-2}-1)/(p-2)] \times \Lambda(\gamma)/\pi + F_{p-1,1}[((ct)^{-2}-1)/(p-1)], 1\}f_{T}(t)dt,$$
(5.8)

where  $f_T$  is the density function of the random variable T, c is a critical value.

In a special case when p = 2 and  $\mathbf{f}(x) = (1, x)^T$  where x belongs to a subset  $\mathcal{X}$ , the given model reduces to a usual simple linear regression model with a restricted predictor variable. Accordingly, the conservative confidence band becomes exact, because, for this special case, the path  $\gamma(x)$  is already on the unit circle so that it is unnecessary to straighten it out. One may find  $\mu\{\Gamma(\gamma)_{(\tau)}\}$  directly. Then the confidence level is

$$1 - \int_0^{\frac{1}{c}} \min\{\Lambda(\gamma)/\pi + F_{1,1}[(ct)^{-2} - 1], 1\} f_T(t) dt,$$
 (5.9)

where  $\Lambda(\boldsymbol{\gamma})$  is the length of the path.

It is of natural interest to show the equivalence between (5.9) and one of the computational formulae obtained in Chapter 3, which is used to calculate the critical values for the exact two-sided confidence bands for a simple linear regression.

Note that, in connection with (5.5), (5.6) can be written alternatively as

$$1 - \int_{0}^{\frac{1}{c}} P\Big\{ \sup_{v \in \Gamma} |u^{T}v| > ct \Big\} f_{T}(t) dt.$$
 (5.10)

By changing the variable of the integration, we have (5.10) further equal to

$$1 - \int_{\frac{c^2}{2}}^{\infty} \mathbb{P}\Big\{\sup_{v \in \Gamma} |u^T v| > \frac{c}{\sqrt{2w}}\Big\} dF_{2,\nu}(w),$$
(5.11)

where  $F_{2,\nu}$  stands for an F random variable with 2 and  $\nu$  degrees of freedom.

Recall (3.34) and the definitions of u and v in (5.11), and we find that (5.11) is equivalent to formula (3.34). In connection with the equivalence of the formulae in Section 3.2, it can be concluded that the formula of Naiman's conservative method for the simple linear regression case is equivalent to that obtained by the exact method, e.g., formula (3.41).

## 5.2 Approximate confidence bands

Sun and Loader (1994) stated a method of constructing approximate  $1 - \alpha$  simultaneous confidence bands for a parametric or nonparametric function over a constrained predictor space. This method, which is in fact an approximation to the tube formula, can be applied to the multiple regression case, and is adaptable for a wide class of linear estimators. More details about the volume-of-tube formula, see, e.g., Loader (2004).

Consider the multiple regression model

$$y_i = f(\mathbf{x}_i) + \varepsilon, \tag{5.12}$$

where  $\mathbf{x}_i, y_i, i = 1, ..., n$  are the observations,  $\mathbf{x}_i \in \mathcal{R}^d$  is a vector of the predictor variables,  $f(\cdot)$  is an unknown function which needs to be estimated based on the observations, and  $\varepsilon$  is the normally distributed random error with mean 0 and variance  $\sigma^2$  which is assumed to be unknown. A linear estimator of the mean response  $f(\mathbf{x})$  is given by

$$\hat{f}(\mathbf{x}) = \sum_{i=1}^{n} l_i(\mathbf{x}) y_i = \mathbf{l}(\mathbf{x})^T \mathbf{Y},$$
(5.13)

where  $l(\mathbf{x}) = (l_1(\mathbf{x}), \dots, l_n(\mathbf{x}))^T$  and  $\mathbf{Y} = (y_1, \dots, y_n)^T$ .

A simultaneous confidence band for  $f(\mathbf{x})$  over a subset  $\mathcal{X}$  of the predictor space has the form given by

$$\{(\hat{f}(\mathbf{x}) - c\hat{\sigma} \| \mathbf{l}(\mathbf{x}) \|, \hat{f}(\mathbf{x}) + c\hat{\sigma} \| \mathbf{l}(\mathbf{x}) \|) : \mathbf{x} \in \mathcal{X}\},$$
(5.14)

where c is a critical value and  $\hat{\sigma}$  is the usual unbiased estimator of  $\sigma$ . If we assume the band (5.14) has  $1 - \alpha$  confidence level. Then, we have

$$1 - \alpha = \inf_{f \in \mathcal{F}} P_f\{\hat{f}(\mathbf{x}) - c\hat{\sigma} \| \mathbf{l}(\mathbf{x}) \| \le f(\mathbf{x})$$
$$\le \hat{f}(\mathbf{x}) + c\hat{\sigma} \| \mathbf{l}(\mathbf{x}) \|, \forall \mathbf{x} \in \mathcal{X}\},$$
(5.15)

where  $\mathcal{F}$  is a wide suitable class of functions. Next, we evaluate the probability on the right-hand side of (5.15) in order to obtain a computational formula for calculating the critical value c.

A class  $\mathcal{F}$ , of natural interest, is a set of functions for which  $\hat{f}(\mathbf{x})$  is an unbiased estimator, i.e.,

$$\mathcal{F} = \{ f : f(\mathbf{x}) = \mathbf{l}(\mathbf{x})^T \boldsymbol{\mu}, \forall \mathbf{x} \},\$$

where  $\boldsymbol{\mu} = (f(\mathbf{x}_1), \dots, f(\mathbf{x}_n))^T$ . In this case the probability that coverage fails for the band (5.14) has the following expressions

$$\begin{aligned} \alpha &= P\left\{\sup_{\mathbf{x}\in\mathcal{X}} \frac{|\hat{f}(\mathbf{x}) - f(\mathbf{x})|}{||\mathbf{l}(\mathbf{x})||} > c\hat{\sigma}\right\} \\ &= P\left\{\sup_{\mathbf{x}\in\mathcal{X}} \frac{|\mathbf{l}(\mathbf{x})^T\mathbf{Y} - \mathbf{l}(\mathbf{x})^T\boldsymbol{\mu}|}{||\mathbf{l}(\mathbf{x})||} > c\hat{\sigma}\right\} \\ &= P\left\{\sup_{\mathbf{x}\in\mathcal{X}} |\mathbf{T}(\mathbf{x})^T\boldsymbol{\varepsilon}| > c\hat{\sigma}\right\} \\ &= P\left\{\sup_{\mathbf{x}\in\mathcal{X}} |\frac{\mathbf{T}(\mathbf{x})^T\boldsymbol{\varepsilon}}{\sigma}| > \frac{c\hat{\sigma}}{\sigma}\right\} \\ &= P\left\{\sup_{\mathbf{x}\in\mathcal{X}} |\frac{\mathbf{T}(\mathbf{x})^T\mathbf{N}}{||\mathbf{N}||} |> c\frac{(\hat{\sigma}/\sigma)}{||\mathbf{N}||}\right\} \\ &= \int_c^{\infty} P\left\{\sup_{\mathbf{x}\in\mathcal{X}} |\mathbf{T}(\mathbf{x})^T\mathbf{U}| > \frac{c}{z}\right\} g(z)dz, \end{aligned}$$
(5.16)

where  $\mathbf{T}(\mathbf{x}) = \mathbf{l}(\mathbf{x})/||\mathbf{l}(\mathbf{x})||$ ,  $\boldsymbol{\varepsilon} = \mathbf{Y} - \boldsymbol{\mu}$  is an *n*-dimensional vector of random errors, g(z) is the density function of the random variable  $Z = ||\mathbf{N}||/(\hat{\sigma}/\sigma)$ ,  $\mathbf{N} = \boldsymbol{\varepsilon}/\sigma$  has the  $N_n(\mathbf{0}, \mathbf{l}(\mathbf{x})^T \mathbf{l}(\mathbf{x}))$  distribution, and  $\mathbf{U} = \mathbf{N}/||\mathbf{N}||$  is a unit vector on the surface of the unit sphere  $S^{n-1}$  and is independent of  $||\mathbf{N}||$ .

Letting  $\mathcal{M} = \{\mathbf{T}(\mathbf{x}) : \mathbf{x} \in \mathcal{X}\}$ , the probability on the right-hand side of the last equality in (5.16) is simply the volume of a tubular neighborhood of  $\mathcal{M} \cup -\mathcal{M}$  on the surface of  $S^{n-1}$ . Here, approximate formulae for onedimensional and two-dimensional cases are given. Although this approximate method can be applied to high dimensional case by following the similar idea, lots of geometric constants are needed to be calculated. So we only consider the low dimensional cases, i.e.,  $d \leq 2$ . The difficulty on the computation of the geometric constants is thought as the drawback of this method.

Assume the manifold  $\mathcal{M}$  is the third order continuous with a positive critical radius. Suppose  $\mathbf{T} : \mathcal{X} \longrightarrow \mathcal{M}$  is one-to-one, three times differentiable and there exists a vector  $\boldsymbol{\lambda}$  such that  $\boldsymbol{\lambda}^T \mathbf{T}(\mathbf{x}) > 0$  for all  $\mathbf{x} \in \mathcal{X}$  which

ensures the tubes around  ${\mathcal M}$  and  $-{\mathcal M}$  do not intersect for sufficiently small radii.

Proposition 5.2.1 (One-dimensional) Suppose  $x \in [a, b]$ . The length of  $\mathcal{M}$  is  $\kappa_0 = \int_a^b \|\mathbf{T}'(\mathbf{x})\| dx$ , where  $\mathbf{T}(\mathbf{x}) = \mathbf{l}(\mathbf{x})/\|\mathbf{l}(\mathbf{x})\|$  with  $\mathbf{l}(\mathbf{x}) = X(X^T X)^{-1}\mathbf{x}$  for linear regression models, X is the design matrix. And  $\nu \hat{\sigma}^2 / \sigma^2 \sim \chi^2_{\nu}$ . Then

$$\alpha \approx \frac{\kappa_0}{\pi} (1 + \frac{c^2}{\nu})^{-\nu/2} + P\{|t_\nu| > c\},$$
(5.17)

where the last term on the right-hand side of (5.17) is the probability of the absolute value of a t random variable with  $\nu$  degrees of freedom larger than c.

**Proposition 5.2.2** (Two-dimensional) Suppose  $\mathcal{X}$  is a rectangle in  $\mathcal{R}^2$ . Let  $\kappa_0$  be the area of  $\mathcal{M}$ ,  $\zeta_0$  be the length of the boundary of  $\mathcal{M}$ . Then

$$\alpha \approx \frac{\kappa_0}{\pi^{3/2}} \frac{\Gamma((\nu+1)/2)}{\Gamma(\nu/2)} \frac{c}{\sqrt{\nu}} (1 + \frac{c^2}{\nu})^{-(\nu+1)/2} + \frac{\zeta_0}{2\pi} (1 + \frac{c^2}{\nu})^{-\nu/2} + P\{|t_\nu| > c\}.$$
(5.18)

For computing constants  $\kappa_0$  and  $\zeta_0$ , denote  $\mathbf{T}_j(\mathbf{x}) = \partial \mathbf{T}(\mathbf{x}) / \partial x_j, j=1,2$ . Then

$$\kappa_0 = \int_{\mathcal{X}} det^{1/2} (A^T A) d\mathbf{x}, \qquad (5.19)$$

$$\zeta_0 = \int_{\partial \mathcal{X}} det^{1/2} (\mathbf{A_*}^T \mathbf{A_*}), \qquad (5.20)$$

where  $A = (\mathbf{T}_1(\mathbf{x}), \mathbf{T}_2(\mathbf{x})), \mathbf{A}_* = \mathbf{T}_1(\mathbf{x})$  or  $\mathbf{T}_2(\mathbf{x})$ .

# 5.3 Simulation-based confidence bands for a polynomial regression

Liu, Wynn and Hayter (2005) proposed the simulation-based method for constructing simultaneous confidence bands for an one-dimensional polynomial regression model with the only predictor variable restricted in an interval. Monte Carlo simulation is used to find an accurate approximation to the critical value of the confidence band when the number of simulations is set to be sufficiently large.

Consider the one-dimensional polynomial regression model

$$\mathbf{Y} = X\boldsymbol{\beta} + \boldsymbol{\varepsilon},\tag{5.21}$$

where  $\mathbf{Y}_{n\times 1}$  is the vector of the observed responses,  $X_{n\times p}$  is the full columnrank design matrix with the *i*th  $(1 \leq i \leq n)$  row given by  $(1, x_i, \ldots, x_i^{p-1})$ ,  $\boldsymbol{\beta} = (\beta_1, \ldots, \beta_p)^T$  is the vector of unknown regression coefficients, and  $\boldsymbol{\varepsilon}$  is the vector of independent and identically distributed normal random errors with mean 0 and variance  $\sigma^2$ , which is assumed to be unknown. Denote the maximum likelihood estimator of  $\boldsymbol{\beta}$  by  $\hat{\boldsymbol{\beta}}$ , therefore,  $\hat{\boldsymbol{\beta}} \sim N_p(\boldsymbol{\beta}, \sigma^2(X^T X)^{-1})$ . Also, denote an unbiased estimator of  $\sigma^2$  by  $\hat{\sigma}^2$  so that  $\nu \hat{\sigma}^2 / \sigma^2 \sim \chi_{\nu}^2$ . Moreover,  $\hat{\boldsymbol{\beta}}$  and  $\hat{\sigma}^2$  are independent.

A hyperbolic-shape simultaneous confidence band for the mean response  $\mathbf{x}^T \boldsymbol{\beta}$  over the restricted predictor space when  $x \in (a, b)$  is given by

$$\mathbf{x}^{T}\boldsymbol{\beta} \in \mathbf{x}^{T}\hat{\boldsymbol{\beta}} \pm c\hat{\sigma}\sqrt{\mathbf{x}^{T}(\boldsymbol{X}^{T}\boldsymbol{X})^{-1}\mathbf{x}}, \forall \boldsymbol{x} \in (a, b),$$
(5.22)

where  $\mathbf{x} = (1, x, \dots, x^{p-1})$ , c is a critical value such that the confidence band (5.22) has the confidence level equal to  $1 - \alpha$ . Alternatively, (5.22) can be arranged as

$$\sup_{a < x < b} \frac{|\mathbf{x}^T(\hat{\boldsymbol{\beta}} - \boldsymbol{\beta}) / \sigma|}{(\hat{\sigma} / \sigma) \sqrt{\mathbf{x}^T (\boldsymbol{X}^T \boldsymbol{X})^{-1} \mathbf{x}}} \le c.$$
(5.23)

Define

$$T = \sup_{a < x < b} \frac{|\mathbf{x}^T(\hat{\boldsymbol{\beta}} - \boldsymbol{\beta})/\sigma|}{(\hat{\sigma}/\sigma)\sqrt{\mathbf{x}^T(X^TX)^{-1}\mathbf{x}}},$$
(5.24)

the confidence level of the band (5.22) is given by  $P\{T \leq c\}$ . The following procedure shows how to use Monte Carlo simulation method to approximate the critical value c.

Step 1 Generate N =  $(\hat{\boldsymbol{\beta}} - \boldsymbol{\beta}) / \sigma \sim N_p(\mathbf{0}, (X^T X)^{-1}).$ 

**Step 2** Generate  $s = \hat{\sigma}/\sigma \sim \sqrt{\chi_{\nu}^2/\nu}$ .

Step 3 Calculate T from (5.24). To find the supreme in (5.24), firstly find all the stationary points of

$$h(x) = \left(\frac{|\mathbf{x}^T \mathbf{N}|}{\sqrt{\mathbf{x}^T (X^T X)^{-1} \mathbf{x}}}\right)^2 = \frac{\mathbf{x}^T \mathbf{N} \mathbf{N}^T \mathbf{x}}{\mathbf{x}^T (X^T X)^{-1} \mathbf{x}}$$

by solving h'(x) = 0, i.e.,

$$g(x) = \left(\frac{d\mathbf{x}^T}{dx}\mathbf{N}\mathbf{N}^T\mathbf{x}\right) \left[\mathbf{x}^T (X^T X)^{-1}\mathbf{x}\right] - \left(\mathbf{x}^T \mathbf{N}\mathbf{N}^T\mathbf{x}\right) \left[\frac{d\mathbf{x}^T}{dx} (X^T X)^{-1}\mathbf{x}\right] = 0.$$

Since g(x) is a polynomial of order 4p - 6, it has at most 4p - 6 zero points. If they are denoted by  $x_1, \ldots, x_q$ , from (5.24) we have

$$T = \max\{\sqrt{h(a)}, \sqrt{h(b)}, \max_{1 \le i \le q; x_i \in (a,b)} \sqrt{h(x_i)}\}/s.$$

Step 4 Simulate R independent replicates of T, say,  $T_1, \ldots, T_R$ , and use the  $[(1 - \alpha)R]$ th largest  $T_i$  as an approximation of c, denoted by  $\hat{c}$ .

The base of this approach is that the sample  $100(1 - \alpha)$  percentile  $\hat{c}$  converges almost surely to the population  $100(1 - \alpha)$  percentile c when the number of simulations R goes to infinity. Furthermore, to gauge the accuracy of  $\hat{c}$ , it is useful to estimate its standard error. It is known that, under certain regularity conditions,  $\hat{c}$  is asymptotically normal with mean c and standard error

$$s.e. = \sqrt{\frac{\alpha(1-\alpha)}{RG^2(c)}},\tag{5.25}$$

where G(c) is the density function of T evaluated at c (see, e.g., Serfling, 1980). And G(c) may be approximated by the kernel density estimator

$$G(c) = \frac{1}{Rd\sqrt{2\pi}} \sum_{i=1}^{R} e^{-[(\hat{c}-T_i)/d]^2/2},$$

where  $T_i$  is the *i*th simulated value and *d* is the smoothing parameter. We usually set d = 0.1, 0.01, 0.001.

## 5.4 Simulation-based confidence bands for a multiple linear regression

Liu, Jamshidian, Zhang and Donnelly (2005) presented a method of constructing simultaneous confidence bands for a normal-error multiple linear regression model based on Monte Carlo simulation procedure. The confidence bands constructed via this method have hyperbolic shape and can be applied to a model with any number of predictor variables.

Consider the multiple linear regression model

$$\mathbf{Y} = X\boldsymbol{\beta} + \boldsymbol{\varepsilon},$$

where  $X_{n \times p}$  is the design matrix with the first column given by  $(1, \ldots, 1)^T$ and the *j*th  $(2 \le j \le p)$  column given by  $(x_{1,j-1}, \ldots, x_{n,j-1})^T$ . Inferences on estimators of unknown parameters  $\beta$  and  $\sigma^2$  can be obtained as usual.

It is of interest to construct a simultaneous confidence band on the most popular rectangular region  $\mathcal{X}$  of the predictor space, which is of the form

$$\mathcal{X} = \{ (x_1, \dots, x_{p-1})^T : a_i \le x_i \le b_i, i = 1, \dots, p-1 \},$$
 (5.26)

where  $-\infty \leq a_i < b_i \leq \infty, i = 1, ..., p-1$  are given constants. The central task is to find an appropriate critical value c such that the confidence band has the confidence level equal to a preassigned  $1 - \alpha$ .

Note that the confidence level of the band is given by  $P\{T < c\}$ , where

$$T = \sup_{x_i \in [a_i, b_i], i=1, \dots, p-1} \frac{|\mathbf{x}^T (\hat{\boldsymbol{\beta}} - \boldsymbol{\beta}) / \sigma|}{(\hat{\sigma} / \sigma) \sqrt{\mathbf{x}^T (\boldsymbol{X}^T \boldsymbol{X})^{-1} \mathbf{x}}}.$$
 (5.27)

The distribution of T depends on the design matrix and the intervals  $(a_i, b_i)$ in a complicated manner. This makes a challenge to derive the distribution function of T directly. In such a case, it is motivated to introduce a simulation-based method to find an approximation to the critical value c, say  $\hat{c}$ , which can be as accurate as one wants by simulating a sufficiently large number of T's. It is clear from (5.27) that the calculation of T is in fact an optimization problem. Consequently, our analysis focuses on the optimization algorithm. Let P be a  $p \times p$  non-singular matrix such that  $(X^T X)^{-1} = P^T P$ . Then generate one  $\mathbf{N} = (P^T)^{-1}(\hat{\boldsymbol{\beta}} - \boldsymbol{\beta})/\sigma \sim N_p(\mathbf{0}, I)$  and one independent  $\hat{\sigma}/\sigma \sim \sqrt{\chi_{\nu}^2/\nu}$ . Therefore, T becomes

$$T = Q \frac{\|\mathbf{N}\|}{(\hat{\sigma}/\sigma)},\tag{5.28}$$

where

Ł

$$Q = \sup_{x_i \in [a_i, b_i], i=1, \dots, p-1} \frac{|(P\mathbf{x})^T \mathbf{N}|}{\|P\mathbf{x}\| \| \|\mathbf{N}\|}.$$

Accordingly, the optimization problem of T transforms to the optimization of Q which involves the maximization of a p-variate function over the given rectangular region of the predictor space. Two methods were included in Liu, Jamshidian, Zhang and Donnelly (2005) to solve such a maximization problem. They are the branching method and the active set method respectively. T can be obtained after Q is ready.

As stated in Section 5.3, we simulate R replicates of the random variable T, and set the  $[(1 - \alpha)R]$ th largest simulated value  $\hat{c}$  as an approximate of the critical value c. Also, one may estimate the standard error of  $\hat{c}$  using (5.25) to gauge its accuracy.

## 5.5 Comparisons

For the methods of constructing confidence bands introduced in this chapter, we are interested in comparing them in terms of the critical value to have a general view on the goodness of each. All the critical values in this section are calculated using MATLAB programmes.

#### 5.5.1 For simple linear regression

We start with the comparison for a simple linear regression model. As already pointed out, for simple linear regression case, Naiman's method turns to be exact. So the methods in our first comparison include: the exact method, the approximate method of Sun and Loader (1994), and the simulation-based method of Liu, Wynn and Hayter (2005).

Note that, all the methods depend on the design matrix, the restricted interval for the only predictor variable and the confidence level. However, one may go further to consider the nature of the methods.

For the exact method, we have the computational formula for the critical value given by

$$1 - \alpha = \frac{2\theta^*}{\pi} F_{2,\nu}(\frac{c^2}{2}) + \frac{2}{\pi} \int_0^{\frac{\pi}{2} - \theta^*} F_{2,\nu}(\frac{c^2}{2\cos^2\theta}) d\theta,$$
(5.29)

where  $F_{2,\nu}$  stands for the *F* cumulative distribution function with 2 and  $\nu = n - 2$  degrees of freedom, and  $\theta^*$  can be found in the following way: define  $\mathbf{a} = (1, a)^T$ ,  $\mathbf{b} = (1, b)^T$  where a, b are the lower and upper bounds of the restricted interval, then we have

$$\theta^* = \frac{1}{2} \arccos \frac{\mathbf{a}^T (X^T X)^{-1} \mathbf{b}}{(\mathbf{a}^T (X^T X)^{-1} \mathbf{a} \cdot \mathbf{b}^T (X^T X)^{-1} \mathbf{b})^{1/2}}.$$
 (5.30)

It is clear that the critical value depends on the angle  $\theta^*$ , the degree of freedom  $\nu$  and the given confidence level  $1 - \alpha$ , where  $\theta^*$  is half the angle between  $P\mathbf{a}$  and  $P\mathbf{b}$  with P consistently defined as before.

Similar argument can be applied to the approximate method, the key of which is to compute the length of the path on the surface of the unit sphere in  $\mathcal{R}^n$ . So we are interested in finding the relationship between the length of the path and the angle  $\theta^*$ .

For linear regression models, vector l(x) in the approximate method has the explicit form given by

$$l(\mathbf{x}) = X(X^T X)^{-1} \mathbf{x} = X P^T P \mathbf{x},$$

where X is the design matrix,  $\mathbf{x}$  is the vector of the covariates, and

$$\|\mathbf{l}(\mathbf{x})\| = \left[\mathbf{l}(\mathbf{x})^T \mathbf{l}(\mathbf{x})\right]^{\frac{1}{2}} = \left[\mathbf{x}^T (X^T X)^{-1} \mathbf{x}\right]^{\frac{1}{2}} = \|P\mathbf{x}\|.$$

Then we have

$$\mathbf{T}(\mathbf{x}) = \frac{\mathbf{l}(\mathbf{x})}{\|\mathbf{l}(\mathbf{x})\|} = \frac{XP^T \cdot P\mathbf{x}}{\|P\mathbf{x}\|} = XP^T \cdot \boldsymbol{\gamma}(\mathbf{x})$$

by studying (5.4) for Naiman's method. Furthermore, we have

$$\begin{split} \|\mathbf{T}'(\mathbf{x})\|^2 &= \left[\mathbf{T}'(\mathbf{x})\right]^T \left[\mathbf{T}'(\mathbf{x})\right] \\ &= \left[\boldsymbol{\gamma}'(\mathbf{x})\right]^T P X^T \cdot X P^T \left[\boldsymbol{\gamma}'(\mathbf{x})\right] \\ \cdot &= \left[\boldsymbol{\gamma}'(\mathbf{x})\right]^T \left[P(P^T P)^{-1} P^T\right] \left[\boldsymbol{\gamma}'(\mathbf{x})\right] \\ &= \left[\boldsymbol{\gamma}'(\mathbf{x})\right]^T I_p \left[\boldsymbol{\gamma}'(\mathbf{x})\right] = \|\boldsymbol{\gamma}'(\mathbf{x})\|^2, \end{split}$$

which implies that

$$\|\mathbf{T}'(\mathbf{x})\| = \|\boldsymbol{\gamma}'(\mathbf{x})\|.$$
 (5.31)

Thus, by assuming the only predictor variable  $x \in [a, b]$ , since the length of the path

$$\Lambda(\boldsymbol{\gamma}) = \int_{a}^{b} \|\boldsymbol{\gamma}'(\mathbf{x})\| dx = \int_{a}^{b} \|\mathbf{T}'(\mathbf{x})\| dx = \kappa_{0}, \qquad (5.32)$$

then we obtain the equivalence between the length of the path in Naiman's method and that in the approximate method of Sun and Loader (1994).

In particular for simple linear regression case, the path in Naiman's method is on the unit circle, which, in connection with the fact that  $2\theta^*$  is equal to the angle between the two unit vectors starting from the origin and pointing to the two ends of the path, implies that  $2\theta^* = \Lambda(\gamma) = \kappa_0$ .

Therefore, formula (5.17) becomes

$$\alpha = \frac{2\theta^*}{\pi} (1 + \frac{c^2}{\nu})^{-\nu/2} + \mathbb{P}\{|t_\nu| > c\},$$
 (5.33)

where  $t_{\nu}$  is a *t* random variable with  $\nu$  degrees of freedom. Clearly, the critical value depends on  $\theta^*$ ,  $\nu$ ,  $1 - \alpha$  as well.

For the simulation-based method, a suitable manipulation simplifies the computation of T defined in (5.24). Define  $\mathbf{U} = (U_1, U_2)^T = \mathbf{N}/||\mathbf{N}||$ , where  $\mathbf{N} = (P^T)^{-1}(\hat{\boldsymbol{\beta}} - \boldsymbol{\beta})/\sigma$ . Let  $u_1$  and  $u_2$  be the generated values of random

variables  $U_1$  and  $U_2$ . Then, under the definition of  $\phi^* = 2\theta^*$ , T can be calculated in the following way:

$$T = \begin{cases} \frac{\|\mathbf{N}\|}{(\hat{\sigma}/\sigma)} & \text{if } |u_1| \ge \cos\frac{\phi^*}{2}, \\ \frac{\|\mathbf{N}\|}{(\hat{\sigma}/\sigma)} |u_1 \cos\frac{\phi^*}{2} + u_2 \sin\frac{\phi^*}{2}| & \text{if } 0 \le u_1 < \cos\frac{\phi^*}{2}, u_2 > \sin\frac{\phi^*}{2} \\ & \text{or } -\cos\frac{\phi^*}{2} < u_1 < 0, u_2 < -\sin\frac{\phi^*}{2}, \\ \frac{\|\mathbf{N}\|}{(\hat{\sigma}/\sigma)} |u_1 \cos\frac{\phi^*}{2} - u_2 \sin\frac{\phi^*}{2}| & \text{otherwise.} \end{cases}$$

By following the procedure stated in Section 5.3, an approximation of the critical value can be found. Also, one may calculate the standard error accordingly. Overall, all these methods depend on  $\theta^*$ ,  $\nu$  and  $1 - \alpha$ .

Now, we design the levels for these three factors. Since  $\theta^* \in [0, \pi/2]$ , set  $\theta^* = 0.0, 0.1, 0.2, \cdots, 1.3, 1.4, 1.5, 1.57$ . Set the degree of freedom  $\nu = 2, 4, 6, 8, 10, 15, 20, 30, 40, 60$ , from small to large, to see how this factor affects the critical value. In addition, the three most popular confidence levels 90%, 95%, 99% are used. Tables 5.1-5.10 contain the critical values computed based on these methods. The simulation results are based on 100,000 simulations. Results with a star behind in the tables are based on 200,000 simulations in order to make the distinction more clear.

From the results, we can draw some conclusions. For each method, the critical value increases with the angle  $\theta^*$  and the confidence level, and decreases with the degree of freedom. The critical values based on the approximate method are generally larger than those of the exact method, good enough when  $\theta^*$  takes small values, but being worse and worse as  $\theta^*$  goes large. This trend becomes less and less evident as  $\nu$  goes large, but the gap still exists clearly. The simulation-based method computes as good critical values as the exact method. The difference between the critical values of the simulation-based method and those of the approximate method is basically at the second or third decimal place, increasing with the confidence level and decreasing with the degree of freedom.

d.f. = 2
----------

. . . .

cl	8*	cv ext	cv nai	cv app	cv simu	5.e.	1
	0.00	2.9200	2.9200	2.9200	2.9103	0.0153	1
	0.10	3.1200	3,1200	3.1208	3.1125	0.0161	
-	0.20	3,3055	3,3055	3.3114	3.2976	0.0210	Ł
- A - 1	0.30	3.4746	3.4746	3,4927	3.4589	0.0128	
	0.40	3.6260	3,6260	3,6660	3,6050	0.0132	*
	0.50	3,7592	3,7592	3.8321	3,7489	0.0137	
	0.60	3.8742	3.8742	3.9918	3,8454	0.0228	
	0.70	3 9712	3 9712	4 1458	3,9522	0.0190	
90%	0.80	4 0509	4 0509	4 2945	4 0505	0.0154	*
0070	0.00	1 1112	4 1140	4 4385	4 1056	0.0211	
	1.00	4 1692	1 1622	4 5782	4 1489	0.0215	1
	1 10	d 1060	4 1969	4 7140	A 1971	0.0147	
	1.10	4 9200	4 2200	1 9450	4.2068	0.0190	
	1.20	4.2200	4.2200	4.0435	4.2000	0.0130	
	1.30	4.2331	4.2331	4.3140 £ 1000	4.1075	0.0103	1
	1.40	4.2404	4.2404	5.1000	4.2230	0.0223	1
	1.50	4:2420	4.2423	5 2067	4 2422	0.0202	
-	1.37	4.2421	4.2421	3.3007	4.2432	0.0109	-
	0.00	4.3021	4.3025	4.3027	4.2014	0.0302	
	0.10	4.5016	4.5015	4.5020	4.5012	0.0299	4
	0.20	4.8403	4 8403	4:04/8	4.63/4	0.0344	١.
	0.30	5.0765	5.0765	5.1000	5.0591	0.0306	ľ
1.42	0.40	5.2887	5.2887	5.3408	5.2892	0.0453	
	0.50	5.4761	5.4761	5.5718	5.4712	0.0331	
-	0.60	5.6386	5.6386	5.7937	5.6107	0.0281	ľ
	0.70	5.7760	5.7758	6.0078	5.7418	0.0393	4
95%	0.80	5:8892	5.0892	6.2149	5.7967	0.0402	1
	0.90	5.9794	5.9794	6.4152	5.9549	0.0455	1
	1.00	6.0486	6.0484	6.6097	6.0284	0.0317	1
	1.10	6.0984	6.0984	6.7988	6.0639	0.0453	
	1.20	6.1317	6.1317	6.9828	6.1348	0.0553	
	1.30	6.1516	6.1516	7.1621	6.1127	0.0521	1
	1.40	6.1611	6.1611	7.3372	6.1565.	0.0310	ľ
	1.50	6.1641	6.1641	7.5082	6 1580	0.0297	ľ
	1.57	6.1643	6.1643	7.6256	6.1350	0.0479	
	0.00	9.9249	9.9247	9.9249	9.8140	0.0662	7
	0.10	10.5420	10.5420	10.5441	10.6691	0.1004	ł
	0.20	11.1141	11.1141	11.1295	11.1316	0.1312	
	0.30	11.6370	11.6370	11.6858	11.5289	0.0833	
	0.40	12,1081	12,1079	12.2173	12.0785	0,1430	1
	0.50	12 5250	12 5250	12 7267	12,5740	0.4441	
	0.60	12 8872	12 8872	13,2167	12,7368	0.2089	
	0.70	13 1949	13 1947	13.6891	13,2957	0.1347	1
200	0.80	13 4491	13 4491	14 1460	13 0626	0 1170	1
0010	0.00	13:6525	13 6523	14 5885	13 1477	0 2324	1
	1.00	13 8082	13.8082	15 0182	13 7085	0.1167	ŀ
	1 10	13 0213	13 9911	15 4350	14 2853	0 3344	
	1 20	12 9020	13 0020	15 8405	14 0068	0 2136	
	1.20	14 0440	11.0320	16.0204	14.0000	0.24.00	
	1.30	14.0413	14.04 13	16 6969	13 9603	0.1014	1
	1.40	14.0039	14.0037	17 0017	14 0654	0.2142	
	1.50	14.0702	14.0705	17.004/	44.0000	0.4750	
	1.40 1.50 1.57	14.0639 14.0707 14.0713	14.0637 14.0705 14.0713	16.6263 17.0047 17.2645	13.8603 14.0654 14.0603	0.1011 0.2143 0.1750	

Table 5.1: Critical values for simple linear regression

d.f. = 4

ŧ

ς.

cl	8*.	cv_ext	cv_nai	cv app	cv_simu	5.8.
1111	0:00	2.1319	2.1317	2.1319	2.1250	0.0057
	0.10	2.2505	2.2503	2.2505	2.2515	0.0091
19	0.20	2.3590	2.3590	2.3592	2.3604	0.0092
	0.30	2.4583	2.4583	2.4594	2.4575	0.0090
	0.40	2:5485	2,5485	2.5523	2.5432	0.0065
	0.50	2,6293	2,6293	2,6290	2.6265	0.0066
	0.60	2,7006	2,7006	2.7202	2,6980	0.0067
	0.70	2,7618	2.7618	2,7967	2,7504	0.0063
90%	0 80	2.8131	2 8131	2.8688	2.8160	0.0077
	0.90	2 8545	2 8545	2 9372	2 8503	0.0100
	1.00	2 8865	2 8865	3 0022	2 8654	0.0101
	1 10	2 9097	2 9097	3 0642	2 9063	0.0097
	1 20	2 9254	2 9954	3 1234	2 9224	0.0108
	1 30	2:03/0	2 9349	3 1803	2 9360	0 0074
3	1.00	2 8305	2 0203	3 2348	2 9/35	0.0072
	1.40	2.3.330	2.0000	3 2972	2 0364	0.0411
	1.57	2.5400	2.0400	2.3997	2.3304	0.0073
	1.07	0 7766	0 7765	3.3221	2.3324	0.0014
	0.00	2.1100	2.1100	2.1103	2.7770	0.0130
	0.10	2.9147	2.5145	2.3141	2.3013	0.0132
	0.20	3.0403	3.0403	3.0405	3.0137	0.0454
	0.30	3.1049	3.1049	0.1000	3 1362	0.0101
	0.40	3:2592	3.2592	3.2020	3.2500	0.0124
	0.50	3.3532	3.3532	3.3619	3.3510	0.0169
	0:60	3.4367	3.4367	3.4550	3.4397	0.0146
-	0.40	3.5091	3.5091	3.5423	3.5132	0.0100
95%	0.80	3:5703	3.5701	3.6248	3.5739	0.0160
	0.90	3.6201	3.6201	3.7030	3.6169	0.0108
	1.00	3.6591	3.6591	3.7773	3.6472	0.0172
	1.10	3.6877	3.6877	3.6463	3.6765	0.0148
	1.20	3.7074	3.7074	3.9161	3.7095	0.0110
	1.30	3.7190	3.7190	3.9809	3.7099	0.0168
	1.40	3.7247	3.7247	4.0433	3.7119	0.0193
	1.50	3.7266	3.7266	4.1033	3.7181	0.0148
-	1.57	3.7268	3.7268	4.1441	3.7210	0.0112
	0.00	4.6041	4.6040	4.6041	4.5947	0.0305
	0.10	4.8056	4.8056	4.8056	4.8122	0.0425
	0.20	4.9873	4.9873	4.9875	4.9801	0.0385
	0.30	5.1526	5.1526	5.1536	5.1292	0.0316
	0.40	5.3030	5,3030	5.3065	5.2951	0.0321
	0.50	5.4391	5.4391	5,4485	5.4124	0.0357
	0.60	5.5608	5.5608	5.5812	5.5327	0.0420
	0.70	5.6677	5.6675	5.7058	5.6595	0.0279
99%	0:60	5.7588	5.7588	5.8235	5.7466	0.0320
1000	0.90	5.8343	5,8343	5.9348	5.8554	0.0351
	1.00	5,8940	5,8940	6.0408	5,8222	0.0315
	1.10	5,9386	5.9384	6.1418	5.8970	0.0347
-	1.20	5.9691	5,9691	6,2385	5,9874	0.0324
	1.30	5,9876	5.9876	6.3311	5,9580	0.0445
	1.40	5.9970	5.9968	6.4202	5.8860	0.0428
	1.50	5 9998	5,9998	6.5058	5.9738	0.0499
	1.57	6 0000	6 0000	6 5630	6 0047	0.0339

Table 5.2: Critical values for simple linear regression

d.f.	-	6	
------	---	---	--

,

٢

.

.

cl :	8	cv ext	cv nai	cy app	cv simu	5.8.	
	0.00	1.9432	1.9432	1.9432	1.9493	0.0050	٦,
	0.10	2.0440	2.0440	2.0440	2.0332	0.0067	
	0.20	2.1354	2.1354	2.1354	2.1297	0.0068	4
	0.30	2,2183	2.2183	2.2185	2.2007	0.0071	
	0.40	2 2938	2 2938	2 2947	2 2944	0.0048	1
	0.50	2 3618	2 3618	2 3653	2.3559	0 0072	
	0.60	2 4225	2 4225	2 4305	2 4215	0.0076	
	0.00	2 4749	2 4749	2 4917	2 4669	0.0081	
00%	0.80	2 5193	2 5193	2 5483	2 5155	0.0074	
3070	nan	2 5553	2.5155	2 6010	2 5490	0 0077	
	1.00	2.5535	2.5555	2.6694	2 5851	0 0072	
	1.00	2.0000	2.0030	2,0524	2.5051	0.0072	
	1.10	2.0041	2.0041	2.7.000	2.0010	0.0027	
	1.20	2.0101	2.0101	2.7404	2.0232	0.0053	
	1.30	2.6264	2.6264	2.1861	2.0231	0.0004	
	1.40	2.6305	2.6305	2.8299	2.6346	0.0079	
	1.50	2.6318	2.6318	2.8693	2.6318	0.0076	
	1.57	2.6318	2.6318	2.8958	2.6295	0.0075	-
	0.00	2.4469	2.4469	2.4469	2.4509	0:0071	
11. 11.3	0.10	2.5578	2.5578	2.5578	2.5564	0.0105	
	0.20	2.6573	2:6573	2.6573	2.6526	0.0116	
	0.30	2.7471	2.7471	2.7473	2.7410	0.0079	1
	0.40	2.8287	2:8287	2.8295	2.8263	0.0074	
	0.50	2.9027	2.9025	2.9050	2.8947	0.0098	
	0.60	2.9686	2.9686	2.9747	2.9650	0.0111	÷
	0.70	3.0268	3.0268	3.0398	3.0231	0.0075	
95%	0.80	3.0765	3.0765	3,1006	3.0686	0.0078	
	0.90	3:1175	3.1175	3.1578	3,1098	0.0114	
	1.00	3 1499	3 1499	3:2115	3.1458	0.0120	
	1 10	3 1742	3 1742	3 2626	3 1675	0 0113	
	1 20	3 1907	3 1906	3 3108	3 1882	0.0130	
	1 30	3 2007	3 2007	3 3570	3 1998	0 0088	
	140	3 2056	3 2056	3 4008	3 1871	0 0107	
	1 1 50	3 2074	3 2071	2 4428	3 2046	0.0103	
	1.50	2 2072	3 2072	3 1740	2 2002	0.0113	
	0.00	2 7073	2 7074	2 7074	3.6113	0.0750	-1
	0.00	3.1014	3.10/4 3 0404	3,1414	2 0214	0.0252	
	0.90	3.0404	3.0404	3.0404	3.0314	0.0207	
	0.20	3.9731	3.9731	3.37.31	3.5349	0.0204	
	0.30	4.0848	4.0847	4.0848	4.1056	0.0340	
	0:40	4,1857	4.185/	4.1861	4.1426	0.0319	
	0.50	4.2772	4.2770	4.2/8/	4.2697	0.0387	
	0.60	4.3597	4.3598	4.3641	4.3371	0.0239	
	0.70	4.4331	4.4331	4.4436	4.4598	0.0198	
99%	0.60	4.4972	4.4972	4.5176	4.5096	0.0200	
	0.90	4.5511	4.5511	4.5872	4.5135	0.0295	
	1.00	4.5946	4.5946	4.6528	4.5632	0.0298	
	1.10	4.6276	4.6276	4.7147	4.6103	0.0213	
	1.20	4.6507	4.6507	4.7736	4.6337	0.0260	
	1.30	4.6648	4.6648	4.8297	4.6455	0.0177	
	. 1.40	4.6718	4.6718	4.8830	4,6696	0.0302	
	1.50	4:6741	4.6741	4,9341	4.6181	0.0279	
	1 57	4 6743	4 6743	4,9686	4,6226	0.0380	

Table 5.3: Critical values for simple linear regression

d.f.	= 8
------	-----

-

(

-

cl	0 *	cv ext	cv nai	cv app	cv simu	6.8.
	0.00	1.8595	1.8595	1.8595	1.8595	0.0042
	0.10	1.9529	1.9527	1.9529	1.9519	0.0042
	0.20	2.0368	2,0368	2.0368	2.0312	0.0067
	0.30	2.1127	2.1127	2.1127	2,1130	0.0042
	0.40	2 1817	2 1817	2 1821	2.1706	0.0066
	0.50	2.2440	2 2440	2 2456	2 2442	0.0066
	0.60	2 2997	2 2995	2 3043	2 2969	0.0066
	0.70	2 3483	2 3481	2 3586	2 3432	0.0067
90%	0.80	2 3895	2.3895	2 4093	2 3910	0.0066
00 10	0.00	2 4232	2 4232	2.4568	2.1299	0.0065
	1.00	2 4195	2 1495	2 5012	2 1151	0 0046
	1 10	2 4690	2 4690	2 5431	2 4628	2200.0
	1.10	2.4030	2.4000	2 5830	2 4847	0.0065
	1 30	2.4021	2.4021	2.0000	2.4047	0.0000
	1.30	2:4301	2,4301	2.0200	2.4030	0.0003
	1.40	2.4540	2,4540	2.0304	2.4310	0.0007
	1.50	2.4931	2.4951	2.0905	2.4050	0.0040
	1.57	2.4955	2.4903	2./130	2.4009	0.0000
	0.00	2.3060	2.3050	2.3000	2.3095	0.0002
	0.10	2.4059	2.4059	2.4059	2.4.108	0.0002
	0.20	2.4945	2.4945	2.4945	2.4903	0.0087
	0.30	2.5/42	2.5/42	2.5142	2,5867	0.0095
	0.40	2.6463	2 6463	2.6465	2.6494	0.0065
	0.50	2.7115	2.7115	2.7124	2.7051	0.0095
	0.60	2.7700	2.7700	2.7731	2.7703	0.0091
	0.70	2.8220	2.8219	2.8291	2.8165	0.0062
95%	0.80	2.8667	2.8667	2.8813	2.8604	0.0073
	0.90	2.9040	2.9038	2.9303	2.9002	0.0070
	1.00	2.9336	2.9336	2.9761	2.9251	0.0090
	1.10	2.9557	2.9557	3.0192	2.9374	0.0085
	1.20	2.9709	2.9709	3.0602	2.9540	0.0097
	1.30	2.9801	2.9801	3.0989	2.9768	0.0083
	140	2.9847	2.9847	3.1356	2.9777	0.0086
	1.50	2.9862	2.9862	3.1707	2.9708	0.0068
1.1.1	1.57	2.9864	2.9864	3.1944	2.9846	0.0073
-	0.00	3.3555	3.3553	3.3555	3.3605	0.0144
	0.10	3.4740	3.4740	3.4740	3.4398	0.0213
	0.20	3.5776	3.5776	3.5776	3,5720	0.0157
	0.30	3.6694	3.6694	3,6694	3.6514	0.0144
	0.40	3,7518	3.7518	3 7520	3.7517	0.0221
	0.50	3 8263	3 8263	3 8267	3.7964	0 0205
	0.60	3 8936	3 8936	3 8953	3 8705	0 0143
	0.70	3 9543	3 9541	3.9586	3 9/31	0.0203
9996	0.00	4 0074	4 0073	4 0174	4 0125	0.0167
55.70	0.00	1 0528	4.0526	1 0791	4 11393	0.0169
	1 00	4.0020	4:000D	1 1235	1 0885	0.0257
	1.00	4.0050	1 1190	4 1720	4 1174	0.0237
	1.10	4.1102	4.1102	4.1120	4.1171	0.02.33
	1.20	4.1302	4.1302	4.21/1	4.12/3	0.0100
	1.30	4.1506	4.1506	4.2010	4.1595	0.0213
	1.40	4.1569	4.1569	4.3022	4.1405	0.0161
	1.50	4.1590	4.1590	4.3416	4.14.54	0.0141
E	1.57	4.1592	4.1592	4.3679	4.1477	0.0178

Table 5.4: Critical values for simple linear regression

d.f.	-	10	
------	---	----	--

,

c1	8	cv ext	cv nai	cv_app	cv_simu	5.8.
	0.00	1:8124	1.8124	1.8124	1.8109	0.0041
1	0.10	1.9016	1.9016	1.9016	1.8993	0.0044
an l	0.20	1.9815	1.9813	1.9815	1.9797	0.0060
	0.30	2.0534	2.0534	2.0536	2.0490	0.0060
	0.40	2.1188	2,1188	2,1190	2,1180	0.0058
	0.50	2.1779	2.1777	2.1788	2,1791	0.0041
	0.60	2,2307	2 2307	2,2337	2,2320	0.0041
	0.70	2 2770	2 2778	2 2846	2 2773	0 0060
90%	0.80	2 3165	2 3165	2 3319	2 3120	0 0056
	n 9n	2 3489	2 3489	2 3759	2 3485	0.0064
1	1.00	2 3744	2 3744	2 4173	2 3750	0.0064
	1 10	2 3931	2 3931	2 4562	2 3852	0.0064
-	1.20	2 4059	2 4059	2 4928	2 3958	0.0059
	1 30	2.4000	2 4135	2 6976	2 4134	0.0000
	1.30	2.4155	2 4474	2.5605	2.4140	0.0002
	1.40	2.4.171	2.4171	2.0000	2.4 140	0.0050
1.1	1.50	2.4 103	2.4103	2.0210	2.4 135	0.0007
	1.07	2.4 100	2.4100	2.0129	2.4111	0.0003
	0.00	2.2282	2.2280	2.2282	2.2162	0.0011
	0.10	2.3220	2.3220	2.3220	2.3101	0.0006
	0.20	2.4049	2.4049	2.4049	2.4042	0.0003
	0.30	2.4/91	2.4791	2.4791	24/90	0.0084
	0.40	2.5458	2.5458	2.6460	2.5236	0.0085
	0.50	2.6064	2.6062	2.6068	2.5976	0.0077
	0.60	2.6608	2.6608	2.6627	2.6513	0.0087
	0.70	2.7092	2.7092	2.7140	2.7092	0.0093
95%	0.80	2.7511	2.7511	2.7616	2.7382	0.0084
	0.90	2.7862	2.7862	2.8062	2.7853	0.0092
2. 1. 3	1.00	2.8142	2.8142	2.8478	2.8124	0.0090
	1.10	2.8354	2.8352	2.8869	2 8332	0.0087
	1.20	2.8499	2.8499	2,9237	2.8396	0.0087
	1.30	2.8586	2.8586	2.9585	2.8557	0.0086
	1.40	2.8630	2.8630	2.9917	2.8585	0.0064
	1.50	2,8644	2.8644	3.0232	2.8607	0.0060
	1.57	2.8646	2.8646	3.0443	2.8595	0.0088
1.	0.00	3.1692	3.1692	3.1692	3.1669	0.0194
	0.10	3.2765	3.2763	3,2765	3.2794	0.0123
1.1	0.20	3,3692	3.3692	3,3692	3,3656	0.0190
	0.30	3.4510	3,4510	3,4510	3,4360	0.0146
	0.40	3 5238	3 5238	3.5240	3.5137	0.0165
•	0.50	3 5896	3 5896	3 5898	3.5688	0.0218
	0.60	3 6490	3 6490	3 6498	3 6539	0.0154
	0.00	3 7026	3 7026	3 7051	3 7003	0.0196
99%	0.90	3 7501	3 7501	3 7562	3 7300	0.0132
3370	0.00	3 7000	3 7900	3 9036	3 7711	0.0214
5	1.00	2 0244	2 9244	2 8470	3 8440	0.0214
	1.00	2.0244	3.0244	3.04/5	3.0110	0.0150
	1.10	3.0000	3.0000	3.0090	3.0230	0.0100
	1.20	3.0690	3.0000	3.9289	3.0025	0.0130
	1.30	3.8805	3.8805	3.9667	3.8943	0.0196
	1.40	3.8862	3.6862	4.0013	1.8573	0.0140
	1.50	3.8881	3,0881	4.0347	3.8726	0.0168
- Conne	1.57	3.8883	3.8883	4.0574	3,8596	0.0141

Table 5.5: Critical values for simple linear regression

d.f.	-	15	
------	---	----	--

(

,

cl	0 *	cv. ext	cv nai	cv app	cv simu	5.e.	
	0.00	1.7531	1.7529	1.7531	1.7534	0.0052	
1	0.10	1.8370	1.8370	1:8370	1.8343	0:0057	4
5	0.20	1.9119	1.9117	1.9119	1.9117	0.0038	3
	0.30	1.9790	1.9790	1.9790	1.9792	0.0056	
	0.40	2.0397	2,0397	2.0397	2.0383	0.0052	1
1	0.50	2.0946	2.0946	2.0949	2.0905	0.0054	1
	0.60	2,1439	2.1439	2.1455	2,1505	0.0053	
	0 70	2 1874	2 1874	2 1922	2 1846	0.0040	-
90%	0.80	2 2246	2 2246	2 2353	2 2218	0.0040	1
	0.90	2 2553	2 2553	2 2753	2 2532	0.0038	
	1.00	2 2795	2 2795	2 3127	2 2812	0.0057	
	1 10	2 2974	2 2974	2 3477	2 2955	0.0041	
	1.20	2 3096	2 3096	2 3807	2 3078	0.0051	1
	1 30	2 3169	2 3169	2 4118	2 3174	0.0039	1
	1.40	2 3205	2 3205	2 4413	2 3193	0.0057	
-	1.60	2 3246	2 3216	2 4692	2 3120	0.0055	
	1.50	2.3210	0 1010	2.4032	2 2157	0.0000	
	0.00	2.1210	2.3210	2.4013	2.3107	0.0000	
	0.00	2.1314	0.0470	2.1314	2.1300	0.0030	
	0.10	2.21/0	2.2113	2.2113	2.2.104	0.0075	
-	0.20	2.2940	2.2940	2.2340	2.2040	0.0075	
	0.30	2.3015	2.3015	2:3015	2.3491	0.0003	
de stille	0.40	2.4219	2.4219	2:4219	2.4201	0.0069	
1000	0.50	2.4764	2.4764	2.4766	2.4662	0.0049	
	0.60	2.5256	2.5256	2.5264	2.5222	0.0055	
	0.70	2.5696	2.5696	2.5/23	2.5621	0:00/3	
95%	0.80	2.6081	2.6081	2.6144	2.6142	0.0049	
	0.90	2.6406	2.6406	2.6537	2.6263	0.0078	4
	1.00	2.6665	2.6665	2.6903	2.6668	0.0071	1
	1.10	2.6653	2.6863	2.7246	2.6893	0.0051	
-	1.20	2.6998	2.6998	2.7568	2.6953	0.0053	
a - 1	1.30	2.7082	2.7082	2.7872	2.7061	0:0077	
	1.40	2.7124	2.7124	2.8159	2.7093	0.0082	÷,
	1.50	2.7138	2.7138	2.6432	2.7090	0.0079	9
-	1.57	2.7138	2.7138	2:8613	2.7086	0.0076	
	0.00	2.9467	2.9467	2.9467	2.9381	0.0159	i.
	0.10	3.0405	3.0405	3:0405	3.0364	0.0098	i,
	0.20	3.1208	3.1208	3.1208	3.1187	0.0185	1
	0.30	3.1907	3.1907	3.1907	3.1902	0.0175	1
	0.40	3.2529	3.2529	3.2529	3.2611	0.0145	
	0:50	3.3084	3.3084	3.3084	3.2960	0.0133	
	0.60	3.3585	3.3585	3.3587	3:3569	0.0112	
	0.70	3.4039	3.4039	3.4048	3.3911	0.0153	
99%	0.80	3.4445	3.4443	3.4472	3.4244	0.0149	
and a second	0.90	3.4796	3.4796	3.4862	3,4700	0.0140	
	1.00	3.5091	3.5089	3.5226	3.4641	0.0149	
	1.10	3.5320	3.5320	3,5568	3.5154	0.0116	
	1.20	3.5486	3.5486	3.5888	3.5527	0.0112	
	1.30	3.5591	3.5591	3,6189	3,5614	0.0117	
	1.40	3 5644	3 5644	3 6475	3 5767	0.0106	
	1.50	3 5661	3 5661	3 6746	3 5595	0.0148	
	1.00	1 9,9001	2.0001	0.0170	0.0000	2.2.30	

Table 5.6: Critical values for simple linear regression

d.f.	=	20
------	---	----

١

Carl Street			the second se	the second se	and the second se	
90%	0.00	1.7247	1.7247	1.7247	1,7089	0.0050
	0.10	1.8063	1.8063	1.8063	1.7968	0.0052
	0.20	1.8788	1.8788	1.8788	1.8790	0.0036
	0.30	1.9436	1.9436	1.9436	1.9479	0.0036
	0.40	2.0021	2.0021	2.0021	1:9982	0.0036
	0.50	2.0549	2.0549	2.0553	2.0568	0.0054
	0.60	2,1026	2.1026	2.1037	2.1032	0.0052
	0 70	2.1447	2.1447	2,1483	2.1361	0.0053
	0.80	2,1809	2.1807	2.1895	2.1810	0.0035
	0.90	2,2109	2,2109	2 2276	2 2071	0.0055
	1.00	2 2343	2 2343	2,2633	2,2308	0.0053
	1 10	2 2518	2 2518	2 2966	2 2488	0.0037
	1 20	2 2639	2 2637	2 3279	2 2627	0.0050
	1 30	2 2709	2.2709	2 3573	2 2667	0.0055
	1.10	2 2745	2 2743	2 3951	2 9747	0.0052
	1.40	2,2145	2.2145	2.0001	2 2600	0.0051
	1.50	2.2155	2.2155	9 4901	2 2675	0.0001
10 10	0.00	2.2751	2.21.07	2.4231	2.2010	0.00.04
	0.00	2.0000	2.0000	2.0000	2.0030	0.0049
	0.10	2.1091	2.1051	2.1031	2.1007	0.0040
	0.20	2.2419	2.2417	2.2413	2.2200	0.0005
	0:30	2.3062	2.3062	2.3002	2 2901	0.0045
	0.40	2.3037	2.3637	2.3031	2.3619	0.0046
95%	0.50	2.4156	24156	2.4156	2.4111	0.0067
	0.60	2.4623	2.4623	2.4629	2.4601	0.0077
	0.70	2:5043	2.5043	2.5060	2:5206	0.0072
	0.80	2.5410	2:5410	2.5458	2.6422	0.0078
	0.90	2 5721	2.5721	2.5828	2.5706	0.0073
	1.00	2.5973	2.5973	2.6169	2.5910	0.0072
	1.10	2.6163	2.6163	2.6491	2.6059	0.0071
	1.20	2.6295	2.6295	2.6791	2.6313	0.0065
1.01	1.30	2.6377	2.6377	2.7075	2.6363	0.0072
	1 40	2.6417	2.6417	2.7342	2.6425	0.0049
	1.50	2.6428	2.6428	2.7595	2.6501	0.0050
	1.57	2:6430	2.6430	2 7765	2.6449	0.0069
	0.00	2.8453	2.8453	2.8453	2.8386	0.0099
	0.10	2.9332	2.9332	2.9332	2.9225	0.0124
	0.20	3.0079	3.0079	3.0079	2.9913	0.0152
99%	0.30	3.0727	3.0727	3.0727 -	3.0766	0:0147
	0.40	3.1299	3.1299	3.1299	3.1259	0.0104
	0.50	3,1810	3.1810	3.1810	3,1807	0.0141
	0.60	3.2272	3.2270	3.2272	3.2252	0.0144
	0.70	3.2687	3.2687	3.2691	3.2535	0.0096
	0.80	3.3051	3.3059	3.3076	3.3163	0.0095
	0.90	3,3387	3.3387	3.3433	3,3333	0.0090
	1.00	3,3661	3.3661	3,3762	3.3479	0.0128
	1.10	3,3879	3,3879	3,4071	3.3824	0.0100
	1 20	3 4035	3 4035	3 4359	3 3848	0.0120
	1.30	3 4 1 3 4	3 4134	3 1632	3 4028	0 0101
	1.40	3 4 184	3 4 184	3 4887	3.4343	0.0129
	1.50	3 4201	3 4201	3 5120	3 4159	0.0155
	1.57	3 4201	3 4003	3 6204	3,4949	0.0100

Table 5.7: Critical values for simple linear regression

.

d.f. = 30

ł

.

cl	9	cv ext	cv nai	cv app	cv simu	5.8.	
90%	0.00	1.6973	1.6973	1.6973	1.6983	0.0037	
	0.10	1.7764	1.7764	1.7764	1.7752	0.0048	1
	0:20	1.8467	1.8467	1.8467	1.8450	0.0049	3
	0.30	1.9095	1.9095	1.9095	1.9041	0.0049	
	0.40	1.9659	1.9657	1.9659	1.9601	0.0049	1
	0.50	2.0168	2.0168	2.0168	2.0162	0.0047	
	0.60	2.0625	2:0625	2.0633	2.0614	0.0035	5
	0.70	2.1033	2.1033	2.1060	2.1053	0.0034	9
	0.80	2.1384	2.1384	2.1455	2.1268	0.0047	
	0.90	2.1676	2.1575	2.1819	2.1665	0.0049	
	1.00	2,1906	2,1906	2.2156	2.1866	0.0050	1
	1.10	2,2078	2.2078	2.2473	2.2041	0.0051	
	1.20	2.2194	2.2194	2.2770	2,2183	0.0037	
	1.30	2,2265	2.2265	2,3048	2,2208	0.0036	
	1.40	2,2299	2 2299	2 3311	2,2285	0.0050	
	1.50	2 2309	2 2309	2 3561	2 2332	0 0048	
	1 57	2 2314	2 2311	2 3729	2.2239	0 0047	
95%	0.00	2.0423	2 0423	2 0423	2 6407	0 0046	٦
	0.00	2 1222	2 1999	2 1222	2 1204	0 0063	
	0.20	2 1970	21918	2 1920	2 1931	0 0069	
	0.20	2.0524	2.0534	2 2534	2 2496	0.0063	h
	0.00	2.2004	2.2004	2 2084	2 3010	0.00000	
	0.40	2.3001	2.3001	2.3001	2 3552	1200.0	
	0.50	2.3313	2.0010	2,3313	2,3332	0.0004	
	0.00	2.4017	2.4011	2.4021	2.4025	0.0045	
	0.00	5 4700	2.4410	0 4000	2:4000	0.0003	
	0.00	2.4/00	2,4/00	2.4002	2,4735	0.0002	
	1.00	2.0000	2.5005	2.0145	2.4330	0.0040	
	1.00	2.3307	2:0007	2.04/1	2.5252	0.0040	1
	1.10	2.3492	2.3492	2.0111	2.3301	0.0000	
	1.20	2.0020	2.5020	2,0001	2.0009	0.0002	2
	1.30	2.07.00	2.5/00	2.0310	2.3032	0.0040	
	1.40	2.5/38	2.5/38	2.5500	2.5766	0.0000	i,
	1.50	25/52	2.5752	2.6800	2.5050	0.0063	
	1.5/	2.5/52	2.5/52	2.6956	2.5/05	0.0000	2
99%	0.00	2.7500	2.7500	2.7500	2.1213	0.0081	
	0.10	2.8323	2:6321	2.8523	2.8278	0.0134	
	0.20	2.9019	2.9019	2.9019	2.8936	0.0120	
	0.30	2,9620	2.9620	2.9620	2.9523	0.0102	9
	0.40	3.0148	3.0148	3.0148	3:0035	0.0081	
	0.50	3.0617	3.0517	3.0617	3.0600	0.0113	
	0.60	3.1040	3.1040	3.1040	3.1005	0.0146	
	0.70	3.1421	3:1421	3.1423	3.1382	0.0104	
	0:80	3.1764	3.1763	3.1774	3.1838	0.0098	
	0.90	3.2066	3.2066	3.2096	3.2053	0.0137	
	1.00	3.2323	3.2321	3.2395	3.2264	0.0093	
	1.10	3.2525	3.2525	3.2674	3.2540	0.0093	
	1.20	3.2674	3.2674	3.2933	3.2507	0.0085	
	1.30	3.2769	3.2769	3.3179	3.2657	0.0086	
	1.40	3.2817	3.2817	3.3408	3.2828	0.0093	
	1.50	3.2832	3.2832	3.3627	3.2830	0.0116	
	1.57	3.2834	3.2834	3.3772	.3.2827	0.0165	

Table 5.8: Critical values for simple linear regression
d.f.	-	40
------	---	----

ι

c1	0.	cv_ext	cv_nai	cv_app	cv_simu	5.0.
	0.00	1.6839	1.6837	1.6839	1.6826	0.0050
	0.10	1.7619	1,7619	1.7619	1.7600	0.0035
	0.20	1.8311	1:8311	1.8311	1.8303	0.0047
	0.30	1.8927	1.8927	1.8927	1.8848	0.0044
	0.40	1.9482	1,9482	1.9482	1,9491	0.0051
	0.50	1.9981	1,9981	1.9981	2:0005	0.0035
	0.60	2.0431	2.0431	2:0437	2.0454	0.0033
- H	0.70	2 0831	2 0831	2 0854	2 0816	0.0032
90%	0.80	2 1178	2 1178	2 1239	2 1178	0 0045
	0.90	2 1466	2 1465	2 1596	2 1453	0.0034
2	1.00	2 1693	2 1693	2 1926	2 1699	0 0033
	1.10	2 1863	2 1863	2 2224	2 1804	0.0034
	1.10	2.1005	2 1003	2 2222	2 1067	0.0048
	1.20	2.13/1	2.1311	2.2322	2 1007	0.0054
	1.30	2.2040	2.2040	2.21.30	2.1037	0.0031
11 19-0	1.40	2.2000	2.2000	2.3000	2.2041	0.0047
	1.50	2.2091	2.2091	2.3232	2.2141	0.0045
	1.57	2.2093	2.2093	2.3454	2.2095	0.0033
	0.00	2.0212	2.0210	2.0212	2.0186	0.0064
	0.10	2.0995	2.0995	2.0995	2.0973	0.0045
	0.20	2.1678	2.1676	2.1678	2.1665	0.0046
	0.30	2.2278	2.2275	2.2278	2.2294	0.0062
	0.40	2.2812	2.2812	2.2812	2.2752	0.0044
	0.50	2.3291	2.3291	2.3292	2.3265	0.0041
	0.60	2.3723	2.3723	2.3725	2.3704	0.0041
2.16	0.70	2.4112	2.4112	2.4122	2.4056	0.0060
95%	0.80	2.4455	2.4455	2.4486	2.4385	0.0062
	0.90	2 4749	2.4749	2,4821	2.4643	0.0055
5	1.00	2.4987	2.4985	2.5134	2.4939	0.0059
	1.10	2.5168	2.5166	2.5424	2.5163	0.0062
	1.20	2.5294	2.5294	2.5694	2.5230	0.0043
3	1.30	2.5372	2.5370	2.5950	2.5366	0.0062
1	140	2.5410	2.5410	2.6190	2.5364	0.0061
111	1 50	2 5422	2 5422	2.6419	2:5422	0.0067
	1.57	2 5424	2 5424	2 6570	2 5437	0 0046
1.00.000	0.00	2 7044	2 7044	2 7044	2 7154	0.0082
	0.10	2 7841	2 7841	2 7841	2 7770	0.0123
	0.20	2 8514	2 8514	2 8514	2 8459	0.0137
	0.20	2 8092	2.0014	2 9092	2 8942	0.0129
1.1	0.40	2.3032	2,3032	2.0002	2.0542	0.0125
1	0.40	2.5555	2.33333	2.0030	2.0000	0.01122
	0.00	3.0049	3.0043	2.0472	2.0330	0.0122
	0.00	3.0453	3.0403	3.0433	3.0400	0.0001
0001	0.70	3.0619	3.0017	3.0015	3.0/33	0.0050
99%	0.80	3.1147	3.1147	3.1154	3.1104	0.0100
	0.90	3.143/	3.143/	3.1461	3.1421	0.0112
	1.00	3.1684	3.1684	3.1745	3.15/9	0.0094
	1 10	3.1883	3,1883	3,2010	3.1813	0.0105
	1.20	3.2026	3.2026	3.2258	3,1946	0.0124
	1.30	3.2119	3.2119	3.2489	3.2015	0.0137
1.1	1.40	3.2165	3.2165	3.2708	3.2098	0.0109
1.	1.50	3.2182	3.2180	3.2914	3.2158	0.0090
	1.57	3.2182	3,2182	3,3051	3.2170	0.0138

Table 5.9: Critical values for simple linear regression

ι

cl	8	cv_ext	cv_nai	cv_app	cv_simu	5.8.	
	0.00	1.6706	1.6706	1.6706	1.6652	0.0034	3
	0.10	1.7476	1.7476	1.7476	1.7516	0.0046	1
	0.20	1.8157	1.8157	1.8157	1.8133	0.0035	
	0.30	1.8763	1.8763	1.8763	1.8713	0.0046	
	0.40	1.9306	1,9306	1.9306	1.9281	0.0034	
	0.50	1,9798	1.9798	1.9798	1.9856	0.0050	
	0.60	2.0240	2.0240	2.0244	2.0237	0.0045	
	0.70	2 0633	2 0633	2 0654	2 0608	0.0045	1
90%	0.80	2 0974	2 0974	2 1030	2 0955	0.0034	
50 %	ngn	2 1258	2 1258	2 1377	2 1232	0 0045	
	1.00	2.12.00	2 1493	2 1600	2 1463	0.0049	
	1.00	2 1405	2 1400	2,1033	2 1642	0.0024	
	1.10	2.1043	2.1049	2.2000	2.1042	0.0034	1
	1.20	2.1/64	2.1764	2.2200	2.1140	0.0044	
	1.30	2.1832	2.18.32	2.2545	2.1020	0.0033	1
	1.40	2.1866	2.1866	2.2795	2.1846	0.0045	9
	1.50	2.1878	2.1878	2.3029	2.1863	0.0035	
	1.57	2.1878	2.1878	2.3186	2.1904	0.0047	
	0.00	2.0004	2.0002	2.0004	1.9950	0.0066	
	0.10	2.0772	2.0772	2.0772	2.0780	0.0042	
	0.20	2.1439	2.1439	2.1439	2.1384	0.0062	1
	0.30	2.2027	2.2027	2.2027	2 1996	0:0046	
	0.40	2.2549	2.2547	2.2549	2.2589	0.0058	
	0:50	2:3016	2.3016	2.3016	2.3008	0.0042	
	0.60	2.3437	2.3437	2.3437	2.3415	0.0047	
	0.70	2.3817	2.3817	2.3822	2.3841	0.0044	
95%	0.80	2.4150	2.4150	2,4177	2.4180	0.0043	
	0.90	2.4438	2.4438	2.4501	2,4395	0.0056	
	1.00	2.4671	2:4671	2.4804	2.4702	0.0041	
	1 10	2 4850	2 4850	2 5084	2 4791	0 0041	
	1.20	2 4974	2.4974	2 5348	2 5028	0 0064	
	1 30	2 6060	2 5050	2 5593	2 5056	0.00043	
	1.40	2 5089	2.5030	2 5826	2 5078	0.0058	1
	1.40	2.5000	2.5000	2.0020	2.5070	0.0000	
	1.50	2.3100	2.0100	2.0043	2.3034	0.0001	
	1.57	2.5102	2.5102	2.0.190	2.00/0	0.0042	-
	0.00	2.0002	2.000Z	2.0002	2.0044	0.0075	1
	0.10	2.1314	2.1314	2.1314	2.7.313	0.0079	
	0.20	2.8024	2.8024	2.8024	2.1978	0.0136	
	0.30	2.8581	2.8581	2.8581	2.8581	0.0128	
	0.40	2.9069	2.9067	2.9069	2.9066	0.0131	
	0.50	2.9500	2.9500	2:9500	2.9479	0.0077	
	0.60	2.9667	2.9885	2.9887	2.9881	0.0082	
	0.70	3.0236	3.0235	3.0236	3.0153	0.0080	
99%	0.80	3.0550	3.0550	3.0554	3.0451	0.0119	
	0.90	3.0828	3:0828	3.0847	3.0799	0.0081	
	1.00	3.1067	3.1067	3.1118	3.0903	0.0102	
	1 10	3.1259	3,1259	3:1370	3.1044	0.0124	
	1.20	3.1398	3 1398	3.1604	3.1382	0.0101	
	1.30	3.1488	3.1488	3.1824	3.1477	0.0089	
	1.40	3.1536	3,1536	3,2031	3.1445	0.0102	
	1.50	3 1551	3 1549	3 2226	3,1599	0.0075	
	4.57	3 4764	0 4754	3 9355	2 4470	0.0400	

Table 5.10: Critical values for simple linear regression

#### 5.5.2 For polynomial regression of various orders

In this subsection, we compare the conservative method of Naiman (1986), the approximate method of Sun and Loader (1994), and the simulation-based method of Liu, Wynn and Hayter (2005) for an one-dimensional polynomial regression of (p-1)th order. In our comparison, we set p = 3, 4, 5 respectively corresponding to the quadratic regression, the cubic regression, and the 4th order polynomial regression.

For Naiman's method, we calculate the critical values via the following formula

$$1 - \alpha = 1 - \int_{0}^{1/c} \min\{F_{p-2,2}[2((ct)^{-2} - 1)/(p-2)] \times \Lambda(\gamma)/\pi + F_{p-1,1}[((ct)^{-2} - 1)/(p-1)], 1\}f_{T}(t)dt,$$
(5.34)

where  $f_T$  is the density function of the random variable T such that  $pT^2 \sim F_{\nu,p}$ , the F distribution with  $\nu = n - p$  and p degrees of freedom, c is a critical value, and  $\Lambda(\gamma)$  can be obtained from

$$\Lambda(\gamma) = \int_a^b \|\gamma'(\mathbf{x})\| dx,$$

where  $\gamma'(\mathbf{x})$  denotes the derivative of  $\gamma(\mathbf{x})$  with  $\mathbf{x} = (1, x, x^2, \dots, x^{p-1})$  for all  $x \in [a, b]$ . Specifically,  $\Lambda(\gamma)$  can be calculated in the following way. We have

$$\begin{split} \gamma'(\mathbf{x}) &= \left(\frac{P\mathbf{x}}{\|P\mathbf{x}\|}\right)' \\ &= \frac{(P\mathbf{x})'\|P\mathbf{x}\| - (\|P\mathbf{x}\|)'(P\mathbf{x})}{\|P\mathbf{x}\|^2} \\ &= \frac{(P\mathbf{x})'(\|P\mathbf{x}\|^2)^{1/2} - [(\|P\mathbf{x}\|^2)^{1/2}]'(P\mathbf{x})}{\|P\mathbf{x}\|^2} \\ &= \frac{(P\mathbf{x})'(\|P\mathbf{x}\|^2)^{1/2} - \frac{1}{2}(\|P\mathbf{x}\|^2)^{-1/2}(\|P\mathbf{x}\|^2)'(P\mathbf{x})}{\|P\mathbf{x}\|^2}, \end{split}$$

where  $P\mathbf{x} = (\mathbf{p}_0, \mathbf{p}_1, \dots, \mathbf{p}_{p-1})(1, x, x^2, \dots, x^{p-1})^T = \mathbf{p}_0 + \mathbf{p}_1 x + \mathbf{p}_2 x^2 + \dots + \mathbf{p}_{p-1} x^{p-1}$ ,  $\mathbf{p}_0, \dots, \mathbf{p}_{p-1}$  are the *p* columns of the matrix *P*. Note that  $||P\mathbf{x}||^2$ 

is the polynomial of order 2p-2, whose coefficients can be obtained by using commands conv and sum,  $(P\mathbf{x})'$  and  $(||P\mathbf{x}||^2)'$  are the polynomials of order p-2 and 2p-3 respectively, where their coefficients can be obtained by using command polyder. Then,  $\gamma'(\mathbf{x})$  can be found. By using command quad to implement the numerical integration, we can easily compute  $\Lambda(\gamma)$ .

For the approximate method, critical values can be calculated from

$$\alpha = \frac{\kappa_0}{\pi} (1 + \frac{c^2}{\nu})^{-\nu/2} + \mathbb{P}\{|t_\nu| > c\},$$
(5.35)

where  $\kappa_0$  is the length of the path on the surface  $S^{n-1}$  of the unit sphere. Note that  $\kappa_0 = \Lambda(\gamma)$  from (5.32).

For the simulation-based method, we obtain the critical values by following the procedure in Section 5.3.

From (5.34) and (5.35), it is clear that both Naiman's method and the approximate method depend on the length of the path, the degree of freedom and the confidence level. However, it is not clear that the simulation-based method depends on the same factors. So we use three general common factors here, i.e., the design matrix, the restricted interval for x and the preassigned confidence level.

First, we come to choose the design matrix. This can be done by choosing some design points of different locations on preassigned design intervals. Now we choose three design intervals [-1, 1], [0, 2] and [-2, 0]. For each interval, we have four structures of 8 design points. Take the case when the interval considered is [-1, 1] for example, the four structures are:

- 1.  $S_1 = [-0.2 0.16 0.13 0.06 \ 0 \ 0.07 \ 0.11 \ 0.18]$ , where the design points are distributed around the middle of the interval,
- 2.  $S_2 = [-1 0.95 0.9 0.89 \ 0.92 \ 0.95 \ 0.98 \ 1]$ , where the design points concentrate on the two ends of the interval,
- 3.  $S_3 = [0.86 \ 0.89 \ 0.91 \ 0.93 \ 0.96 \ 0.98 \ 0.99 \ 1]$ , where the design points are near the upper bound of the interval,

4.  $S_4 = [-1 -0.7 -0.4 -0.1 0.2 0.5 0.8 1.1]$ , where all the design points are equally spaced.

Such four structures of 8 design points are also adopted for the design intervals [0, 2] and [-2, 0]. So we have another 8 sets (four structures  $\times$  two design intervals) of 8 design points given by

$$S_{5} = [0.85 \ 0.88 \ 0.93 \ 0.97 \ 1 \ 1.04 \ 1.09 \ 1.12],$$

$$S_{6} = [-0.05 \ -0.02 \ 0 \ 0.03 \ 1.94 \ 1.99 \ 2 \ 2.03],$$

$$S_{7} = [-0.01 \ -0.03 \ 0 \ 0.02 \ 0.05 \ 0.06 \ 0.09 \ 0.1],$$

$$S_{8} = [0 \ 0.3 \ 0.6 \ 0.9 \ 1.2 \ 1.5 \ 1.8 \ 2.1],$$

$$S_{9} = [-1.11 \ -1.08 \ -1.01 \ -1 \ -0.99 \ -0.97 \ -0.95 \ -0.92],$$

$$S_{10} = [-2 \ -1.99 \ -1.96 \ -1.91 \ -0.08 \ -0.05 \ -0.01 \ 0.02],$$

$$S_{11} = [-0.1 \ -0.07 \ -0.02 \ 0 \ 0.03 \ 0.09 \ 0.15],$$

$$S_{12} = [-2 \ -1.7 \ -1.4 \ -1.1 \ -0.8 \ -0.5 \ -0.2 \ 0.1].$$

Therefore, 12 design matrices can be obtained so far which are marked by  $D1, \ldots, D12$ . In addition, it is motivated to choose extra 12 design matrices of 35 design points in order to make the degree of freedom be both small ( $\nu < 5$ ) and large ( $\nu > 30$ ) in our comparison. We choose these extra 12 design matrices also of the same four structures as described previously, still on the three design intervals [-1, 1], [0, 2] and [-2, 0] respectively. The 12 sets (four structures × three design intervals) of 35 design points are:

- 1.  $S_{13} = [-0.39 0.36 0.31 0.29 0.23 0.21 0.2 0.18 0.17 0.14 0.13 0.11 0.1 0.07 0.06 0.03 0.01 0 0.02 0.03 0.05 0.09 0.11 0.13 0.14 0.18 0.2 0.21 0.24 0.25 0.3 0.32 0.36 0.39 0.4],$
- 2.  $S_{14} = [-1.23 1.21 1.15 1.1 1.08 1.02 1 0.99 0.95 0.94 0.92 0.89 0.82 0.73 0.72 0.71 0.7 0.71 0.73 0.76 0.79 0.81 0.84 0.85 0.88 0.92 0.95 0.98 0.99 1.02 1.04 1.08 1.12 1.13 1.19],$
- 3.  $S_{15} = [0.71\ 0.72\ 0.74\ 0.75\ 0.77\ 0.78\ 0.81\ 0.82\ 0.85\ 0.88\ 0.9\ 0.91\ 0.93\ 0.94$

 $\begin{array}{c} 0.98 \ 1 \ 1.01 \ 1.07 \ 1.08 \ 1.09 \ 1.11 \ 1.12 \ 1.13 \ 1.16 \ 1.19 \ 1.2 \ 1.22 \ 1.25 \ 1.26 \\ 1.28 \ 1.29 \ 1.3 \ 1.31 \ 1.35 \ 1.4], \end{array}$ 

¢

- 4.  $S_{16} = [-1.36 1.28 1.2 1.12 1.04 0.96 0.88 0.8 0.72 0.64 0.56 0.48 0.4 0.32 0.24 0.16 0.08 0 0.08 0.16 0.24 0.32 0.4 0.48 0.56 0.64 0.72 0.8 0.88 0.96 1.04 1.12 1.2 1.28 1.36],$
- 5.  $S_{17} = [0.65 \ 0.69 \ 0.71 \ 0.72 \ 0.75 \ 0.76 \ 0.78 \ 0.82 \ 0.85 \ 0.88 \ 0.89 \ 0.9 \ 0.93 \ 0.95$  $0.97 \ 0.99 \ 1 \ 1.02 \ 1.04 \ 1.07 \ 1.08 \ 1.13 \ 1.15 \ 1.19 \ 1.2 \ 1.21 \ 1.23 \ 1.25 \ 1.26$  $1.28 \ 1.3 \ 1.32 \ 1.33 \ 1.35 \ 1.4],$
- 6.  $S_{18} = [-0.13 \ -0.12 \ -0.1 \ -0.09 \ -0.07 \ -0.05 \ -0.03 \ -0.01 \ 0 \ 0.03 \ 0.05 \ 0.09 \ 0.12$ 0.16 0.17 0.18 0.23 0.28 0.31 0.35 1.72 1.76 1.81 1.83 1.85 1.94 1.95 1.97 1.99 2 2.02 2.05 2.07 2.14 2.16],
- 7.  $S_{19} = [1.68 \ 1.71 \ 1.73 \ 1.76 \ 1.77 \ 1.79 \ 1.8 \ 1.82 \ 1.85 \ 1.87 \ 1.88 \ 1.91 \ 1.92 \ 1.94$ 1.95 \ 1.99 \ 2 \ 2.01 \ 2.03 \ 2.07 \ 2.12 \ 2.13 \ 2.15 \ 2.18 \ 2.19 \ 2.24 \ 2.26 \ 2.29 \ 2.31 2.33 \ 2.34 \ 2.37 \ 2.39 \ 2.4 \ 2.42],
- 8.  $S_{20}$  = [-0.36 -0.28 -0.2 -0.12 -0.04 0.04 0.12 0.2 0.28 0.36 0.44 0.52 0.6 0.68 0.76 0.84 0.92 1 1.08 1.16 1.24 1.32 1.4 1.48 1.56 1.64 1.72 1.8 1.88 1.96 2.04 2.12 2.2 2.28 2.36],
- 9.  $S_{21} = [-1.7 1.62 1.5 1.43 1.41 1.38 1.37 1.35 1.31 1.28 1.22 1.2 1.18 1.15 1.13 1.11 1.09 1.07 1.05 1.04 1.02 1.01 0.98 0.96 0.95 0.92 0.85 0.81 0.78 0.72 0.71 0.69 0.68 0.65 0.61],$
- 10.  $S_{22}$ =[-2.36 -2.31 -2.28 -2.27 -2.25 -2.2 -2.12 -2.09 -2.06 -2.01 -2 -1.99 -1.97 -1.93 -1.91 -1.86 -1.81 -0.53 -0.44 -0.42 -0.41 -0.38 -0.35 -0.33 -0.31 -0.27 -0.26 -0.24 -0.2 -0.15 -0.12 -0.11 -0.08 -0.05 0],
- 11.  $S_{23}$ =[-2.36 -2.31 -2.29 -2.28 -2.26 -2.25 -2.2 -2.18 -2.12 -2.09 -2.06 -2.01 -2 -1.99 -1.97 -1.93 -1.91 -1.86 -1.85 -1.81 -1.77 -1.75 -1.73 -1.72 -1.68 -1.66 -1.64 -1.61 -1.56 -1.53 -1.52 -1.49 -1.48 -1.45 -1.41],

12.  $S_{24} = [-2.2 \ -2.13 \ -2.06 \ -1.99 \ -1.92 \ -1.85 \ -1.78 \ -1.71 \ -1.64 \ -1.57 \ -1.5 \ -1.43 \ -1.36 \ -1.29 \ -1.22 \ -1.15 \ -1.08 \ -1.01 \ -0.94 \ -0.87 \ -0.8 \ -0.73 \ -0.66 \ -0.59 \ -0.52 \ -0.45 \ -0.38 \ -0.31 \ -0.24 \ -0.17 \ -0.1 \ -0.03 \ 0.04 \ 0.11 \ 0.18].$ 

We denote the 12 design matrices obtained from  $S_{13}, \ldots, S_{24}$  by  $D13, \ldots, D24$ . Consequently, we have totally 24 design matrices  $D1, \ldots, D24$  for our comparison.

Next, we choose the restricted intervals of x on which confidence bands are constructed. For each design interval, we choose two restricted intervals. One is the same as the design interval, the other is of smaller length. Specifically, these six restricted intervals are: [-1, 1], [-0.7, 0.7], [0, 2], [0.6, 1.4], [-2, 0] and [-1.5, -0.5]. Note that since both the design matrices and the restricted intervals are chosen according to the design intervals, in our comparison, the first two restricted intervals are used together with  $D1, \ldots, D4$ and  $D13, \ldots, D16$ , the middle two with  $D5, \ldots, D8$  and  $D17, \ldots, D20$ , and the last two with  $D9, \ldots, D12$  and  $D21, \ldots, D24$ .

Finally, 90% and 95% confidence levels are employed. The choice of such designs is to obtain as many combinations of the three factors as possible such that our comparison gives a general view.

We calculate the critical values of the confidence bands based on the three methods for polynomial regression of up to the 4th order, and record them in Tables 5.11-5.16. The columns titled  $\kappa_0$  contain the values of the length of the path.

From the results, we may draw some conclusions. When the degree of freedom is small ( $\nu < 5$ ), Naiman's method and the approximate method of Sun and Loader (1994) have almost the same critical values for  $\kappa_0 < 0.6$ ; when  $\kappa_0 > 0.6$ , the critical values of Naiman's method are generally smaller than those of the approximate method and the difference between the critical

values of these two methods follows that:

$0.6 < \kappa_0 < 1.5$	the difference is at the third decimal place,
$1.5 < \kappa_0 < 3$	the difference is at the second decimal place
$3 < \kappa_0 < 4$	the difference is around 0.15,
$4 < \kappa_0 < 5$	the difference is around 0.25,
$5 < \kappa_0 < 6$	the difference is around 0.3,
$6 < \kappa_0 < 7$	the difference is around 0.5,
$7 < \kappa_0 < 8.5$	the difference is around $0.7$ ,
$8.5 < \kappa_0 < 10$	the difference is around 0.9.

5

The critical values of the simulation-based method are even smaller than those of Naiman's method, with the difference generally at the second decimal place. When  $\nu > 30$ , the distinctions among the critical values of the three methods are not evident relative to the case when  $\nu < 5$ , generally at the second decimal place. Also, the simulation-based method obtains the smallest critical values.

Consider that for a large number of simulations, the simulation-based method seems to be able to compute as accurate critical values as the exact method. Therefore, we may conclude that Naiman's method is good enough because it is basically a conservative method but its critical values are not much conservative actually, the approximate method is not good as its critical values are even larger than those of the conservative method. However, in particular, three methods give almost the same critical values when  $\kappa_0 < 1$ .

D1         5.3026         90%         3.1396         3.4360         3.0844         0           (-1, 1)         D2         4.5157         90%         3.0947         3.3124         3.0631         0           D2         4.5157         90%         3.0947         3.3124         3.0631         0           D3         4.5376         90%         3.0947         3.3124         3.0631         0           D3         4.5376         90%         3.0961         3.3160         3.0728         0           D4         3.5219         90%         3.0991         3.1334         3.0200         0           D4         3.5219         90%         3.0913         3.1334         3.0200         0           04         3.5219         90%         3.0913         3.134         3.0200         0           04         3.5219         90%         3.0913         3.134         3.0200         0           04         3.5219         90%         3.1348         3.4215         3.1091         0           102         0.3200         90%         2.1823         2.1824         2.1754         0           (-0.7, 0.7)         03         0.1544         9	3,6.
95%         3.8404         4.1381         3.7748         0           D2         4.5157         90%         3.0947         3.3124         3.0631         0           D3         4.5376         90%         3.0947         3.3124         3.0631         0           D3         4.5376         90%         3.0961         3.3160         3.0728         0           D4         3.5219         90%         3.0991         3.1334         3.0200         0           D4         3.5219         90%         3.0991         3.1334         3.0200         0           D4         3.5219         90%         3.0991         3.1334         3.0200         0           95%         3.6863         3.8048         3.7299         0         0         3.7992         3.1334         3.0200         0           1         5.2056         90%         3.1348         3.4215         3.1991         0           1         5.2056         90%         3.1348         3.4215         3.1991         0           1         95%         3.6863         3.2048         3.7590         0         0           (-0.7, 0.7)         95%         2.7663         2.7584 <td>0.0106</td>	0.0106
D2         4.5157         90%         3.0947         3.3124         3.0631         0           (-1, 1)         95%         3.7872         4.0018         3.7639         0           D3         4.5376         90%         3.0961         3.3160         3.0728         0           95%         3.7872         4.0018         3.7639         0         0         3.0921         3.3160         3.0728         0           95%         3.7890         4.0057         3.7385         0         0         95%         3.6863         3.8046         3.7209         0           04         3.5219         90%         3.0941         3.1334         3.0200         0         3.6863         3.8046         3.7209         0           01         5.2056         90%         3.1348         3.4215         3.1091         0         95%         3.8348         4.1220         3.7943         0           02         0.3200         90%         2.1823         2.1824         2.1754         0           (-0.7, 0.7)         95%         2.6651         2.6661         2.6728         0         95%         2.6651         2.6651         2.6728         0           04	0.017.1
(-1, 1)         95%         3.7872         4.0018         3.7639         (           D3         4/5376         90%         3.0961         3.3160         3.0728         (           95%         3.7890         4.0057         3.7385         ( </td <td>0.0152</td>	0.0152
D3         4:5376         90%         3.0961         3.3160         3.0728         0           D4         3:5219         90%         3.0091         3.1334         3.0200         0           D4         3:5219         90%         3.6863         3:8048         3.7209         0           95%         3:6863         3:8048         3.7209         0         3.5219         3.6863         3:8048         3.7209         0           95%         3:6863         3:8048         3.7209         0         3.7345         3.1091         0           95%         3:6863         3:8048         3.4215         3.1091         0         5.755         3.8348         4.1220         3.7943         0           95%         3:8348         4.1220         3.7943         0         9.56%         2.7583         2.7584         2.7590         0           903         0.1544         90%         2.0990         2.0989         2.1068         0           95%         2.6651         2.6651         2.6651         2.6728         0           95%         3.4734         3.6053         3.5166         0           95%         3.4734         3.6053         3.5166 <td>1.0221</td>	1.0221
95%         3.7890         4.0057         3.7385         0           D4         3.5219         90%         3.0091         3.1334         3.0200         0           95%         3.6863         3.8048         3.7299         0           95%         3.6863         3.8048         3.7299         0           95%         3.6863         3.8048         3.7299         0           91         5.2056         90%         3.1348         3.4215         3.1991         0           95%         3.8346         4.1220         3.7943         0         3.7943         0           102         0.3200         90%         2.1823         2.1824         2.1754         0           95%         2.7683         2.7584         2.7590         0         0         0         95%         2.6651         2.6661         2.6728         0           95%         2.6651         2.6661         2.6728         0         95%         3.4734         3.6063         3.6166         0           95%         3.4734         3.6063         3.6166         0         95%         3.4734         3.6063         3.6166         0	0.0114
D4         3:5219         90%         3:0091         3:1334         3:0200         0           95%         3:6863         3:8048         3:7209         0           D1         5:2056         90%         3:1348         3:4215         3:1091         0           95%         3:8348         4.1220         3.7943         0 <td>1.0206</td>	1.0206
D1         5.2056         90%         3.6863         3.8048         3.7209         0           D1         5.2056         90%         3.1348         3.4215         3.1091         0           95%         3.8348         4.1220         3.7943         0           D2         0.3200         90%         2.1823         2.1824         2.1754         0           D3         0.1544         90%         2.0990         2.0989         2.1068         0           D4         2.2914         90%         2.6651         2.6661         2.6728         0           D4         2.2914         90%         3.4734         3.6053         3.5166         0           95%         3.4734         3.6053         3.5166         0         0         95%         3.4734         3.6053         3.5166         0	1.0119
D1         5.2056         90%         3.1348         3.4215         3.1091         0           95%         3.8348         4.1220         3.7943         0           D2         0.3200         90%         2.1823         2.1824         2.1754         0           D3         0.1544         90%         2.0990         2.0989         2.1068         0           D4         2.2914         90%         2.6651         2.66651         2.6728         0           D4         2.2914         90%         3.4734         3.6053         3.5166         0           D5         5.3104         90%         3.1430         3.4734         3.6053         3.5166         0	1.0176
95%         3.8348         4.1220         3.7943         0           D2         0.3200         90%         2.1823         2.1824         2.1754         0           55%         2.7683         2.7584         2.7590         0         0         0           D3         0.1544         90%         2.0990         2.0989         2.1068         0           95%         2.6651         2.6661         2.6728         0         0         3.8246         2.6728         0           D4         2.2914         90%         2.8244         2.8606         2.8286         0         3.5166         0           D5         5.3104         90%         3.1400         3.4372         3.1064         0	0.0141
D2         0.3200         90%         2.1823         2.1824         2.1754         0           (-0.7, 0.7)         95%         2.7683         2.7584         2.7590         0           D3         0.1544         90%         2.0990         2.0969         2.1068         0           95%         2.6651         2.6651         2.6651         2.6728         0           D4         2.2914         90%         2.8244         2.6605         2.62866         0           95%         3.4734         3.6053         3.5166         0           D5         5.3104         90%         3.1400         3.4372         3.1004         0	0.0185
(-0.7, 0.7)         95%         2.7583         2.7584         2.7590         0           D3         0.1544         90%         2.0990         2.0989         2.1068         0           95%         2.6651         2.6661         2.6728         0         0         0           D4         2.2914         90%         2.8244         2.8606         2.8286         0           95%         3.4734         3.6053         3.6166         0           D5         5.3104         90%         3.1400         3.4372         3.1064         0	0.0119
D3         0.1544         90%         2.0990         2.0989         2.1068         0           95%         2.6651         2.6651         2.6651         2.6728         0           D4         2.2914         90%         2.8244         2.8606         2.8286         0           95%         3.4734         3.6053         3.5166         0           D5         5.3104         90%         3.1400         3.4372         3.1004         0	0.0173
95%         2.6651         2.6651         2.6728         0           D4         2.2914         90%         2.8244         2.8606         2.8286         0           95%         3.4734         3.6053         3.5166         0           D5         5.3104         90%         3.1400         3.4372         3.1004         0	0.0095
D4         2.2914         90%         2.8244         2.8606         2.8286         0           95%         3.4734         3.6053         3.5166         0           D5         5.3104         90%         3.1400         3.4372         3.1004         0	0.0192
95% 3.4734 3.6053 3.6166 0 D5 5.3104 90% 3.1400 3.4372 3.1004 0	0.0116
D5 5.3104 90% 3.1400 3.4372 3.1004 (	0.0200
	0.0115
95% 3.8408 4.1394 3.7724 (	0.0195
D6 3.0409 90% 2.9499 3.0349 2.9222 0	0.0128
(0, 2) 95% 3,6176 3,6966 3,6108 (	0.0186
D7 3.5613 90% 3.0132 3.1411 2.9373 (	0115
95% 3 6912 3 8133 3 6221 0	0188
D8 35219 90% 3.0091 3.1334 3.0330 0	0135
95% 3,6863 3,8048 3,7318	0183
05 5.0487 90% 3.1267 3.3977 3.0955 0	0134
95% 3.8251 4.0957 3.7755 0	0191
D6 0.0637 90% 2.0504 2.0504 2.0562 0	0113
(0.6.1.4) 95% 2.6105 2.6106 2.5969 0	0167
D7 0.0373 90% 2.0359 2.0359 2.0523 0	0114
95% 2 5943 2 5942 2 5970 0	10144
D8 0.9811 90% 2.4608 2.4619 2.5057 0	0113
95% 3.0668 3.0677 3.1145	0143
D9 5.3279 90% 3.1408 3.4398 3.0870 0	1.0123
95% 3.8418 4.1422 3.7878 0	0182
D10 4 1462 90% 3 0676 3 2492 3 0676 0	0135
(-2 0) 95% 3 7549 3 9321 3 7248 0	0181
D11 2.5200 90% 3.0811 3.1579 3.0077 0	0145
95% 38793 3.9553 3.7830 0	0245
D12 3 5219 90% 3 0091 3 1334 3 0230 0	0142
95% 3,6863 3,8048 3,6984 0	0225
D9 5 2084 90% 3 1350 3 4219 3 0795 0	0128
95% 38350 4 1225 3 7704	0183
D10 0.1205 90% 2.0811 2.0811 2.0536 0	0105
15 0 51 95% 2 6451 2 6451 2 6568 0	0197
D11 0.0982 90% 2.1914 2.1914 2.1994 0	0123
95% 28160 28160 28239 0	10184
012 13623 90% 25893 25944 26163 0	0125
95% 3 2094 3 2134 3 2979 0	0181

d.f. = 5

٤

.

Table 5.11: Critical values for quadratic regression

D1         7.4228         90%         3.6452         4.1263         3.5498         0.0156           (-1, 1)         D2         6.0073         90%         3.5609         3.9054         3.4359         0.0349           D2         6.0073         90%         3.5609         3.9964         3.4800         0.0157           D3         6.5732         90%         3.5922         3.9976         3.1112         0.0153           D4         4.9461         90%         3.4405         4.5052         4.3415         0.0244           D1         7.3262         90%         3.6403         4.1128         3.6432         0.0156           D2         1.2913         90%         2.7504         2.757         2.7376         0.0137           D3         0.1528         90%         2.6833         2.6832         2.8176         0.0166           D4         2.7636         90%         3.6565         3.2176         0.0161         95%         3.4997         0.0324           (0.7)         D5         7.6387         90%         3.2655         3.2176         0.0166           D4         2.7636         90%         3.552         3.5555         3.217         0.0151 <th>RI</th> <th>DM</th> <th>k0</th> <th>cl</th> <th>cv nai</th> <th>cv app</th> <th>cv simu</th> <th>s.e.</th>	RI	DM	k0	cl	cv nai	cv app	cv simu	s.e.
(-1, 1)         95%         4.5609         5.0633         4.4359         0.0349           (-1, 1)         95%         4.442         4.8134         4.822         0.0271           D3         6.5732         90%         3.5962         3.9976         3.1112         0.0157           D3         6.5732         90%         3.6982         3.9976         3.1112         0.0153           04         4.9461         90%         3.4728         3.7157         3.4598         0.0173           07         1.2913         90%         2.7504         2.7557         2.7376         0.0135           02         1.2913         90%         2.7564         2.7557         2.7376         0.0137           102         1.2913         90%         2.7564         2.7557         2.7376         0.0136           102         1.2913         90%         2.2233         2.2234         2.2217         0.0118           95%         3.4909         3.4955         3.4896         0.0206         0.0264           104         2.7536         90%         3.6565         4.1680         0.3457         0.0214           105         7.6387         90%         3.4593         3.7090 <td>En la la</td> <td>D1</td> <td>7.4228</td> <td>90%</td> <td>3.6452</td> <td>4.1269</td> <td>3.5498</td> <td>0.0158</td>	En la la	D1	7.4228	90%	3.6452	4.1269	3.5498	0.0158
(-1, 1)         D2         6.0073         90%         3.5609         3.9054         3.4880         0.0157           D3         6.5732         90%         3.5982         3.9976         3.1112         0.0163           D4         4.9461         90%         3.4728         3.7157         3.4598         0.0289           D4         4.9461         90%         3.4493         4.1126         3.6452         0.0163           D1         7.3262         90%         3.6403         4.1126         3.6452         0.0173           D1         7.3262         90%         3.6403         4.1126         3.6452         0.0164           D1         7.3262         90%         2.7504         2.757         2.7376         0.0137           D2         1.2913         90%         2.6833         2.6832         2.6176         0.0166           D4         2.7636         90%         3.6655         4.1680         3.3495         0.026           D4         2.7637         90%         3.6655         4.1680         3.3457         0.0165           95%         4.2634         4.111         4.0321         0.0224         0.0234           D5         7.6387         <			and the second sec	95%	4.5509	5.0693	4:4359	0.0349
(-1, 1)         03         6.5732         95%         4.4482         4.6138         4.3232         0.0271           03         6.5732         90%         3.5982         3.9976         3.1112         0.0163           04         4.961         90%         3.4728         3.7157         3.4698         0.0173           04         4.961         90%         3.6403         4.1128         3.6432         0.0166           01         7.3262         90%         3.6403         4.1128         3.6432         0.0166           01         7.3262         90%         2.7504         2.7557         2.7376         0.0137           02         1.2913         90%         2.233         2.2234         2.2277         0.0116           04         2.7536         90%         3.6555         4.1680         3.3457         0.0150           05         7.6387         90%         3.6555         4.1560         3.3457         0.0164           0.6         4.1500         90%         3.4555         4.1663         0.0304           0.6         4.1500         90%         3.4555         4.1361         0.0224           0.6         4.1500         90%         3		D2	6.0073	90%	3.5609	3.9054	3.4880	0.0157
D3         6.5732         90%         3.5982         3.9976         3.1112         0.0163           D4         4.9461         90%         3.4728         3.7157         3.4598         0.01289           D4         4.9461         90%         3.6403         4.1128         3.6432         0.0163           D1         7.3262         90%         3.6403         4.1128         3.6432         0.0156           D2         1.2913         90%         2.7504         2.7577         2.7376         0.0137           D4         2.7536         90%         2.6833         2.0832         2.8176         0.0166           D4         2.7536         90%         3.6555         4.1680         3.3435         0.0166           D4         2.7536         90%         3.6555         4.1663         0.0345         0.0164           95%         3.9697         4.0322         3.9239         0.0228         0.0228           06         4.1500         90%         3.6555         4.1663         0.0344           07         4.9113         90%         3.4555         3.2117         0.0164           95%         4.2661         4.1663         0.0204         0.0224	(-1, 1)			95%	4.4482	4.8138	4.3232	0.0271
04         95%         4,4936         4,5202         3,9330         0,0289           04         4,9461         90%         3,4728         3,7157         3,4558         0,0244           95%         4,3415         4,5952         4,3415         0,0244           95%         4,5450         5,0529         4,4449         0,0283           02         1,2913         90%         2,7504         2,7577         2,7376         0,0137           95%         3,4909         3,4955         3,4896         0,0206         0,0137           03         0,1528         90%         2,2233         2,2234         2,2277         0,0118           95%         2,8633         2,8632         2,8176         0,0365         0,026         0,026           04         2,7536         90%         3,6555         4,1630         3,3457         0,0161           95%         3,9697         4,0322         3,9233         0,0224         0,024           06         4,1500         90%         3,6555         4,1630         3,3457         0,0161           95%         4,2614         4,111         4,0381         0,0224         4,244         0,0234           07		D3	6.5732	.90%	3.5982	3,9978	3.1112	0.0153
D4         4.9461         90%         3.4728         3.7157         3.4598         0.0173           95%         4.3415         4.5952         4.3415         0.0244           D1         7.3262         90%         3.6403         4.1128         3.6432         0.0156           D2         1.2913         90%         2.7504         2.7557         2.7376         0.0137           D3         0.1528         90%         2.2233         2.2234         2.2277         0.0166           D4         2.7536         90%         3.1614         3.2243         3.0355         0.0160           D4         2.7536         90%         3.6555         4.1560         3.3457         0.0161           D4         2.7536         90%         3.3652         3.2655         3.2117         0.0165           D5         7.6387         90%         3.3652         3.5555         3.2117         0.0164           D6         4.1500         90%         3.375         4.5636         6.1052         4.1663         0.0204           D7         4.9113         90%         3.4728         3.7157         3.3164         0.0214           (0.2)         D7         4.9461         <			a contract of the second	95%	4,4936	4.9202	3,9330	0.0289
(-0.7, 0.7)         01         7.3262         90%         3.6403         4.1128         3.5432         0.0156           D2         1.2913         90%         2.7504         2.7557         2.7376         0.0137           D3         0.1528         90%         2.2233         2.2234         2.2277         0.0118           D4         2.7636         90%         2.2833         2.2834         2.2277         0.0118           D4         2.7636         90%         3.6697         4.0322         3.9233         0.0228           D4         2.7636         90%         3.6555         4.1560         3.3457         0.0146           0.5         7.6387         90%         3.6555         3.2117         0.01451           95%         4.5636         6.1052         4.1663         0.0204           06         4.1500         90%         3.6555         3.2117         0.01451           95%         4.2361         4.4111         4.0381         0.0204           07         4.9113         90%         3.4693         3.7090         3.2998         0.0154           0.6.114)         D6         7.6255         90%         3.6452         4.1273         3.3499 </td <td>E E</td> <td>D4</td> <td>4.9461</td> <td>90%</td> <td>3.4728</td> <td>3.7157</td> <td>3,4598</td> <td>0.0173</td>	E E	D4	4.9461	90%	3.4728	3.7157	3,4598	0.0173
D1         7.3262         90%         3.6403         4.1126         3.6432         0.0156           (-0.7, 0.7)         1.2913         90%         2.7504         2.7557         2.7376         0.0137           0.1528         90%         2.2233         2.2234         2.2277         0.0118           0.4         2.7656         90%         2.2833         2.8832         2.8176         0.0166           0.4         2.7636         90%         3.6655         4.1580         3.0495         3.0335         0.0160           0.4         2.7636         90%         3.6655         4.1580         3.3457         0.0161           0.5         7.6387         90%         3.6655         4.1580         3.3457         0.0164           0.5         7.6387         90%         3.6655         4.1580         3.3457         0.0164           0.5         7.6387         90%         3.6655         3.2117         0.0165         0.0264           0.6         4.1500         90%         3.4693         3.7090         3.2998         0.0154           0.55%         4.3375         4.5875         4.128         0.0251         0.0251           0.6         0.7692         <			1	95%	4.3415	4:5952	4.3415	0.0244
(-0.7, 0.7)         D2         1.2913         90%         2.7504         2.7574         2.7376         0.0137           (-0.7, 0.7)         0.1528         90%         2.7604         2.7557         2.7376         0.0137           0.1528         90%         2.2233         2.2234         2.2277         0.0118           0.4         2.7636         90%         3.1614         3.2249         3.0935         0.0150           0.4         2.7636         90%         3.6565         4.1500         3.923         0.0226           0.5         7.6387         90%         3.6565         4.1500         3.9457         0.0161           0.6         4.1500         90%         3.3652         3.5556         3.2117         0.0165           0.7         4.9113         90%         3.4693         3.7090         3.2998         0.0144           0.7         4.9113         90%         3.4632         4.172         0.0234           0.8         4.9461         90%         3.6452         4.1273         3.3499         0.0144           0.7         7.4255         90%         2.6377         2.5365         2.5121         0.0152           0.6         0.7692 <t< td=""><td></td><td>D1</td><td>7.3262</td><td>90%</td><td>3.6403</td><td>4.1128</td><td>3.5432</td><td>0.0156</td></t<>		D1	7.3262	90%	3.6403	4.1128	3.5432	0.0156
D2         1.2913         90%         2.7504         2.7557         2.7376         0.0137           (-0.7, 0.7)         D3         0.1528         90%         2.2233         2.2234         2.2274         0.0166           D4         2.7536         90%         3.1614         3.2249         3.0355         0.0166           D4         2.7636         90%         3.6565         4.1580         3.3457         0.0161           95%         3.9697         4.0322         3.9233         0.0228           D5         7.6387         90%         3.6565         4.1580         3.3457         0.0161           95%         4.5636         6.1052         4.1663         0.0204           D6         4.1500         90%         3.3652         3.2117         0.0165           95%         4.2361         4.4111         4.0381         0.0204           D7         4.9113         90%         3.4693         3.7090         3.2998         0.0154           98         4.9461         90%         3.4728         3.7157         3.3499         0.0144           95%         4.5511         5.0697         4.2144         0.0251           0.6         0.7692				95%	4,5450	5.0529	4.4449	0:0283
(-0.7, 0.7)         95%         3.4909         3.4955         3.4896         0.0206           D3         0.1528         90%         2.2233         2.2234         2.2277         0.0118           D4         2.7636         90%         3.1614         3.2249         3.0935         0.0160           D4         2.7636         90%         3.6555         4.1580         3.3457         0.0151           0.6         4.1500         90%         3.6555         4.1580         3.3457         0.0164           0.6         4.1500         90%         3.6555         3.2117         0.0165           0.6         4.1500         90%         3.4693         3.7090         3.2998         0.0154           0.7         4.9113         90%         3.4728         3.7157         3.3149         0.0234           0.8         4.9461         90%         3.4728         3.7157         3.3149         0.0134           95%         4.3415         4.5052         4.1723         0.3249         0.0144           0.6         0.7692         90%         2.5377         2.5366         2.5121         0.0152           (0.6, 1.4)         D6         0.7692         90%         2.6	Ī	D2	1.2913	90%	2.7504	2.7557	2.7376	0.0137
D3         0.1528         90%         2.2233         2.2234         2.2277         0.0118           D4         2.7636         90%         3.1614         3.2493         3.0935         0.0166           D4         2.7636         90%         3.1614         3.2249         3.0935         0.0166           D5         7.6387         90%         3.6555         4.1560         3.3457         0.0161           0.6         4.1500         90%         3.3852         3.6555         3.2117         0.0165           95%         4.2361         4.4111         4.0381         0.0234         0.0234           0.6         4.1500         90%         3.4693         3.7090         3.2998         0.0154           0.7         4.9113         90%         3.4693         3.7090         3.2984         0.0234           0.8         4.9461         90%         3.4728         3.7157         3.3164         0.0234           0.8         7.4255         90%         3.6452         4.1273         3.3499         0.0144           0.6         0.7692         90%         2.5377         3.22467         3.2211         0.0259           0.7         0.0367         90%	1-0.7. 0.71			95%	3,4909	3,4955	3,4896	0.0206
Image: constraint of the system of		D3	0.1528	90%	2.2233	2.2234	2.2277	0.0118
D4         2.7536         90%         3.1614         3.2249         3.0935         0.0150           05         7.6387         90%         3.6555         4.1580         3.3457         0.0151           95%         4.5636         6.1052         4.1663         0.0304           06         4.1500         90%         3.3852         3.5555         3.2117         0.0155           07         4.9113         90%         3.4693         3.7090         3.2998         0.0154           08         4.9461         90%         3.4728         3.7157         3.3164         0.0234           08         4.9461         90%         3.44728         3.7157         3.3164         0.0251           95%         4.3375         4.5875         4.1284         0.0251           95%         3.6452         4.1273         3.3499         0.0144           0.253         95%         3.2461         3.2467         3.2211         0.0253           0.6         0.7692         90%         2.5377         2.5365         2.5121         0.0152           0.6         0.7692         90%         2.1545         2.1529         0.0117           95%         3.6367	1121220			95%	2.8833	2.8832	2.8176	0.0166
(0.2)         D5         7:6387         90%         3.6555         4.1580         3.3457         0.0151           (0.2)         D6         4.1500         90%         3.3655         4.1580         3.3457         0.0151           (0.2)         D6         4.1500         90%         3.3852         3.5555         3.2117         0.0155           (0.2)         D7         4.9113         90%         3.4693         3.7090         3.2998         0.0124           D8         4.9461         90%         3.4728         3.7157         3.3164         0.0132           D8         4.9461         90%         3.6452         4.1273         3.3499         0.0144           D5         7.4255         90%         3.6452         4.1273         3.3499         0.0144           0.12         95%         4.5511         5.0697         4.2144         0.0253           D6         0.7692         90%         2.5377         2.5365         2.5121         0.0152           0.14         95%         3.2461         3.2467         3.2211         0.0254           D7         0.0367         90%         2.1545         2.1529         0.0117           95% <t< td=""><td></td><td>D4</td><td>2,7636</td><td>90%</td><td>3 1614</td><td>3 2249</td><td>3.0935</td><td>0.0150</td></t<>		D4	2,7636	90%	3 1614	3 2249	3.0935	0.0150
(0.2)         D5         7:6387         90%         3:6555         4.1580         3:3457         0.0151           (0.2)         D6         4.1500         90%         3:3852         3:5555         3:2117         0.0165           (0.2)         D7         4.9113         90%         3:3852         3:5555         3:2117         0.0165           (0.2)         D7         4.9113         90%         3:4693         3:7090         3:2998         0.0154           (0.4)         D7         4.9461         90%         3:4728         3:7157         3:3164         0.0234           D8         4.9461         90%         3:6452         4.1273         3:3499         0.0144           95%         4:5511         5.0697         4:2144         0.0253           D6         0.7692         90%         2:5377         2:5365         2:5121         0.0152           D7         0.0367         90%         2:4613         3:2467         3:2241         0.0209           D7         0.0367         90%         2:6565         2:8898         2:7966         0.0113           95%         3:6367         3:6488         3:6497         0.0219           D8				95%	3.9697	4.0322	3 9233	0.0228
(0.2)         06         4.1500         90%         3.3852         3.6555         3.2117         0.0155           90%         4.2361         4.4111         4.0381         0.0204           D7         4.9113         90%         3.4693         3.7090         3.2998         0.0154           D8         4.9461         90%         3.4728         3.7157         3.3164         0.0132           D8         4.9461         90%         3.6452         4.1273         3.3499         0.0144           D5         7.4255         90%         3.6452         4.1273         3.3499         0.0142           95%         4.3511         5.0697         4.2144         0.0253         0.0152           0.6         0.7692         90%         2.5377         2.5365         2.5121         0.0152           0.7         0.0367         90%         2.1645         2.1645         2.1529         0.0117           95%         2.8028         2.8028         2.6375         0.0233         0.0199           07         0.0367         90%         3.6597         4.1702         3.2333         0.0133           98         1.6600         90%         3.6597         4.1702		D5	7:6387	90%	3.6555	4,1580	3.3457	0.0151
(0. 2)         D6         4.1500         90%         3.3852         3.5555         3.2117         0.0155           (0. 2)         D7         4.9113         90%         3.4693         3.7090         3.2998         0.0154           D7         4.9113         90%         3.4728         3.7157         3.3164         0.0234           D6         4.9461         90%         3.4728         3.7157         3.3164         0.0132           95         4.3415         4.5952         4.1728         0.0251         0.0251           95         7.4255         90%         3.6452         4.1273         3.3499         0.0144           95         4.5611         5.0697         4.2144         0.0253           0.6         0.7692         90%         2.5377         2.5365         2.5121         0.0152           0.7         0.0367         90%         2.1545         2.1529         0.0117           95%         2.8028         2.8028         2.6375         0.0233           0.8         1.6600         90%         3.6597         4.1702         3.2333         0.0133           95%         4.5686         5.1192         4.0554         0.0255         0.0249 <td>1000</td> <td></td> <td>1.1.1</td> <td>95%</td> <td>4.5636</td> <td>5 1052</td> <td>4 1663</td> <td>0.0304</td>	1000		1.1.1	95%	4.5636	5 1052	4 1663	0.0304
(0, 2)         95%         4.2361         4.4111         4.0381         0.0204           D7         4.9113         90%         3.4693         3.7090         3.2998         0.0154           95%         4.3375         4.5875         4.1284         0.0234           D6         4.9461         90%         3.4726         3.7167         3.3164         0.0132           95%         4.3415         4.5952         4.1728         0.0251           D5         7.4255         90%         3.6452         4.1273         3.3499         0.0144           95%         4.5611         5.0697         4.2144         0.0253           D6         0.7692         90%         2.5377         2.5365         2.5121         0.0152           0.7         0.0367         90%         2.1545         2.1529         0.0117           95%         3.6367         3.6488         3.6487         0.0254           D8         1.6600         90%         2.8766         2.8198         2.7966         0.0139           95%         4.5696         5.1192         4.0554         0.0255         0.0139           910         5.6165         90%         3.5315         3.8384	-	D6	4 1500	90%	3 3852	3 6555	3,2117	0.0155
D7         4.9113         90%         3.4693         3.7090         3.2998         0.0154           D6         4.9461         90%         3.4728         3.7157         3.3164         0.0234           D6         4.9461         90%         3.4728         3.7157         3.3164         0.0132           95%         4.3415         4.5952         4.1728         0.0251           D5         7.4255         90%         3.6452         4.1273         3.3499         0.0144           0.6         0.7692         90%         2.5377         2.5366         2.5121         0.0152           D6         0.7692         90%         2.1545         2.1529         0.0117           95%         3.2461         3.2467         3.2211         0.0209           D7         0.0367         90%         2.1545         2.1529         0.0117           95%         2.8028         2.8375         0.0234         0.0219           D8         1.6600         90%         2.8765         2.8898         2.7966         0.0113           99         7.7237         90%         3.6367         4.1702         3.2333         0.0139           910         5.6165         <	(0 2)			95%	4 2361	4 4111	4 0381	0.0204
Image: space	(0. ~/	D7	4 9113	90%	3 4693	3 7090	3 2998	0 0154
D6         4.9461         90%         3.4726         3.7157         3.3164         0.0132           95%         4.3415         4.5952         4.1728         0.0251           95%         4.3415         4.5952         4.1728         0.0251           95%         4.3415         4.5952         4.1728         0.0251           95%         4.5511         5.0697         4.2144         0.0253           96         0.7692         90%         2.5377         2.5365         2.5121         0.0109           97         0.0367         90%         2.1545         2.1529         0.0117           95%         2.8028         2.8028         2.6375         0.0234           98         1.6600         90%         2.8765         2.8898         2.7966         0.0113           95%         3.6367         3.6488         3.5487         0.0259           99         7.7237         90%         3.6597         4.1702         3.2333         0.0139           95%         4.5665         5.1192         4.0564         0.0259         0.0153           910         5.6165         90%         3.5315         3.8384         3.3497         0.0156			1.0,1.0	95%	4 3375	4 5875	4 1284	0 0234
Dis         95%         4.3415         4.5952         4.1728         0.0251           Dis         7.4255         90%         3.6452         4.1273         3.3499         0.0144           95%         4.5511         5.0697         4.2144         0.0253           Dis         7.4255         90%         2.5377         2.5365         2.5121         0.0152           Dis         0.0367         90%         2.1545         2.1545         2.1529         0.0214           Dis         1.6600         90%         2.8765         2.8028         2.8028         2.6375         0.0234           Dis         1.6600         90%         2.8765         2.8088         2.7966         0.0113           Dis         1.6600         90%         3.6597         4.1702         3.2333         0.0139           95%         3.6567         3.6488         3.5487         0.0255           Dis         5.6165         90%         3.5315         3.8384         3.3497         0.0153           95%         4.4125         4.7363         4.1687         0.0259           Dis         5.6165         90%         3.7321         3.9436         3.5419         0.0145 <tr< td=""><td>1</td><td>DB</td><td>4 9461</td><td>90%</td><td>3 4728</td><td>3 7157</td><td>3 3164</td><td>0.0132</td></tr<>	1	DB	4 9461	90%	3 4728	3 7157	3 3164	0.0132
D5         7.4255         90%         3.6452         4.1273         3.3499         0.0144           0.6, 1.4)         D6         0.7692         90%         2.5377         2.5365         2.5121         0.0152           D6         0.7692         90%         2.5377         2.5365         2.5121         0.0152           D7         0.0367         90%         2.1645         2.1645         2.1529         0.0117		20		95%	4 3415	4 5952	4 1728	0.0251
Image: constraint of the system of		05	7 4255	90%	3 6452	4 1273	3 3499	0.0144
D6         0.7692         90%         2.5377         2.5385         2.5121         0.0152           (0.6, 1.4)         D7         0.0367         90%         2.1545         2.1545         2.1529         0.0117           D7         0.0367         90%         2.1545         2.1545         2.1529         0.0117           D8         1.6600         90%         2.8765         2.8028         2.6375         0.0234           D8         1.6600         90%         2.8765         2.8488         2.7966         0.0113           95%         3.6367         3.6488         3.6487         0.0219           9         7.7237         90%         3.6597         4.1702         3.2333         0.0139           9         7.7237         90%         3.5315         3.8384         3.3497         0.0153           9         7.7237         90%         3.5315         3.8384         3.3497         0.0153           1010         5.6165         90%         3.7321         3.9436         3.5419         0.0176           95%         4.4125         4.7363         4.1687         0.0259         0.460         0.1453           911         3.4267         90%	1000			95%	4 5511	5 0697	4 2144	0.0253
(0.6, 1.4)         0         95%         3.2461         3.2467         3.2411         0.0209           D7         0.0367         90%         2.1545         2.1529         0.0117           95%         2.8028         2.8028         2.6375         0.0234           D8         1.6600         90%         2.8765         2.8898         2.7966         0.0113           95%         3.6367         3.6487         0.0219         95%         3.6597         4.1702         3.2333         0.0139           95%         3.6587         4.1702         3.2333         0.0139         95%         4.5686         5.1192         4.0554         0.0259           D10         5.6165         90%         3.5315         3.8384         3.3497         0.0153           95%         4.4125         4.7363         4.1687         0.0259           D11         3.4267         90%         3.7321         3.9436         3.5419         0.0176           95%         4.3415         4.5952         4.2536         0.0243           D12         4.9461         90%         3.4728         3.7157         3.2417         0.0157           99         7.6347         90%         3.6653		D6	0 7692	90%	2 5377	2 5385	2 5121	0.0152
D7         0.0367         90%         2.1545         2.1545         2.1529         0.0117           D8         1.6600         90%         2.8765         2.8028         2.8375         0.0234           D8         1.6600         90%         2.8765         2.8088         2.7966         0.0117           95%         3.6367         3.6488         3.5487         0.0219           99         7.7237         90%         3.6597         4.1702         3.2333         0.0139           910         5.6165         90%         3.5515         3.8384         3.3497         0.0153           910         5.6165         90%         3.7321         3.9436         3.5419         0.0259           911         3.4267         90%         3.7321         3.9436         3.5419         0.0176           95%         4.8915         5.1318         4.6957         0.0460         0.124         95%         4.3415         4.5952         4.2536         0.0243           99         7.6347         90%         3.6653         4.1575         3.2417         0.0157           910         0.9690         90%         2.6242         2.6259         2.6024         0.0141	(0.6 1.4)			95%	3 2461	3 2467	3 2211	0.0209
Diamon         95%         2.8026         2.8028         2.8033         2.8033         0.8019         0.8019         0.8019         0.8019         0.8019         0.8019         0.8019         0.8019         0.8019         0.8019         0.8019         0.8019         0.8014         0.8019         0.8014         0.8019 <td>44.44, 10.17</td> <td>D7</td> <td>0.0367</td> <td>90%</td> <td>2 1545</td> <td>2 1545</td> <td>2 1529</td> <td>0.0117</td>	44.44, 10.17	D7	0.0367	90%	2 1545	2 1545	2 1529	0.0117
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$				95%	2 8028	2 8028	2 8375	0 0234
$(-2, 0) \begin{array}{ c c c c c c c c c c c c c c c c c c c$		<b>D8</b>	1.6600	90%	2 8765	2 8898	2 7966	0.0113
$(-2, 0) \begin{array}{ c c c c c c c c c c c c c c c c c c c$				95%	3 6367	3 6488	3.5487	0.0219
$(-2, 0) \begin{array}{ c c c c c c c c c c c c c c c c c c c$		09	7 7237	90%	3.6597	4 1702	3.2333	0.0139
$(-2, 0) \begin{array}{ c c c c c c c c c c c c c c c c c c c$				95%	4 5586	5 1192	4 0554	0 0255
(-2, 0)         95%         4.4125         4.7363         4.1687         0.0259           D11         3.4267         90%         3.7321         3.9436         3.5419         0.0176           95%         4.8915         5.1318         4.6957         0.0460           D12         4.9461         90%         3.4728         3.7157         3.4284         0.0145           95%         4.3415         4.5952         4.2536         0.0243           99         7.6347         90%         3.6553         4.1575         3.2417         0.0157           95%         4.5634         5.1046         4.0763         0.0254           010         0.9690         90%         2.6242         2.6259         2.6024         0.0119           (-1.5, -0.5)         95%         3.3455         3.3470         3.3339         0.0203           D11         0.0788         90%         2.4100         2.4101         2.4075         0.0144           95%         3.2526         3.2787         0.0247         0.0137           D12         1.9716         90%         2.9700         2.9933         2.6802         0.0137           95%         3.7452         3.7671 <t< td=""><td>171.19</td><td>D10</td><td>5 6165</td><td>90%</td><td>3 5315</td><td>3 8384</td><td>3 3497</td><td>0.0153</td></t<>	171.19	D10	5 6165	90%	3 5315	3 8384	3 3497	0.0153
D11         3.4267         90%         3.7321         3.9436         3.5419         0.0176           D12         4.9461         90%         3.4728         3.7157         3.4284         0.0145           D12         4.9461         90%         3.4728         3.7157         3.4284         0.0145           95%         4.3415         4.5952         4.2536         0.0243           D9         7.6347         90%         3.6553         4.1575         3.2417         0.0157           95%         4.5634         5.1046         4.0763         0.0254           D10         0.9690         90%         2.6242         2.6259         2.6024         0.0119           95%         3.3456         3.3470         3.3339         0.0203           D11         0.0788         90%         2.4100         2.4075         0.0144           95%         3.2526         3.2787         0.0247         0.0247           D12         1.9716         90%         2.9700         2.9933         2.6802         0.0137           95%         3.7452         3.7671         3.6658         0.0232	(-2 0)			95%	4 4125	4 7363	4 1687	0.0259
95%         4.8915         5.1318         4.6957         0.0460           D12         4.9461         90%         3.4728         3.7157         3.4284         0.0145           95%         4.3415         4.5952         4.2536         0.0243           95%         4.3415         4.5952         4.2536         0.0243           99         7.6347         90%         3.6553         4.1575         3.2417         0.0157           95%         4.5634         5.1046         4.0763         0.0254           D10         0.9690         90%         2.6242         2.6259         2.6024         0.0119           95%         3.3455         3.3470         3.3339         0.0203           D11         0.0788         90%         2.4100         2.4075         0.0144           95%         3.2526         3.2787         0.0247           D12         1.9716         90%         2.9700         2.9933         2.6802         0.0137           95%         3.7452         3.7671         3.6658         0.0232	(-, -,	D11	3.4267	90%	3.7321	3 9436	3 5419	0 0176
D12         4.9461         90%         3.4728         3.7157         3.4284         0.0145           95%         4.3415         4.5952         4.2536         0.0243           D9         7.6347         90%         3.6553         4.1575         3.2417         0.0157           95%         4.5634         5.1046         4.0763         0.0254           D10         0.9690         90%         2.6242         2.6259         2.6024         0.0119           95%         3.3455         3.3470         3.3339         0.02043           D11         0.0788         90%         2.4100         2.4075         0.0144           95%         3.2526         3.2787         0.0247           D12         1.9716         90%         2.9700         2.9933         2.6802         0.0137           95%         3.7452         3.7671         3.6658         0.0232				95%	4 8915	5 1318	4 6957	0.0460
D9         7.6347         90%         3.6553         4.1575         3.2417         0.0157           95%         4.3415         4.5952         4.2536         0.0243         0.0157           99         7.6347         90%         3.6553         4.1575         3.2417         0.0157           95%         4.5634         5.1046         4.0763         0.0254           0.10         0.9690         90%         2.6242         2.6259         2.6024         0.0119           95%         3.3455         3.3470         3.3339         0.02034           0.11         0.0788         90%         2.4100         2.4075         0.0144           95%         3.2526         3.2526         3.2787         0.0247           0.12         1.9716         90%         2.9700         2.9933         2.6802         0.0137           95%         3.7452         3.7671         3.6658         0.0232		D12	4 9461	90%	3 4728	3 7157	3 4284	0.0145
D9         7.6347         90%         3.6553         4.1575         3.2417         0.0157           95%         4.5634         5.1046         4.0763         0.0254           0.15         95%         3.26242         2.6259         2.6024         0.0119           95%         3.3455         3.3470         3.3339         0.0203           011         0.0788         90%         2.4100         2.4101         2.4075         0.0144           95%         3.2526         3.2526         3.2787         0.0247           012         1.9716         90%         2.9700         2.9933         2.6802         0.0137           95%         3.7452         3.7671         3.6658         0.0232         0.0232				95%	4 3415	4 5952	4 2536	0 0243
95%         4.5634         5.1046         4.0763         0.0254           0.10         0.9690         90%         2.6242         2.6259         2.6024         0.0119           (-1.5, -0.5)         95%         3.3455         3.3470         3.3339         0.0203           D11         0.0768         90%         2.4100         2.4101         2.4075         0.0144           95%         3.2526         3.2526         3.2787         0.0247           D12         1.9716         90%         2.9700         2.9933         2.6802         0.0137           95%         3.7452         3.7671         3.6658         0.0232         0.0237		Dg	7 6347	90%	3 6553	4 1575	3 2417	0.0157
D10         0.9690         90%         2.6242         2.6259         2.6024         0.0119           (-1.5, -0.5)         95%         3.3455         3.3470         3.3339         0.0203           D11         0.0768         90%         2.4100         2.4101         2.4075         0.0144           95%         3.2526         3.2526         3.2526         3.25787         0.0247           D12         1.9718         90%         2.9700         2.9933         2.6802         0.0137           95%         3.7452         3.7671         3.6658         0.0232         0.0232			1.0047	95%	4 5634	5 1046	4 0763	0 0254
(-1.5, -0.5) 95% 3.3455 3.3470 3.3339 0.0203 D11 0.0768 90% 2.4100 2.4101 2.4075 0.0144 95% 3.2526 3.2526 3.2787 0.0247 D12 1.9718 90% 2.9700 2.9933 2.6802 0.0137 95% 3.7452 3.7671 3.6658 0.0232	-	D10	0.989.0	90%	2 6242	2 6259	2 6024	0 0119
D11         0.0768         90%         2.4100         2.4101         2.4075         0.0144           95%         3.2526         3.2526         3.2526         3.2526         3.2526         0.0247           D12         1.9716         90%         2.9700         2.9933         2.6802         0.0137           95%         3.7452         3.7671         3.6658         0.0232	1-15 -0.51	0.10	0.0000	95%	3 3455	3 3470	3 3339	0 0203
95%         3.2526         3.2526         3.2787         0.0247           D12         1.9718         90%         2.9700         2.9933         2.6802         0.0137           95%         3.7452         3.7671         3.6658         0.0232         0.0232	1.0, 0.0	D11	0.0788	90%	2 4100	2 4101	2 4075	0 0144
D12 1.9718 90% 2.9700 2.9933 2.6802 0.0137 95% 3.7452 3.7671 3.6658 0.0232			0.0100	95%	3 2526	3 2526	3 2787	0.0247
95% 3.7452 3.7671 3.6658 0.0232	1	D12	1 9718	90%	2 9700	2 9933	2 6802	0.0137
	1000			95%	3.7452	3.7671	3.6658	0.0232

d.f. = 4

Table 5.12: Critical values for cubic regression

RI	DM	k0	cl	cv nai	cv app	cy simu	s.e.
10-1-0-2-1-	D1	9:5821	90%	4.4008	5.3870	4.2972	0.0232
A DESCRIPTION OF			95%	5.7397	6.9125	5.6521	0.0376
E F	D2	8.1877	90%	4.3208	5.1235	4.2971	0.0208
(-1, 1)			95%	5.6370	6.5862	5 5020	0.0368
	D3	8.5104	90%	4.3411	5.1869	3,0442	0.0157
a contra de			95%	5.6632	6.6646	4.0336	0.0336
	D4	6.2884	90%	4.1715	4.7173	4 1753	0.0235
			95%	5.4458	6.0843	5.3716	0.0456
	D1	9 4935	90%	4.3962	5.3710	4.2923	0.0217
1			95%	5.7340	6.8926	5.5911	0.0489
1	D2	0.2424	90%	2.5223	2.5223	2.5073	0.0157
(-0.7. 0.7)			95%	3:3911	3.3911	3.3663	0.0205
in the second	D3	0.1246	90%	2.4421	2.4421	2.4672	0.0167
		Section Company	95%	3.2923	3.2923	3.2890	0.0250
ſ	D4	3.7802	90%	3.8356	4.0542	3.7480	0.0193
			95%	5.0191	5.2678	4.9218	0.0311
ET NULL I	D5	9:6723	90%	4.4053	5.4033	3.1014	0.0190
			95%	5.7455	6.9326	4.1268	0.0342
	D6	5.2263	90%	4.0558	4.4585	3.8969	0.0185
(0.2)			95%	5.2984	5.7651	5.1019	0.0352
	D7	6.4701	90%	4.1885	4.7591	4.0562	0 0205
1.1.1			95%	5.4676	6.1356	5:2982	0.0472
	D8	6.2884	90%	4,1715	4.7173	4.1380	0.0268
and the second		Section 1	95%	5,4458	6:0843	5.4158	0.0488
	D5	9.4448	90%	4.3936	5.3621	3.1369	0.0180
			95%	5.7306	6.8816	4.0577	0.0310
	D6	0:0600	90%	2.3967	2.3967	2.3913	0.0147
(0.6, 1.4)		- management of	95%	3.2362	3.2360	3.2062	.0.0249
100 M	D7	0.0281	90%	2.3737	2.3738	2.3895	0.0157
			95%	3.2078	3.2077	3.2094	0.0247
	D8	2.1419	90%	3.4282	3.4852	3.4198	0.0195
	-4		95%	4.5077	4.5702	4.5244	0.0323
	D9	9.6721	90%	4,4053	5.4033	2.8066	0.0162
		1 - march	95%	5.7455	6.9326	3 7636	0.0237
in the second	D10	7.5293	90%	4.2754	4.9897	4.1819	0.0212
(-2, 0)			95%	5.5789	6.4206	6.4942	0.0320
	D11	4.5032	90%	5.2095	6.0663	4.8847	0.0382
			95%	7.5187	7.9999	7.1059	0.0641
	D12	6.2884	90%	4.1715	4.7173	4.1431	0.0218
	1.11		95%	5.4458	6.0843	5.4060	0.0419
	D9	9.5552	90%	4,3994	5.3822	2.8201	0.0181
			95%	5.7380	6.9065	3.7483	0.0275
	D10	0.0920	90%	2.4193	2,4194	2.4388	0.0142
(-1.5, -0.5)			95%	3.2642	3.2641	3.2449	0.0208
	D11	0.0757	90%	2.9974	2.9973	3.0243	0.0215
			95%	4.4105	4.4105	4.3834	0.0411
	D12	2.7749	90%	3.6135	3.7234	3.5764	0.0176
		1.1.1.1.1	95%	4.7392	4.8619	4.6602	0.0326

d.f. = 3

ŧ

Table 5.13: Critical values for 4th order polynomial regression

RI	DM	k0	cl	cv nai	cv app	cv_simu	s.e.
	D13	4.9197	90%	2:4691	2.5355	2.4382	0.0065
-		and the second	95%	2.8000	2.8462	2.7746	0:0089
	D14	3.1530	90%	2.3533	2.3675	2,3498	0.0064
(-1, 1)	19/0 21	1.0556.73	95%	2.6800	2.6875	2.6718	0.0082
	D15	2.5281	90%	2.2842	2.2887	2.2341	0:0071
1.1.1			95%	2.6111	2.6131	2.5730	0.0086
F	D16	2.9628	90%	2.3344	2:3449	2:3505	0.0067
			95%	2.6607	2.6662	2.6815	0.0083
1	D13	4.6777	90%	2.4582	2.6159	2.4377	0.0074
and the second second			95%	2.7883	2.8277	2.7728	0.0085
	D14	1:0013	.90%	2.0125	2.0125	2.0029	0.0076
(-0.7. 0.7)		1.2.2.1	95%	2.3505	2.3506	2.3554	0.0088
	D15	0.6914	90%	1.9315	1.9316	1.9276	0.0069
			95%	2.2725	2.2725	2.2476	0.0078
	D16	1.7779	90%	2,1720	2.1723	2.2024	0.0073
			95%	2.5028	2.5030	2.5401	0.0086
(0. 2)	D17	5.0496	90%	2.4747	2.5457	2.4522	0.0066
			95%	2.6057	2.8558	2.7696	0.0094
	D18	3.2945	90%	2.3664	2.3835	2.3757	0.0063
		In course of the same	95%	2.6931	2.7026	2.6776	0.0077
	D19	2.4902	90%	2.2793	2.2835	2.2359	0.0071
-			95%	2.6054	2.6082	2.5724	0.0086
	D20	2,9628	90%	2.3344	2.3449	2.3519	0.0066
		Sensoria Sid Leving	95%	2.6607	2.6662	2.6945	0.0102
and the owned	D17	4.1075	90%	2.4273	2.4660	2.4333	0.0061
			95%	2.7557	2.7806	2.7461	0.0078
	D18	0.2998	90%	1.8088	1.8087	1.8073	0.0073
(0.6, 1.4)			95%	2.1521	2.1522	2.1339	0.0097
	D19	0.1976	90%	1.7719	1.7720	1.7763	0.0065
	and the state		95%	2.1156	2.1156	2.1129	0.0086
	D20	0.7848	90%	1.9573	1.9573	1:9816	0.0070
			95%	2.2973	2.2974	2.3296	0.0086
100	D21	4.6422	90%	2.4564	2,5130	2.4466	0.0064
1.1.1			95%	2.7865	2.8249	2 7731	0.0074
	D22	3 1560	90%	2.3537	2.3678	2.3298	0.0067
(-2, 0)			95%	2.6802	2.6878	2.6763	0.0082
-	D23	2.9052	90%	2.3283	2.3379	2.2900	0.0077
	-		95%	2.6548	2.6595	2.6175	0.0080
	D24	3.4094	90%	2.3765	2.3962	2.3978	0.0071
			95%	2,7034	2.7146	2.7133	0.0079
	D21	3.5553	90%	2.3884	2.4117	2.3952	0.0066
			95%	2,7157	2.7292	2.7239	0.0080
	D22	0.6325	90%	1.9147	1.9147	1.9245	0.0070
(-1.5, -0.5)	and the second second		95%	2.2561	2.2562	2.2638	0.0080
	D23	0.8735	90%	1.9805	1.9806	1.9765	0.0070
			95%	2.3199	2.3199	2.3127	0.0088
	D24	1.2993	90%	2.0799	2.0799	2.1136	0.0069
10-20			.95%	2,4152	2.4151	2,4545	0.0083

d.f. = 32

t

Table 5.14: Critical values for quadratic regression

RI	DM	kO	cl	cv nai	cv app	cv simu	s.e.
	D13	7:0573	90%	2.6222	2.6824	2.5529	0.0067
			95%	2.9472	2.9871	2.6868	0.0083
	D14	3.9602	90%	2.4463	2.4559	2.4316	0.0058
(-1, 1)		and and	95%	2.7680	2.7726	2.7421	0.0093
	D15	3.3519	90%	2.3890	2.3933	2.2818	8300.0
			95%	2.7117	2.7135	2.6065	0.0087
	D16	3.6551	90%	2.4189	2.4256	2.4021	0.0058
S. A.			95%	2.7411	2.7440	2.7063	0.0078
	D13	6.7986	90%	2,6123	2.6675	2.5467	0.0064
1.00			95%	2.9369	2.9729	2.8835	0.0085
	D14	1.5989	90%	2.1424	.2.1424	2.1347	0.0065
(-0.7. 0.7)			95%	2,4759	2.4760	2.4677	0.0084
	D15	0.8327	90%	1.9722	1.9721	1,9681	0.0076
			95%	2.3130	2.3130	2.2959	0.0083
	D16	2,2531	90%	2.2519	2.2522	2.2280	0.0074
12.1			95%	2.5800	2,5801	2.6531	0.0094
	D17	7,1639	90%	2.6262	2.6884	2.4989	0.0072
			95%	2.9511	2,9927	2,8375	0 0088
	D18	4.2371	90%	2:4691	2.4816	2.3972	0 0065
(0.2)			95%	2,7907	2.7971	2,7251	0.0095
	D19	3:3726	90%	2.3912	2.3955	2.2941	0.0073
			95%	2 7137	2.7157	2.6332	0.0106
	D20	3 6551	90%	2 4189	2 4256	2.3320	0.0065
			95%	2 7411	2.7440	2.6387	0.0086
	D17	6.0044	90%	2.5780	2.6180	2,4901	0.0063
6. 11 - 1	na in		95%	2,9009	2,9260	2,8361	0.0090
	D18	0.9009	90%	1,9899	1.9898	1.9874	0.0068
(0.6. 1.4)			95%	2.3301	2.3300	2.3184	0.0090
	D19	0.2084	90%	1,7776	1.7777	1,7852	0.0068
			95%	2.1224	2.1223	2.1200	0.0093
	D20	1.4320	90%	2.1099	2.1098	2.0644	0.0064
			95%	2.4449	2.4450	2,3894	0.0082
	D21	6.8471	90%	2,6143	2.6704	2.3760	0.0075
			95%	2,9388	2.9756	2.7088	0.0085
	D22	4:0813	90%	2.4564	2.4673	2,3510	0.0062
(-2, 0)			95%	2,7782	2.7835	2.6671	0.0089
	D23	4.3276	90%	2,4761	2.4899	2.3165	0.0073
			95%	2.7976	2.8047	2.6534	0.0077
	D24	4.6027	90%	2.4963	2.5136	2.4314	8300.0
			95%	2.8178	2.8272	2.7686	0.0089
	D21	4.8340	90%	2.5120	2.5327	2.3435	0.0063
			95%	2.8337	2.8452	2.6628	0.0092
	D22	1.1504	90%	2.0498	2.0497	2.0327	0.0073
(-1.50.5)			95%	2.3876	2.3875	2.3488	0.0094
1	D23	1.4132	90%	2.1061	2.1061	2.0828	0.0071
			95%	2.4413	2.4414	2.4096	0.0091
	D24	1.8895	90%	2.1942	2.1943	2.1269	0.0062
	1		95%	2.5252	2.5252	2.4756	0.0090

d.f. = 31

ł.

Table 5.15: Critical values for cubic regression

RI	DM	k0	cl	cv.nai	cy app	cv_simu	s.e.
	D13	9.2648	90%	2.7391	2.7977	2.6963	0.0061
			95%	3.0604	3.0986	3.0410	0.0091
	D14	5.0910	90%	2 5463	2.5573	2.5154	0.0064
(-1, 1)			95%	2.8650	2.8703	2.8492	0.0094
	D15	4.3951	90%	2,4939	2.4998	2.4406	0.0067
			95%	2.8135	2.8160	2.7865	0.0081
	D16	4.4047	90%	2.4947	2.5006	2 4883	0:0060
		· · · · · · · · · · · ·	95%	2.8141	2.8168	2.8012	0.0077
	D13	9.0265	90%	2.7317	2.7870	2.7060	0.0071
			95%	3.0527	3.0885	3.0113	0.0088
	D14	1.6200	90%	2.1491	2.1491	2.147.7	0.0069
(-0.7. 0.7)			95%	2.4838	2.4839	2.4955	0.0094
	D15	0.9211	90%	1:9972	1.9972	1.9958	0.0066
Salt of the	and the second	1	95%	2.3386	2.3385	2.3342	0.0089
	D16	3.1220	90%	2.3697	2,3707	2.3558	0.0069
			95%	2.6937	2.6939	2.7003	8800.0
	D17	9.1250	90%	2.7349	2.7915	2.7118	0.0064
			95%	3.0561	3.0927	3.0191	0.0097
	D18	5 4371	90%	2.5693	2.5832	2.5350	0.0068
(0.2)			95%	2.8879	2.8949	2.8714	0.0089
	D19	4.4390	90%	2.4975	2.5036	2.2368	0 0065
			95%	2.8168	2.8197	2.5548	0.0100
	D20	4.4047	90%	2.4947	2:5005	2.4807	0.0066
and the second			95%	2.8141	2.8168	2.8113	0.0091
	D17	7.7445	90%	2.6859	2.7250	2.6734	0.0061
			95%	3.0055	3.0294	2.9965	0.0082
	D18	0.4016	90%	1.8472	1.8473	1.8443	0.0077
(0.6, 1.4)			95%	2.1924	2.1924	2.1882	0.0077
	D19	0.2045	90%	1.7782	1.7782	1.7843	0.0071
			95%	2.1240	2.1239	2.1238	0.0094
	D20	1.6359	90%	2.1521	2.1521	2.1825	0.0068
			95%	2.4868	2.4867	2.5119	0:0078
	D21	9.0585	90%	2.7327	2.7865	2.6984	0.0067
			95%	3.0539	3.0898	3:0313	0.0085
	D22	5.8540	90%	2.5947	2.6125	2.5742	0.0068
(-2, 0)		1	95%	2.9132	2.9227	2.6829	0.0082
	D23	5.3951	90%	2.5667	2.5801	2.4705	0.0063
100		in the second second	95%	2.8851	2.8920	2.7948	0.0096
	D24	5.5182	90%	2.5744	2.5890	2.5779	0.0073
	an inge	1	95%	2.8930	2,9004	2.8764	0.0083
	D21	6.3495	90%	2.6220	2,6450	2.5869	0.0069
			95%	2.9408	2.9534	2.9319	0.0092
	D22	0.9055	90%	1.9934	1.9933	1:9995	0.0073
(-1.5, -0.5)	americ		95%	2.3346	2.3347	2.3367	0.0095
	D23	2.0226	90%	2.2194	2.2193	2.2092	0.0066
			95%	2.5506	2.5505	2.5419	0.0087
[	D24	2.5298	90%	2.2951	2.2952	2.3250	0.0063
			95%	2.6224	2.6225	2.6458	0.0090

d.f. = 30

ť

Table 5.16: Critical values for 4th order polynomial regression

#### 5.5.3 For bivariate linear regression

Also, it is of interest to compare the methods of constructing confidence bands for a multiple linear regression. Here, we consider the bivariate linear regression model, which is the simplest one in multiple case, with the predictor variables restricted in a rectangular region  $\mathcal{X} \subset \mathcal{R}^2$ . The methods concerned in this comparison are the approximate method of Sun and Loader (1994) and the simulation-based method of Liu, Jamshidian, Zhang and Donnelly (2005).

For the approximate method, we calculate critical values using the formula given in Proposition 5.2.2 that

$$\alpha = \frac{\kappa_0}{\pi^{3/2}} \frac{\Gamma((\nu+1)/2)}{\Gamma(\nu/2)} \frac{c}{\sqrt{\nu}} (1 + \frac{c^2}{\nu})^{-(\nu+1)/2} + \frac{\zeta_0}{2\pi} (1 + \frac{c^2}{\nu})^{-\nu/2} + P\{|t_\nu| > c\}.$$
(5.36)

Constants  $\kappa_0$  and  $\zeta_0$  can be computed by

$$\kappa_0 = \int_{\mathcal{X}} \det^{1/2} (A^T A) d\mathbf{x}, \qquad (5.37)$$

$$\zeta_0 = \int_{\partial \mathcal{X}} \det^{1/2} (\mathbf{A}_*^T \mathbf{A}_*), \qquad (5.38)$$

where  $A = (\mathbf{T}_1(\mathbf{x}), \mathbf{T}_2(\mathbf{x}))$ , and  $\mathbf{A}_* = \mathbf{T}_1(\mathbf{x})$  or  $\mathbf{T}_2(\mathbf{x})$  with  $\mathbf{T}_j(\mathbf{x})$  defined by  $\mathbf{T}_j(\mathbf{x}) = \partial \mathbf{T}(\mathbf{x})/\partial x_j$  for j = 1, 2. Note that  $\mathbf{T}(\mathbf{x}) = \mathbf{l}(\mathbf{x})/||\mathbf{l}(\mathbf{x})||$ , where  $\mathbf{l}(\mathbf{x}) = X(X^T X)^{-1}\mathbf{x}$ , and  $\mathbf{x} = (1, x_1, x_2)^T$ . Thus, we have

$$\begin{aligned} \mathbf{T}_{1}(\mathbf{x}) &= \frac{\mathbf{l}'(\mathbf{x}) \|\mathbf{l}(\mathbf{x})\| - \mathbf{l}(\mathbf{x}) \|\mathbf{l}(\mathbf{x})\|'}{\|\mathbf{l}(\mathbf{x})\|^{2}} \\ &= \frac{\mathbf{l}'(\mathbf{x}) (\|\mathbf{l}(\mathbf{x})\|^{2})^{1/2} - \mathbf{l}(\mathbf{x}) [(\|\mathbf{l}(\mathbf{x})\|^{2})^{1/2}]'}{\|\mathbf{l}(\mathbf{x})\|^{2}} \\ &= \frac{\mathbf{l}'(\mathbf{x}) (\|\mathbf{l}(\mathbf{x})\|^{2})^{1/2} - (1/2)\mathbf{l}(\mathbf{x}) (\|\mathbf{l}(\mathbf{x})\|^{2})^{-1/2} (\|\mathbf{l}(\mathbf{x})\|^{2})'}{\|\mathbf{l}(\mathbf{x})\|^{2}}, (5.39) \end{aligned}$$

where

$$\begin{aligned} \mathbf{l}'(\mathbf{x}) &= \partial \mathbf{l}(\mathbf{x}) / \partial x_1 = X(X^T X)^{-1}(0, 1, 0)^T, \\ \| \mathbf{l}(\mathbf{x}) \|^2 &= \mathbf{l}^T(\mathbf{x}) \mathbf{l}(\mathbf{x}) = \mathbf{x}^T (X^T X)^{-1} \mathbf{x}, \\ (\| \mathbf{l}(\mathbf{x}) \|^2)' &= 2 \cdot \mathbf{l}^T(\mathbf{x}) \mathbf{l}'(\mathbf{x}) = 2 \cdot \mathbf{l}^T(\mathbf{x}) \cdot X(X^T X)^{-1}(0, 1, 0)^T. \end{aligned}$$

Similarly, we can obtain  $\mathbf{T}_2(\mathbf{x})$  by replacing  $(0, 1, 0)^T$  by  $(0, 0, 1)^T$  and  $\mathbf{T}_1(\mathbf{x})$  by  $\mathbf{T}_2(\mathbf{x})$  in (5.39). Then both A and  $\mathbf{A}_*$  are ready. Numerical integrations may be used to compute constants  $\kappa_0$  and  $\zeta_0$ .

For the simulation-based method, as described in Section 5.4, the main task is to solve the optimization problem to find T. In practice, we compute critical values using SimReg software from Jamshidin, Liu, Zhang and Jamshidian (2004) on MATLAB 7 platform.

Now, we turn to choose the levels of the common factors for our comparison. Apparently, both methods depend on the design matrix, restricted intervals of the two predictor variables  $x_1$  and  $x_2$ , and the confidence level. Furthermore, recall (5.28) that

$$T = Q \frac{\|\mathbf{N}\|}{(\hat{\sigma}/\sigma)},$$

where

$$Q = \sup_{x_1 \in (a_1, b_1), x_2 \in (a_2, b_2)} \frac{|(P\mathbf{x})^T \mathbf{N}|}{\|P\mathbf{x}\| \|\mathbf{N}\|}$$

Since N and  $(\hat{\sigma}/\sigma)$  are generated numbers, the simulation-based method, in fact, depends on the 3-dimensional vector  $P_{\mathbf{x}}$  together with the two restricted intervals  $(a_1, b_1)$  and  $(a_2, b_2)$ . Let  $P = (\mathbf{p}_0, \mathbf{p}_1, \mathbf{p}_2)$  and define the set

$$\mathcal{L} = \{ P\mathbf{x} : \mathbf{x} \in \mathcal{X} \}$$
  
= {  $\mathbf{p}_0 + x_1\mathbf{p}_1 + x_2\mathbf{p}_2 : x_1 \in [a_1, b_1], x_2 \in [a_2, b_2] \}.$ 

Then, we have

$$Q = \sup_{\mathbf{v} \in \mathcal{L}} \frac{\mathbf{v}^T \mathbf{N}}{\|\mathbf{v}\| \|\mathbf{N}\|},\tag{5.40}$$

where  $\mathbf{v}^T \mathbf{N} / \|\mathbf{v}\| \|\mathbf{N}\|$  is simply the cosine of the angle between  $\mathbf{v}$  and  $\mathbf{N}$ . This determines that, in order to obtain Q, it is sufficient to find the smallest angle between either  $\mathbf{N}$  and  $\mathbf{v}$  or  $-\mathbf{N}$  and  $\mathbf{v}$ , as  $\mathbf{v}$  ranges in  $\mathcal{L}$ . Note that  $\mathcal{L}$  is the



Figure 5.2: The cone determined by three angles

cone spanned by the following four vectors

$$\begin{aligned} \mathbf{v}(a_1, a_2) &= \mathbf{p}_0 + a_1 \mathbf{p}_1 + a_2 \mathbf{p}_2, \\ \mathbf{v}(b_1, a_2) &= \mathbf{p}_0 + b_1 \mathbf{p}_1 + a_2 \mathbf{p}_2, \\ \mathbf{v}(a_1, b_2) &= \mathbf{p}_0 + a_1 \mathbf{p}_1 + b_2 \mathbf{p}_2, \\ \mathbf{v}(b_1, b_2) &= \mathbf{p}_0 + b_1 \mathbf{p}_1 + b_2 \mathbf{p}_2, \end{aligned}$$

and it is depicted in Figure 5.2.

Define three angles that  $\alpha$  is the angle between  $\mathbf{v}(a_1, a_2)$  and  $\mathbf{v}(b_1, a_2)$ ,  $\beta$  is the angle between  $\mathbf{v}(b_1, a_2)$  and  $\mathbf{v}(b_1, b_2)$ ,  $\theta$  is the angle between the two planes  $S_1$  and  $S_2$ , where  $S_1$  is spanned by  $\mathbf{v}(a_1, a_2)$  and  $\mathbf{v}(b_1, a_2)$ ,  $S_2$  is spanned by  $\mathbf{v}(b_1, a_2)$  and  $\mathbf{v}(b_1, b_2)$ . Then the cone  $\mathcal{L}$  is determined by these three angles. Therefore, we may conclude that the simulation-based method essentially depends on the three angles  $\alpha, \beta, \theta$ , the degree of freedom, and the confidence level. This is the nature of the simulation-based method. Also, the approximate method depends on the three angles via the design matrix and the two restricted intervals of the predictor variables. In this comparison, we fix a design matrix and then appropriately choose the restricted intervals such that their combinations determine manifold levels of the three angles.

First, we come to choose the design matrix. The acetylene data of Snee

(1977) is adopted here, since it was used to construct confidence bands in many papers. Another reason to select this dataset is that the critical value computed by my MATLAB programme of the approximate method is the same as the one given in Sun and Loader (1994) for this data when the confidence level is 95% and  $\mathcal{X} = [1100, 1300] \times [5.3, 23]$ . So we can reasonably think that my programme is reliable.

ł

Next, we turn to choose the restricted intervals of the two predictor variables. First consider the three angles  $\alpha$ ,  $\beta$  and  $\theta$ . We are willing to obtain various structures of the cone determined by these three angles. Set three levels for each angle from small to large within its range  $[0, \pi]$ . So we have  $3 \times 3 \times 3 = 27$  structures for the cone. However, realize that for a fixed  $\theta$  when  $\alpha$  and  $\beta$  switch their values, the cone newly obtained has a similar structure with the original cone. Also, note that for fixed  $\alpha$  and  $\beta$ , the cone with large  $\theta$  is similarly structured with the one having small  $\theta$ . Thus, for the sake of similarity, the cone finally has 12 structures of interest. They are SSM, SMM, SLM, MMM, MLM, LLM, SSL, SML, SLL, MML, MLL, LLL, where characters S, M, L stand for small value (around  $\pi/12$ ), medium value (around  $\pi/2$ ) and large value (around  $8\pi/9$ ) respectively for the three angles, and the 3-character string denotes the level of each angle in order, e.g., SLM describes the situation that  $\alpha$  is small,  $\beta$  is large, and  $\theta$ is medium. Now, it is ready to choose the restricted intervals for predictor variables. We use the design matrix and any two initial guesses of restricted intervals to calculate  $\alpha$ ,  $\beta$  and  $\theta$ , then adjust the restricted intervals to ensure the three angles each is near the level of our interest. One may follow the procedure below to find the restricted intervals:

Step 1 Adjust  $b_1$  and  $a_2$  to ensure  $\theta$  is ok.

Step 2 Fix  $b_1$  and  $a_2$ , adjust  $a_1$  to ensure  $\alpha$  is ok.

Step 3 Fix  $b_1$  and  $a_2$ , adjust  $b_2$  to ensure  $\beta$  is ok.

In such a way, we obtain 12 pairs of the restricted intervals for the predictor variables  $x_1$  and  $x_2$  according to 12 structures of the cone.

Restricted	T	hree angl	85	Confidence	Critical values		
intervals	alpha	beta	theta	level	cv app	cv simu	5.8.
(10, 950)	0.2183	0.2315	1.6041	90%	2.1691	2.2749	0.0081
(13. 15)	S	S	44	95%	2.7441	2.8654	0.0122
(1070 1250)	0.3071	1.5149	1:5630	90%	3.2006	3.1088	0.0098
(10, 50)	S	М	M	95%	3.8945	3,7947	0.0128
(920, 1620)	0.4079	2.7006	1.6081	90%	3.3834	3.1857	0.0089
(12, 130)	S	L	64	95%	4.0981	3.9022	0.0152
(100, 1220)	1.6414	1.6184	1.5686	90%	3.0510	2.9914	0.0082
(0, 12)	M	id	M	95%	3.7272	3.6839	0:0147
(650, 1600)	1.6860	2.8126	1.6059	90%	3.3808	3.1713	0.0088
(12.40)	M	L	61	95%	4.0947	3.8897	0.0158
(10, 1600)	2.8843	2,8546	1.6059	90%	3.1580	2.9299	0.0090
(12. 15)	. <i>L</i>	L	М	95%	3.8405	3.5917	0.0149
(1450, 1650)	0.2418	0.1853	2.8146	90%	2.3135	2.3478	0.0077
(-1D, 5)	5	S .	L	95%	2.9053	2.9487	0.0123
(950, 1800)	0.2485	1.6552	2.8438	90%	3:6521	3.2924	0.0104
(-10, 250)	S	М	L	95%	4.4000	4.0240	0.0137
(900, 1750)	0.2677	2.7231	2.9895	90%	3.2545	3.0841	0.0094
(-200, 10)	S	L	L	95%	3.9523	3.7844	0.0134
(950, 1800)	1.6552	1:6400	2.8438	90%	3.6341	3.2920	0.0105
(-10, 40)	ist	M	L	95%	4.3798	4.0229	0.0137
(800, 2000)	1.6351	2.8342	2.9377	90%	3:2630	3.0733	0.0105
(-22, 10)	M	L	L	95%	3.9613	3.7748	0.0131
(400, 2200)	2.7204	2.8541	2.7026	90%	3:0603	2.8362	0.0084
(0.5)	L	L	L	95%	3.7288	3.5086	0.0163

d.f. = 5

Table 5.17: Critical values for bivariate linear regression

We still use 90% and 95% confidence levels. Moreover, we manually set the degree of freedom equal to 5 and 30 to have a general view. Critical values are computed based on the designs described above. All the results are contained in Tables 5.17 and 5.18. Note that the critical values of the simulation-based method are based on 100,000 simulations.

From the result, we can draw some conclusions. The simulation-based method obtains smaller critical values than the approximate method generally, except for the cases when  $\alpha$  and  $\beta$  are both small. When  $\nu = 5$ , the difference between the critical values of the two methods is generally around 0.2; the critical values of the approximate method are at most 11% larger than those of the simulation-based method. When  $\nu = 30$ , the difference between the critical values of the two methods is not apparent, generally at the second decimal place.

d.f.	-	30
սու	-	20

¢

,

Restricted	-	hree angl	es	Confidence	C	ritical valu	es
intervals	alpha	beta	theta	level	cv app	cv_simu	s.e.
(10, 950)	0.2183	0.2315	1.6041	90%	1.8105	1.8808	0.0052
(13, 15)	S	S	M	95%	2 1566	2.2243	0.0066
(1070, 1250)	0.3071	1.5149	1.5630	90%	2.4886	2.4657	0.0051
(10, 50)	S	. М	M	95%	2.8211	2.8037	0.0066
(920, 1620)	0.4079	2.7006	1.6081	90%	2.5937	2.5257	0.0047
(12, 130)	S	L	M	95%	2.9223	2.8666	0.0065
(100, 1220)	1.6414	1.6184	1.5686	90%	2.3970	2.3846	0.0049
(0. 12)	14	M	M	95%	2.7318	2.7247	0.0064
(650, 1600)	1.6860	2.8126	1.6059	90%	2.5911	2.5158	0.0046
(12, 40)	М	L	14	95%	2.9196	2.8579	0.0066
(10, 1600)	2.8843	2.8546	1.6059	90%	2.4485	2.3550	0.0055
(12, 15)	Ľ	L	M	95%	2.7764	2.6967	0.0071
(1450, 1650)	0.2418	0.1853	2.8146	90%	1.9131	1.9404	0.0050
(-10, 5)	S.	.s	L	95%	2.2583	2.2829	0.0066
(950, 1800)	0.2485	1.6552	2.8438	90%	2.7480	2.6028	0.0051
(-10, 250)	S	М	L	95%	3.0725	2,9533	0.0063
(900, 1750)	0.2677	2.7231	2.9895	90%	2.5146	2.4507	0.0048
(-200, 10)	S	L	L	95%	2.8443	2.7920	0.0068
(950, 1800)	1.6552	1.6400	2.8438	90%	2:7382	2.6016	0.0051
(-10, 40)	. M.	M	. L .	95%	3.0630	2.9528	0.0064
(800, 2000)	1:6351	2.8342	2.9377	90%	2.5183	2.4453	0.0047
(-22, 10)	is	L	L	95%	2.8474	2.7861	0.0069
(400, 2200)	2:7204	2.8541	2.7026	90%	2.3842	2.2862	0.0050
(0, 5)	L	L	L	95%	2.7111	2.5270	0.0069

Table 5.18: Critical values for bivariate linear regression

#### 5.5.4 Conclusions

Overall, it may be concluded from our comparisons that the simulationbased method computes as good critical values as the exact method, better than either the conservative method or the approximate method. When we increase the number of simulations, the simulation-based method may get even accurate critical values. Meanwhile, it can be found that Naiman's method is good enough. That is because Naiman's critical values are for conservative confidence bands but they are actually not much conservative. Comparatively speaking, the approximate method is bad, but not seriously.

### 5.6 Numerical examples

#### 5.6.1 Example for simple linear regression

In an 1857 article, a Scottish physicist named James D. Forbes discussed a series of experiments that he had done concerning the relationship between atmospheric pressure and the boiling point of water. He believed that altitude could be determined by atmospheric pressure, measured with a barometer which was a fragile instrument in the middle of the nineteenth century, with lower pressures corresponding to higher altitudes. Forbes wondered whether a simpler measurement of the boiling point of water could substitute for a direct reading of barometric pressure to determine the altitude. He collected data in the Alps and in Scotland and measured pressure in inches of mercury with barometer and boiling point in degrees Fahrenheit using a thermometer at each location. Boiling point measurements were adjusted for the difference between the ambient air temperature when he took the measurements and a standard temperature. The data for 17 locations are reproduced in Table 5.19, which is taken from Weisberg (2005, page 22).

A simple linear regression model is used to fit the data. Atmospheric pressure is viewed as the response and the boiling point of water is regarded as the only predictor variable in the model. Therefore, we have the fitted

Case Number	Temperature	Pressure
1	194.5	20.79
2	194.3	20.79
3	197.9	22.40
4	196.4	22.67
5	199.4	23.15
6	199.9	23.35
7	200.9	23.89
8	201.1	23.99
9	201.4	24.02
10	201.3	24.01
11	203.6	25.14
12	204.6	26.57
13	209.5	28.49
14	208.6	27.76
15	210.7	29.04
16	211.9	29.88
17	212.2	30,06

Table 5.19: Forbes' 1857 data on boiling point and barometric pressure for 17 locations in the Alps and Scotland

regression model given by

$$\hat{y} = -81.0637 + 0.5229x. \tag{5.41}$$

Simultaneous confidence bands can be constructed then over a restricted interval, say, [194.3, 212.2] which takes the smallest and largest observations as the lower and upper bounds. The exact method provides critical values 2.2822, 2.6693 and 3.5122 for 90%, 95% and 99% confidence levels respectively; the approximate method suggests 2.3171, 2.6946, 3.5270, and the simulation-based method gives 2.2837, 2.6715, 3.4968 correspondingly. Note that the simulation-based method is on a basis of 100,000 replicates, and will be so for the other examples in this chapter. The confidence bands are plotted in Figures 5.3-5.5.

#### 5.6.2 Example for polynomial regression

Table 5.20 presents data concerning the strength of kraft paper and the percentage of hardwood in the batch of pulp from which the paper was produced.



Figure 5.3: Confidence bands for 90% confidence level



Figure 5.4: Confidence bands for 95% confidence level



Figure 5.5: Confidence bands for 99% confidence level

These data is taken from Montgomery, Peck and Vining (2006, page 205).

A scatter plot of the data displays that a quadratic regression model may adequately describe the relationship between tensile strength and hardwood concentration. According to these data, the fitted model is given by

$$\hat{y} = -6.6742 + 11.7640x - 0.6345x^2. \tag{5.42}$$

Note that x% here is a percentage so that x should be bounded by the interval [0, 100]. Then we construct simultaneous confidence bands over this restricted interval using Naiman's methods, the approximate method, and the simulation-based method. Consequently, these three methods give critical values 2.5661, 2.6476, 2.5483 for 90% confidence level, and 2.9482, 3.0095, 2.9396 for 95% level, respectively. We plot the confidence bands in Figures 5.6 and 5.7. Note that the bands plotted in the figures are parts of the whole bands over the restricted interval. Doing this is in order to make the observed points more clear.

Hardwood concentration (%)	Tensile strength (psi)	
1	6.3	
1.5	11.1	
2	20.0	
3	24:0	
4	26.1	
4.5	30.0	
5	33.8	
5.5	34.0	
6	36.1	
6.5	39.9	
7	42.0	
8 .	46.1	
9	53.1	
10 .	52.0	
11	52.5	
12	48.0	
13	42.8	
14	27.8	
15	21.9	

ł

Table 5.20: Hardwood concentration in pulp and tensile strength of kraft paper



Figure 5.6: Confidence bands for 90% confidence level



Figure 5.7: Confidence bands for 95% confidence level

#### 5.6.3 Example for bivariate linear regression

A soft drink bottler is analyzing the vending machine service routes in his distribution system. He is interested in predicting the amount of time required by the route driver to service the vending machines in an outlet. This service activity includes stocking the machine with beverage products and minor maintenance or housekeeping. It is suggested by the industrial engineer for this study that the two most important factors affecting the delivery time (y) are the number of cases of product stocked  $(x_1)$  and the distance walked by the route driver  $(x_2)$ . 25 observations on the delivery time has been collected by the engineer, and they are shown in Table 5.21. These data is also taken from Montgomery, Peck and Vining (2006, page 70).

We fit the data using a bivariate linear regression model. Therefore, the fitted model is given by

$$\hat{y} = 2.3412 + 1.6159x_1 + 0.0144x_2. \tag{5.43}$$

We assume the maximum capacity of product stocked is 30 cases and the distance is preferred within 2000 ft. Then  $x_1$  and  $x_2$  should be bounded by

Observation	Delivery Time	Number of	Distance
number	(min)	cases	(ft)
1	16.6B	7	560
2	11.50	3	220
3	12:03	3	340
4	14.88	4	80
5	13.75	6	150
6	18.11	7	330
7	8.00	2	110
8	17.83	7	210
9	79.24	30	1460
10	21.50	5	605
11	40.33	16	668
12	21.00	10	215
13	13.50	4	255
14	19.75	6	462
15	24 00	9	448
16	29.00	10	776
17	15.35	6	200
16	19.00	7	132
19	9.50	3	36
20	35.10	17	770
21	17.90	10	140
22	52.32	26	810
23	18.75	9	450
24	19.83	8	635
25	10,75	4	150

Table 5.21: Delivery time data for bivariate example



Figure 5.8: The approximate band for 90% confidence level

the intervals [0, 30] and [0, 2000] respectively. In such a case, simultaneous confidence bands can be constructed accordingly based on the approximate method and the simulation-based method. As results, these two methods suggest critical values 2.7234, 2.6409 for 90% confidence level, and 3.0707, 2.9787 for 95% confidence level, respectively. To be clear, we plot single band in each picture. So the four confidence bands are shown in Figures 5.8-5.11 respectively.



Figure 5.9: The approximate band for 95% confidence level



Figure 5.10: The simulation-based band for 90% confidence level



t

Figure 5.11: The simulation-based band for 95% confidence level

## Chapter 6

# Simultaneous confidence bands for a logistic regression model

The analysis of dichotomous response data has been popular due to the increasing use of the logistic regression model which enjoys a wide variety of applications nowadays, such as medical treatment, clinical trials, epidemiological test and risk management. Construction of simultaneous confidence bands for a logistic regression model is therefore of interest. However, the existing literatures on this are very limited.

Since the asymptotic distributional approximation of the parameter estimators of interest is the base of construction of confidence regions for a generalized linear model, we first briefly review relevant literatures on, for example, the construction of asymptotic intervals for the binomial parameter. By recalling related works, a general profile on the quality of the asymptotic approximation based on several methods would be obtained. The most frequently mentioned interval in many statistical textbooks is the standard or Wald confidence interval. This interval was shown to perform poorly unless the sample size is quite large in, e.g., Ghosh (1979), Blyth and Still (1983). Clopper and Pearson (1934) proposed "exact" confidence interval based on inverting equal-tailed binomial tests. The "exact" interval is usually necessarily conservative. Therefore, it is inappropriate to treat it as optimal for

statistical practice. Agresti and Coull (1998) discussed that the score confidence interval first presented by Wilson (1927) tends to perform much better than the Wald or "exact" intervals in terms of having coverage probabilities close to the nominal confidence level. Zheng and Loh (1995) and Zheng (1998) considered bootstrapping binomial confidence intervals via bootstrap calibration. Brown, Cai and DasGupta (2000, 2001, 2002) provided a survey of these intervals as well as the Bayes credible intervals, and gave comparisons. Chen (1990) demonstrated the accuracy of such approximate intervals for a binomial parameter.

For the construction of simultaneous confidence bands, an alternative of the methods based on the asymptotic distributional property is the bootstrap percentile method, which was proposed by Yeh (1996) to construct confidence bands for unknown curves based on the bootstrap and the concept of "curve depth". However, it is not considered further in this thesis.

In this chapter, we first introduce some key methods of constructing twosided simultaneous confidence bands for the probability of the dichotomous response in a logistic regression model with or without constrained predictor variables. Two examples are given for one-dimensional and two-dimensional cases respectively. Then simulation studies are given for the comparison of the methods. Meanwhile, the simulation results can be used to gauge the accuracy of the asymptotic distributional approximation. That is to check whether the simulated coverage probability of certain band is close to the nominal confidence level, and how far between them.

## 6.1 Confidence bands for a logistic regression without constraint on predictor variables

#### 6.1.1 For a simple logistic regression

Brand, Pinnock and Jackson (1973) described a method of constructing large sample confidence bands for the logistic response curve for the case of p = 1,

where p is the number of the predictor variables in the regression model.

A data set in this case consists of pairs  $(x_i, y_i), i = 1, 2, 3, ..., N$ , where  $x_i$  is, say, a measure of dose received by the *i*th test subject and  $y_i$  is set to 1 or 0 respectively corresponding to that the response does or does not occur in the *i*th subject. N is required sufficiently large for large sample normality to be a reasonable approximation.

The probability of the response corresponding to dose  $x, 0 \le \pi(x) \le 1$ , is defined in terms of parameters  $\beta_0$  and  $\beta_1$  as

$$\pi(x) = \frac{\exp(\beta_0 + \beta_1 x)}{1 + \exp(\beta_0 + \beta_1 x)}.$$
(6.1)

Suppose  $\hat{\beta}_0$  and  $\hat{\beta}_1$  are the maximum likelihood estimators of parameter  $\beta_0$  and  $\beta_1$ . Thus the components of the information matrix  $I_{11}, I_{12}, I_{22}$  can be expressed by

$$I_{11} = \sum_{i=1}^{N} \{ \exp(\hat{\beta}_{0} + \hat{\beta}_{1}x_{i}) / [1 + \exp(\hat{\beta}_{0} + \hat{\beta}_{1}x_{i})]^{2} \},$$

$$I_{12} = \sum_{i=1}^{N} \{ x_{i} \exp(\hat{\beta}_{0} + \hat{\beta}_{1}x_{i}) / [1 + \exp(\hat{\beta}_{0} + \hat{\beta}_{1}x_{i})]^{2} \},$$

$$I_{22} = \sum_{i=1}^{N} \{ x_{i}^{2} \exp(\hat{\beta}_{0} + \hat{\beta}_{1}x_{i}) / [1 + \exp(\hat{\beta}_{0} + \hat{\beta}_{1}x_{i})]^{2} \}.$$

Recall the large sample asymptotic normality of  $\hat{oldsymbol{eta}} = (\hat{eta}_0, \hat{eta}_1)^T$  given by

$$\sqrt{N}(\hat{\boldsymbol{\beta}} - \boldsymbol{\beta}) \xrightarrow{\mathcal{D}} N_2(\boldsymbol{0}, \boldsymbol{\Sigma}),$$
 (6.2)

where  $\xrightarrow{\mathcal{D}}$  denotes convergence in distribution,  $N_2$  denotes the bivariate normal distribution, and  $\Sigma$  is the asymptotic covariance matrix. Note that the asymptotic covariance matrix for  $\hat{\beta}$ ,  $\Sigma/N$ , can be estimated by the inverse of the information matrix  $J^{-1}$ , i.e.,  $\Sigma \approx N J^{-1}$ . Therefore, we have

$$N(\hat{\beta} - \beta)^{T} \Sigma^{-1}(\hat{\beta} - \beta)$$
  

$$\approx (\hat{\beta} - \beta)^{T} J(\hat{\beta} - \beta)$$
  

$$= I_{11}(\hat{\beta}_{0} - \beta_{0})^{2} + 2I_{12}(\hat{\beta}_{0} - \beta_{0})(\hat{\beta}_{1} - \beta_{1}) + I_{22}(\hat{\beta}_{1} - \beta_{1})^{2} \xrightarrow{\mathcal{D}} \chi_{2}^{2}, (6.3)$$

where  $\chi_2^2$  is the Chi-square distribution with two degrees of freedom. A large sample  $1 - \alpha$  confidence set for  $(\beta_0, \beta_1)$  is therefore given by

$$I_{11}(\hat{\beta}_0 - \beta_0)^2 + 2I_{12}(\hat{\beta}_0 - \beta_0)(\hat{\beta}_1 - \beta_1) + I_{22}(\hat{\beta}_1 - \beta_1)^2 \le \chi^2_{2,\alpha}, \qquad (6.4)$$

where  $\chi^2_{2,\alpha}$  denotes the upper  $\alpha$  percentage point of the  $\chi^2_2$  distribution. Note that the confidence set given by (6.4) is an ellipse centered at  $(\hat{\beta}_0, \hat{\beta}_1)$ . A  $100(1-\alpha)\%$  level confidence band for  $\pi(x)$  can be obtained by finding the maximal and minimal values of  $\pi(x)$  over the confidence ellipse of  $(\beta_0, \beta_1)$  for each x.

Transform (6.1) to the form of interest

$$\lambda(x) = \beta_0 + \beta_1 x = \ln\left(\frac{\pi(x)}{1 - \pi(x)}\right)$$
(6.5)

which is a monotone function of  $\pi(x)$ . We can equivalently find the extremal values of  $\lambda(x)$  over the confidence ellipse (6.4) of  $(\beta_0, \beta_1)$  for each x.

For a fixed x,  $\{\beta_0 + \beta_1 x = q : -\infty < q < \infty\}$  stands for a family of parallel straight lines in the  $(\beta_0, \beta_1)$ -plane with x as the slope. Extremal values of  $\lambda(x) = \beta_0 + \beta_1 x$  over the confidence set (6.4) of  $(\beta_0, \beta_1)$  are attained when the lines in the family are tangent to the boundary of the confidence ellipse (6.4). Each tangent line corresponds to one  $(\beta_0, \beta_1)$  which can be viewed as a solution to the pair of equation (6.5) and the equality obtained by changing the sign from " $\leq$ " to "=" in (6.4). Expressing  $\beta_0 = \lambda(x) - \beta_1 x$  from (6.5) and substituting in the obtained equality gives a quadratic equation in terms of  $\beta_1$ , which has the form given by

$$a\beta_1^2 + b\beta_1 + c = 0$$

with

$$a = a_1,$$
  
 $b = b_1 + b_2 \lambda(x),$   
 $c = c_1 + c_2 \lambda(x) + c_3 \lambda(x)^2,$ 

where

$$a_{1} = I_{11}x^{2} - 2I_{12}x + I_{22},$$

$$b_{1} = 2I_{11}x\hat{\beta}_{0} + 2I_{12}(\hat{\beta}_{1}x - \hat{\beta}_{0}) - 2I_{22}\hat{\beta}_{1},$$

$$b_{2} = -2I_{11}x + 2I_{12},$$

$$c_{1} = I_{11}\hat{\beta}_{0}^{2} + 2I_{12}\hat{\beta}_{0}\hat{\beta}_{1} + I_{22}\hat{\beta}_{1}^{2} - \chi^{2}_{2,\alpha},$$

$$c_{2} = -2I_{11}\hat{\beta}_{0} - 2I_{12}\hat{\beta}_{1},$$

$$c_{3} = I_{11}.$$

Notice that there is only one solution of  $\beta_1$  for a straight line tangent to the confidence ellipse. We have

$$b^2 - 4ac = 0$$

which gives a quadratic equation in terms of  $\lambda(x)$ . And the resulting roots provide the extremal values of  $\lambda(x)$  over the confidence set (6.4) of  $(\beta_0, \beta_1)$ . We denote the maximum and minimum values of  $\lambda(x)$  by  $\lambda_H(x)$  and  $\lambda_L(x)$ respectively, which are therefore given by

$$\lambda_{H}(x), \lambda_{L}(x) = \frac{-(2b_{1}b_{2} - 4a_{1}c_{2})}{2(b_{2}^{2} - 4a_{1}c_{3})} \\ \pm \frac{[(2b_{1}b_{2} - 4a_{1}c_{3})^{2} - 4(b_{2}^{2} - 4a_{1}c_{3})(b_{1}^{2} - 4a_{1}c_{1})]^{\frac{1}{2}}}{2(b_{2}^{2} - 4a_{1}c_{3})}.$$
(6.6)

Also,  $\lambda_H(x)$  and  $\lambda_L(x)$  can be written in matrix form as

$$\begin{aligned} \lambda_H(\mathbf{x}) &= \mathbf{x}^T \hat{\boldsymbol{\beta}} + (\chi^2_{2,\alpha} \mathbf{x}^T J^{-1} \mathbf{x})^{\frac{1}{2}}, \\ \lambda_L(\mathbf{x}) &= \mathbf{x}^T \hat{\boldsymbol{\beta}} - (\chi^2_{2,\alpha} \mathbf{x}^T J^{-1} \mathbf{x})^{\frac{1}{2}}, \end{aligned}$$

where  $\mathbf{x} = (1, x)^T$  and  $\hat{\boldsymbol{\beta}} = (\hat{\beta}_0, \hat{\beta}_1)^T$ .

Then the confidence band for the probability of the dose-response with  $100(1-\alpha)\%$  confidence level is given by

$$\left(\frac{\exp[\lambda_L(x)]}{1+\exp[\lambda_L(x)]}, \frac{\exp[\lambda_H(x)]}{1+\exp[\lambda_H(x)]}\right) \quad \text{for all } x.$$
(6.7)

#### 6.1.2 For a multiple logistic regression

Hauck (1983) considered the construction of simultaneous confidence bands for the logistic response function with any number of predictor variables. He presented a computationally easier and more general method than that in Brand, Pinnock and Jackson (1973).

Let y be a dichotomous response with possible values 1 or 0. The probability of y = 1 denoted by  $\pi(\mathbf{x})$ , which is in terms of the predictor vector  $\mathbf{x} = (x_1, \ldots, x_p)^T$ , is given by

$$\pi(\mathbf{x}) = \frac{\exp(\mathbf{x}^T \boldsymbol{\beta})}{1 + \exp(\mathbf{x}^T \boldsymbol{\beta})},\tag{6.8}$$

where  $\boldsymbol{\beta} = (\beta_0, \beta_1, \dots, \beta_p)^T$  is the vector of the regression coefficients. Alternatively, (6.8) can be transformed as

$$\lambda(\mathbf{x}) = \mathbf{x}^T \boldsymbol{\beta} = \ln\left(\frac{\pi(\mathbf{x})}{1 - \pi(\mathbf{x})}\right)$$

Now, we assume observations **x** and *y* are of sample size *N*, which is large enough for the asymptotic normality of the maximum likelihood estimator vector  $\hat{\beta}$  to be a good approximation, i.e.,

$$\sqrt{N}(\hat{\boldsymbol{\beta}} - \boldsymbol{\beta}) \xrightarrow{\mathcal{D}} N_{p+1}(\boldsymbol{0}, \boldsymbol{\Sigma}), \tag{6.9}$$

where  $\Sigma/N$  can be estimated by  $J^{-1}$  with J being the information matrix of  $\hat{\beta}$ , which has the elements given by

$$J_{jk} = \sum_{i}^{N} \hat{\pi}(\mathbf{x}_{i})[1 - \hat{\pi}(\mathbf{x}_{i})]x_{ij}x_{ik}$$
  
= 
$$\sum_{i}^{N} \{\exp(\mathbf{x}^{T}\hat{\boldsymbol{\beta}})/[1 + \exp(\mathbf{x}^{T}\hat{\boldsymbol{\beta}})]^{2}\}x_{ij}x_{ik}, \qquad (6.10)$$

 $i = 1, \ldots, N; j, k = 1, \ldots, p$ . We subsequently have

$$(\hat{\boldsymbol{\beta}} - \boldsymbol{\beta})^T J(\hat{\boldsymbol{\beta}} - \boldsymbol{\beta}) \xrightarrow{\mathcal{D}} \chi^2_{p+1},$$

where J can be obtained from most statistical package directly. Let  $\chi^2_{p+1,\alpha}$  denotes the upper  $\alpha$  percentage point of the  $\chi^2_{p+1}$  distribution, then

$$\mathbb{P}\{(\hat{\boldsymbol{\beta}}-\boldsymbol{\beta})^T J(\hat{\boldsymbol{\beta}}-\boldsymbol{\beta}) \le \chi^2_{p+1,\alpha}\} \approx 1-\alpha.$$
(6.11)
An approximate  $1 - \alpha$  confidence set for  $\beta$  is therefore given by

$$(\hat{\boldsymbol{\beta}} - \boldsymbol{\beta})^T J(\hat{\boldsymbol{\beta}} - \boldsymbol{\beta}) \le \chi^2_{p+1,\alpha}, \tag{6.12}$$

which is an ellipsoidal region centered at  $\hat{\beta}$ .

Recall the Cauchy-Schwartz inequality which is of the form given by

$$|\mathbf{a}^T \mathbf{b}|^2 \le ||\mathbf{a}||^2 \cdot ||\mathbf{b}||^2$$

for all vectors  $\mathbf{a}$  and  $\mathbf{b}$  in the inner product space. Applying the Cauchy-Schwartz inequality, we have for all  $\mathbf{x}$ ,

$$\begin{aligned} [\mathbf{x}^{T}(\hat{\boldsymbol{\beta}}-\boldsymbol{\beta})]^{2} &= |\mathbf{x}^{T}J^{-\frac{1}{2}}J^{\frac{1}{2}}(\hat{\boldsymbol{\beta}}-\boldsymbol{\beta})|^{2} \\ &= |[(J^{-\frac{1}{2}})^{T}\mathbf{x}]^{T}[J^{\frac{1}{2}}(\hat{\boldsymbol{\beta}}-\boldsymbol{\beta})]|^{2} \\ &\leq ||(J^{-\frac{1}{2}})^{T}\mathbf{x}||^{2} \cdot ||J^{\frac{1}{2}}(\hat{\boldsymbol{\beta}}-\boldsymbol{\beta})||^{2} \\ &= [(J^{-\frac{1}{2}})^{T}\mathbf{x}]^{T}[(J^{-\frac{1}{2}})^{T}\mathbf{x}] \cdot [J^{\frac{1}{2}}(\hat{\boldsymbol{\beta}}-\boldsymbol{\beta})]^{T}[J^{\frac{1}{2}}(\hat{\boldsymbol{\beta}}-\boldsymbol{\beta})] \\ &= (\mathbf{x}^{T}J^{-1}\mathbf{x})[(\hat{\boldsymbol{\beta}}-\boldsymbol{\beta})^{T}J(\hat{\boldsymbol{\beta}}-\boldsymbol{\beta})]. \end{aligned}$$
(6.13)

Substitute (6.13) into (6.11) to obtain

$$1 - \alpha \approx P\{[\mathbf{x}^{T}(\hat{\boldsymbol{\beta}} - \boldsymbol{\beta})]^{2} / [\mathbf{x}^{T} J^{-1} \mathbf{x}] \leq \chi^{2}_{p+1,\alpha}, \text{ for all } \mathbf{x}\}$$
  
$$= P\{|\mathbf{x}^{T}(\hat{\boldsymbol{\beta}} - \boldsymbol{\beta})| \leq (\chi^{2}_{p+1,\alpha} \mathbf{x}^{T} J^{-1} \mathbf{x})^{\frac{1}{2}}, \text{ for all } \mathbf{x}\}$$
  
$$= P\{\mathbf{x}^{T} \boldsymbol{\beta} \leq \mathbf{x}^{T} \hat{\boldsymbol{\beta}} \pm (\chi^{2}_{p+1,\alpha} \mathbf{x}^{T} J^{-1} \mathbf{x})^{\frac{1}{2}}, \text{ for all } \mathbf{x}\}.$$
 (6.14)

Therefore a  $1 - \alpha$  level confidence band for  $\mathbf{x}^T \boldsymbol{\beta}$  is given by

$$\left(\lambda_L(\mathbf{x}), \lambda_U(\mathbf{x})\right) = \left(\mathbf{x}^T \hat{\boldsymbol{\beta}} - (\chi_{p+1,\alpha}^2 \mathbf{x}^T J^{-1} \mathbf{x})^{\frac{1}{2}}, \mathbf{x}^T \hat{\boldsymbol{\beta}} + (\chi_{p+1,\alpha}^2 \mathbf{x}^T J^{-1} \mathbf{x})^{\frac{1}{2}}\right)$$
(6.15)

for all **x**. By making use of the logistic relationship, the corresponding confidence band for  $\pi(\mathbf{x})$  is given by

$$\left(\frac{\exp[\lambda_L(\mathbf{x})]}{1+\exp[\lambda_L(\mathbf{x})]}, \frac{\exp[\lambda_U(\mathbf{x})]}{1+\exp[\lambda_U(\mathbf{x})]}\right) \text{ for all } \mathbf{x}.$$
(6.16)

## 6.2 Confidence bands for a logistic regression with restricted predictor variables

In real problems, some constraints may be imposed on the predictor variables. In this case, a confidence band is restricted to some subset of possible x's. Therefore, the bands described in section 6.1 are unnecessarily wide and conservative. Naturally, it is of great interest to consider methods of constructing confidence bands for a logistic regression with restricted predictor variables. In this section, we focus on this problem. The restricted predictor space considered is the most popular rectangular region, which has the form

$$\mathcal{X} = \{ \mathbf{x} = (x_1, \dots, x_p), a_i \le x_i \le b_i, i = 1, \dots, p \},$$
(6.17)

where  $a_i, b_i$ 's are given real constants.

### 6.2.1 For a simple logistic regression

#### Band based on the method of Wynn and Bloomfield (1971)

For simple logistic regression, we have the asymptotic property that  $\hat{\beta}$  is approximately normally distributed with mean  $\beta$  and estimated covariance matrix  $J^{-1}$  when the sample size N is sufficiently large. Then a confidence band can be constructed for  $\mathbf{x}^T \boldsymbol{\beta}$  of the form

$$\mathbf{x}^{T}\boldsymbol{\beta} \in \mathbf{x}^{T}\hat{\boldsymbol{\beta}} \pm c\sqrt{\mathbf{x}^{T}J^{-1}\mathbf{x}^{T}} \text{ all } x \in [a, b],$$
 (6.18)

which can be written alternatively as

$$\sup_{x \in [a,b]} \frac{|\mathbf{x}^T(\hat{\boldsymbol{\beta}} - \boldsymbol{\beta})|}{\sqrt{\mathbf{x}^T J^{-1} \mathbf{x}}} \le c,$$
(6.19)

where x is the only predictor variable which is restricted in the interval [a, b], c is the critical value such that the band has the simultaneous coverage probability of  $1 - \alpha$ .



Figure 6.1: For Wynn and Bloomfield's method

Assume that there is a  $2 \times 2$  non-singular matrix P such that  $P^T P = J^{-1}$ . Then (6.19) can be further written as

$$\sup_{\mathbf{x}\in[a,b]} \frac{|(P\mathbf{x})^T (P^{-1})^T (\hat{\boldsymbol{\beta}} - \boldsymbol{\beta})|}{\sqrt{(P\mathbf{x})^T (P\mathbf{x})}} = \sup_{\mathbf{x}\in[a,b]} \frac{|(P\mathbf{x})^T \mathbf{N}|}{\|(P\mathbf{x})\|} \le c,$$
(6.20)

where  $\mathbf{N} = (P^{-1})^T (\hat{\boldsymbol{\beta}} - \boldsymbol{\beta})$  has a bivariate standard normal distribution, and so  $\|\mathbf{N}\|^2$  has the  $\chi_2^2$  distribution.

Now, we turn to evaluate the probability of the event in (6.20) so as to find a computational formula for calculation of the critical value c. Define  $\mathbf{a} = (1, a)^T$ ,  $\mathbf{b} = (1, b)^T$ , and  $\theta^*$  is half the angle between  $P\mathbf{a}$  and  $P\mathbf{b}$ . Figure 6.1 may be useful to easily calculate the last supreme in (6.20).  $P\mathbf{x}$  is a vector moving within the circular cone bounded by  $P\mathbf{a}$  and  $P\mathbf{b}$ , whereas N is a vector that can freely locate at any position in the plane. When N is within the circular cone or its opposite, the supreme is equal to  $||\mathbf{N}||$ ; otherwise it equals the the projection of N on the nearest bound of the cones.

Assume  $\theta$  is the angle between the positive horizontal axis and N. As the picture is symmetric, it is only needed to consider the part for  $\theta \in [0, \pi/2]$ .

We have

$$\sup_{x \in [a,b]} \frac{|(P\mathbf{x})^T \mathbf{N}|}{\|P\mathbf{x}\|} = \begin{cases} \|\mathbf{N}\| & \text{for } \theta \in [0, \theta^*], \\ \|\mathbf{N}\| \cos(\theta - \theta^*) & \text{for } \theta \in (\theta^*, \frac{\pi}{2}]. \end{cases}$$

The probability of the confidence band (6.18) is therefore equal to

$$P\left\{\sup_{x\in[a,b]}\frac{|(P\mathbf{x})^{T}\mathbf{N}|}{||P\mathbf{x}||} \le c\right\}$$

$$= 4\left(P\{\|\mathbf{N}\| \le c, 0 \le \theta \le \theta^{*}\}\right)$$

$$+P\{\|\mathbf{N}\| \cos(\theta - \theta^{*}) \le c, \theta^{*} < \theta \le \frac{\pi}{2}\}\right)$$

$$= 4\left(\frac{\theta^{*}}{2\pi}\chi_{2}^{2}(c^{2}) + \frac{1}{2\pi}\int_{\theta^{*}}^{\frac{\pi}{2}}\chi_{2}^{2}\left(\frac{c^{2}}{\cos^{2}(\theta - \theta^{*})}\right)d\theta\right)$$

$$= \frac{2\theta^{*}}{\pi}\chi_{2}^{2}(c^{2}) + \frac{2}{\pi}\int_{0}^{\frac{\pi}{2} - \theta^{*}}\chi_{2}^{2}\left(\frac{c^{2}}{\cos^{2}\theta}\right)d\theta, \qquad (6.21)$$

where  $\theta^*$  can be calculated via the following formula

$$\theta^* = \frac{1}{2} \arccos\left(\frac{\mathbf{a}^T J^{-1} \mathbf{b}}{(\mathbf{a}^T J^{-1} \mathbf{a} \cdot \mathbf{b}^T J^{-1} \mathbf{b})^{1/2}}\right),\tag{6.22}$$

where J can be obtained directly from most statistical packages.

Consequently, given a confidence level, critical value c can be calculated from (6.21) and (6.22), which is used to construct confidence band (6.18) for  $\mathbf{x}^T \boldsymbol{\beta}$ . Hence, a confidence band can be obtained for the logistic response  $\pi(x)$ by making use of the logistic relationship. This method is from Wynn and Bloomfield (1971), so we call the band of this method WB band hereafter.

### Type 4 band of Sun, Loader and McCormick (2000)

Sun, Loader and McCormick (2000) considered confidence bands for generalized linear models. In their paper, it is stated that the approximation to the coverage probability of simultaneous confidence bands for the mean response function in linear models is still applicable without any change to the generalized linear models. However, in generalized linear models, the errors are often non-additive and non-normal. This may influence the accuracy of the approximation when the sample size is not large enough. Under this situation, they proposed to use an Edgeworth expansion for the distribution of  $\hat{\beta}$ in connection with the idea of the Skorohod construction to convert an error term in the Edgeworth expansion to a bias term; then estimate and correct it to adjust the approximation formula such that the coverage probability of the corrected confidence band is much closer to the nominal confidence level. The correction proposed in the paper has two components: one is to apply the tube formula to some modified process; the other uses the method of bias correction in Sun and loader (1994).

For simplicity, only one-dimensional case was studied in Sun, Loader and McCormick (2000) but their method may be applied to cases of multiple dimension. They recommended their Type 4 confidence band which is given by

$$\mathbf{x}^T \hat{\boldsymbol{\beta}} \pm (c - |\hat{r}_p|) (\mathbf{x}^T J^{-1} \mathbf{x})^{\frac{1}{2}}$$
 for all  $x \in [a, b],$  (6.23)

where c and  $\hat{r}_p$  are a critical value and a corrected constant respectively. Their other types of bands are proven not to perform as well as Type 4 band for the logistic regression model when the sample size  $N \geq 200$ . Note that  $(c - |\hat{r}_p|)$  in (6.23) as a whole can be obtained directly by using their software parfit, which can be downloaded from www.locfit.info/.

Note that the band in (6.23) is for  $\mathbf{x}^T \boldsymbol{\beta}$ . The band for the logistic response  $\pi(x)$  can be obtained from the band (6.23) in the usual way.

#### A numerical example

Consider the example of Anti-pneumococcus serum in Collett (2003, pages 6-7). This example is based on the assay taken from Smith (1932), who described a study of the protective effect of a particular serum, 'Serum number 32', on pneumococcus, the bacterium associated with the occurrence of pneumonia. Each of 40 mice was injected with a combination of an infecting dose of a culture of pneumococci and one of five doses of the anti-pneumococcus serum. For all mice that died during the seven-day period following inoculation, a blood smear taken from the heart was examined to determine

Dose of serum	Number of deaths out of 40
0.0028	35
0.0056	21
0.0112	9
0.0225	6
0.0450	

Table 6.1: Number of deaths to different doses of serum

whether pneumococci were present or absent. Mice that still lived on the seventh day were regarded as survivors and not further examined. The dichotomous response variable is therefore death from pneumonia within seven days of inoculation. The numbers of mice succumbing to infection out of 40 exposed to each of five doses of the serum, measured in cc, are given in Table 6.1.

Obviously, a simple logistic regression model is used to fit the data in order to find the relationship between the probability of deaths and dose of serum. A simultaneous confidence band can be constructed. Here we choose [0, 0.0450] as the restricted interval for the dose of serum.

With the same notations as before, we have

$$\hat{\beta}_0 = 1.2179, \quad \hat{\beta}_1 = -146.6927,$$
  
$$J^{-1} = \begin{pmatrix} 0.0858 & -6.1499 \\ -6.1499 & 695.0059 \end{pmatrix}$$

Also, we have the critical values 2.4304 for a WB band and 2.3700 for a Type 4 band respectively at 95% confidence level. Therefore, two simultaneous confidence bands for the probability of deaths can be constructed accordingly. Both bands are given in Figure 6.2.

### 6.2.2 For a multiple logistic regression

#### Method of Piegorsch and Casella (1988)

Piegorsch and Casella (1988) proposed a method of constructing confidence bands for a multiple logistic regression with predictor variables restricted in a rectangular region given by (6.17).



Figure 6.2: 95%-level confidence bands for probability of deaths

The key idea is to embed the rectangular region (6.17) into an ellipsoidal restricted region of predictor variables described in Casella and Strawderman (1980), and then to apply Casella and Strawderman (1980)'s Table 1 to obtain a conservative critical value. In particular, the ellipsoidal region is centered at the means of the predictor variables. If the rectangular region is not centered at the mean point, the critical value obtained from Casella and Strawderman (1980)'s results can be extremely conservative.

Consider, for example, the quantal data in Table 1 of Piegorsch and Casella (1988). Table 5 gives values of  $c^2$  for 95% confidence level based on their method. Note that this is a one-dimensional example, and all three restricted intervals in Table 5 are asymmetric about the mean of the only predictor variable, which is 1.4862. We used the method of Wynn and Bloom-field (1971) to calculate the critical values for the confidence bands with these three restricted intervals respectively and then compare the squared values of them with those of Piegorsch and Casella (1988). All the values are given in Table 6.2.

Restricted interval	C <sup>2</sup>	C_wb2
[-1.3, 2.0]	5.98	5.4943
[-1.3. 0.8]	5.17	4.8638
[-13 -0.2]	471	4 2737

Table 6.2: Squared critical values for 95% confidence level

From the table, the squared critical values based on the method of Piegorsch and Casella (1988) are, respectively, 8.8%, 6.3% and 10.2% larger than those based on the method of Wynn and Bloomfield (1971). Consequently, the method of Piegorsch and Casella (1988) is not considered further in this chapter.

#### Simulation-based method

Liu, Jamshidian, Zhang and Donnelly (2005) construct simultaneous confidence bands for a multiple linear regression over a rectangular restricted predictor space based on simulation. We apply the method to the logistic regression case.

For a logistic regression with at least one predictor variables,  $\hat{\beta}$  is approximately normally distributed with mean  $\beta$  and estimated asymptotic covariance matrix  $J^{-1}$ . Then the coverage probability of a confidence band for  $\mathbf{x}^T \boldsymbol{\beta}$  over  $\mathbf{x} \in \mathcal{X}$  is given by  $P\{T \leq c\}$ , where

$$T = \sup_{\mathbf{x}\in\mathcal{X}} \frac{|\mathbf{x}^T(\hat{\boldsymbol{\beta}} - \boldsymbol{\beta})|}{\sqrt{\mathbf{x}^T J^{-1} \mathbf{x}}},$$
(6.24)

c is a critical value, and  $\mathcal{X}$  is a rectangular region of the form given by (6.17). Assume there is a  $p \times p$  non-singular matrix P such that  $P^T P = J^{-1}$ . Then (6.24) can be further written as

$$T = \sup_{\mathbf{x}\in\mathcal{X}} \frac{|(P\mathbf{x})^T (P^{-1})^T (\hat{\boldsymbol{\beta}} - \boldsymbol{\beta})|}{\sqrt{(P\mathbf{x})^T (P\mathbf{x})}}$$
$$= \sup_{\mathbf{x}\in\mathcal{X}} \frac{|(P\mathbf{x})^T \mathbf{N}|}{\|P\mathbf{x}\|},$$
(6.25)

where  $\mathbf{N} = (P^{-1})^T (\hat{\boldsymbol{\beta}} - \boldsymbol{\beta})$  has a multivariate standard normal distribution.

The key of the simulation-based method is to generate an N so as to find a T via (6.25); repeat this process R times, and set the  $[(1 - \alpha)R]$ th largest value of T,  $\hat{c}$ , as an approximate of the critical value c. For each simulation, Tis obtained by solving an optimization problem. Details can be found in Liu, Jamshidian, Zhang and Donnelly (2005). After  $\hat{c}$  is obtained, a confidence band can be constructed for the logistic response as before.

#### A numerical example

This is another example from Collett (2003, pages 8-9). The erythrocyte sedimentation rate (ESR) is the rate at which red blood cells (erythrocytes) settle out of suspension in blood plasma, when measured under standard conditions. The ESR increases if the level of certain proteins in the blood plasma rise, such as in rheumatic diseases, chronic infections and malignant diseases; this makes the determination of the ESR one of the most commonly used screening tests performed on samples of blood. One aspect of a study carried out by the Institute of Medical Research, Kuala Lumpur, Malaysia, was to examine the extent to which the ESR is related to two plasma proteins, fibrinogen and  $\gamma$ -globulin, both measured in gm/l, for a sample of 32 individuals. The ESR for a 'healthy' individual should be less than 20 mm/hr and since the absolute value of the ESR is relatively unimportant, the response variable used here will denote whether this is the case. A response of zero will signify a healthy individual (ESR < 20), while a response of unity will refer to an unhealthy individual (ESR $\geq 20$ ). The original data were presented in Collett and Jemain (1985) and are relisted in Table 6.3.

In this case, a bivariate logistic regression model is applied to obtain the relationship between the probability of an ESR reading greater than 20 mm/hr and the levels of two plasma proteins. When construct a simultaneous confidence band, we set an restricted interval for each predictor variable formed by the smallest and largest values of the observations. Specifically, they are [2.09, 5.06] and [28, 46] for Fibrinogen and  $\gamma$ -globulin respectively.

Individual	Fibrinogen	r-globulin	Response
1	2.52	38	0
2	2.56	31	0
3	2.19	33	0
4	2.18	31	0
5	3.41	37	0
6	2 46	36	0
7	3.22	38	0
8	2.21	37	0
9	3.15	39	0
10	2.60	41	O
11	2.29	36	0
12	2.35	29	0
13	5.06	37	1
14	3.34	32	1
15	2.38	37	1
16	3.15	36	0
17	3.53	46	1
18	2.68	34	0
19	2.60	38	Ö
20	2.23	37	0
21	2.88	30	0
22	2.65	46	0
23	2.09	44	1
24	2.28	36	0
25	2.67	39	0
26	2.29	31	0
27	2.15	31	0
28	2.54	28	0
29	3.93	32	1
30	3.34	30	0
31	2.99	36	0
32	3.32	35	• 0

Table 6.3: The levels of two plasma proteins and the value of a binary response that denotes whether  $ESR \ge 20$  for each individual



Figure 6.3: 90%-level confidence band for probability of that ESR larger than 20

With the same notations as before, we have

$$\hat{\boldsymbol{\beta}} = \begin{pmatrix} -12.7921 \\ 1.9104 \\ 0.1558 \end{pmatrix} \text{ and } J^{-1} = \begin{pmatrix} 33.5985 & -3.6718 & -0.5987 \\ -3.6718 & 0.9428 & 0.0224 \\ -0.5987 & 0.0224 & 0.0143 \end{pmatrix}.$$

Also, we have the critical values 2.1291 and 2.4118 based on the simulation method of 100,000 simulations for 90% and 95% confidence level respectively. Two simultaneous confidence bands can be constructed then. They are plotted in Figures 6.3 and 6.4.

### 6.3 Simulations

All these methods of constructing simultaneous confidence bands for a logistic regression is based on the large sample asymptotic normality of  $\hat{\beta}$ . So the bands constructed have an approximate  $1 - \alpha$  confidence level. It is therefore of interest to simulate the coverage probabilities of the bands to check how close they are to the nominal level, and what factors affect the accuracy.



Figure 6.4: 95%-level confidence band for probability of that ESR larger than 20

We have carried out simulation studies for the one-dimensional and twodimensional cases, respectively.

### 6.3.1 For one-dimensional case

In this subsection, we compare the confidence band based on the method of Wynn and Bloomfield (1971) with the Type 4 band recommended in Sun, Loader and McCormick (2000). We call them WB band and Type 4 band for simplicity.

With consistent notations, the specific procedure is as follow:

Step 1 Given a set of m values of the only predictor variable  $x, x_1, \ldots, x_m$ , together with a pair of true regression coefficients  $\beta_0$  and  $\beta_1$ , we obtain the probabilities of the logistic response based on the true model via

$$\pi(x_i) = \frac{\exp(\beta_0 + \beta_1 x_i)}{1 + \exp(\beta_0 + \beta_1 x_i)}, i = 1, \dots, m.$$
(6.26)

- Step 2 Generate the logistic response  $y_i$ , corresponding to  $x_i$ , which has a binomial distribution with parameters  $\pi(x_i)$  and  $n_i$ , where  $n_i$  is the sub-sample size.
- Step 3 Estimate  $\beta_0$  and  $\beta_1$  based on  $(x_i, y_i, n_i), i = 1, \ldots, m$  to obtain  $\hat{\beta}_0$ and  $\hat{\beta}_1$ , then calculate  $J^{-1}$  accordingly.
- Step 4 Construct a simultaneous confidence band. WB band is of the form

$$\hat{\beta}_0 + \hat{\beta}_1 x \pm c_1 \sqrt{(1, x) J^{-1}(1, x)^T} \quad x \in [a, b],$$
(6.27)

where  $c_1$  can be calculated using (6.21) and (6.22) for a given nominal confidence level cl. Type 4 band is of the form

$$\hat{\beta}_0 + \hat{\beta}_1 x \pm (c_2 - |\hat{r}_p|) \sqrt{(1, x) J^{-1}(1, x)^T} \quad x \in [a, b],$$
(6.28)

where  $(c_2 - |\hat{r}_p|)$  as a whole can be obtained directly by using the software parfit mentioned in Sun, Loader and McCormick (2000).

Step 5 Check whether the true function  $\beta_0 + \beta_1 x$  is completely in the band for all x's within the restricted interval [a, b].

We repeat Step 1 to Step 5 nsim times. Out of the nsim simulations, the proportion of times that the confidence band includes the true regression model is taken as an approximation of the true coverage probability. It is clear that this simulated coverage probability depends on  $x_i, n_i, \beta_0, \beta_1, [a, b], cl, nsim, \dots$  $i = 1, \dots, m$ .

Now, we turn to the design of these common factors so that various combinations can be obtained to make the comparison as general as possible. First, we choose five design points for the only predictor variable, that is m = 5, which seems reasonable in real problems. Furthermore, we choose four different types of five design points on the design interval [-1, 1]. The first type of design is to set the design points equally spaced throughout the interval [-1, 1]. The second type corresponds to the design points near the center of the design interval. The third type corresponds to the design

Structure	Design points	Restricted interval	Θ*
P1	[-1, -0.5, 0, 0.5, 1]	[-0.5, 0.5]	0.6155
P2	Equally-spaced	[-2, 2]	1.2310
P3	[-0.08, -0.05, 0.02, 0.04, 0.09]	[-0.5, 0.5]	1.4484
P4	Centred	[-2, 2]	1.5400
P5	[0.89, 0.92, 0.95, 0.98, 1]	[-0.5. 0.5]	0.0305
P6	One-ended	[-2, 2]	1.5452
P7	[-1, -0.91, 0.94, 0.98, 1]	[-0.5, 0.5]	0.4721
P8	Two-ended	[-2, 2]	1.1260

Table 6.4: Designs for predictor variable and restricted interval

Structure	Sample size	Total
N1	[10, 10, 10, 10, 10]	N = 50
N2	[22, 35, 58, 46, 39]	N = 200

Table 6.5: Design for total sample size

points concentrated around the upper bound of the design interval. And the last type corresponds to the design points located at the two ends of the interval [-1, 1]. Second, two restricted intervals are chosen, one of which is short and the other is long. These choices of the design points and the restricted intervals provide various values of the angle  $\theta^*$  in (6.21) to give various critical values. In fact, based on our designs, values of  $\theta^*$  varies in the range  $[0, \pi]$  from small (0.0305) to large (1.5452). Third, we choose two sample sizes  $N = \sum_{i=1}^{5} n_i$  of 50 and 200 to check its effect on the simulated coverage probability. Finally, we choose eight pairs of  $\beta_0$  and  $\beta_1$  so that the straight line  $\beta_0 + \beta_1 x$  has various slopes and intercepts. The designs are contained in Tables 6.4-6.6.

Structure	β0	β1
Q1	0.75	0.5
Q2	2.55	1.7
Q3	-0.39	-0.26
Q4	-1.5	-1
Q5	-0.75	0.5
Q6	-2.55	1.7
Q7	0.39	-0.26
Q8	1.5	-1

Table 6.6: Designs for true regression coefficients

The simulated coverage probabilities of WB bands are calculated by the programmes running on MATLAB 7 platform, while those of Type 4 bands are obtained by using parfit on S-plus 6.2 platform. As it is not clear how to change the default confidence level 95% in parfit, confidence level 95% is used in our comparison. To reduce the simulation error, we set *nsim* equal to 10,000. Based on the above designs, simulated coverage probabilities are obtained and listed in Tables 6.7-6.10. Note that, in some cases, the simulated coverage probability can not be worked out. If this is the case for both bands based on the same designs, it is because the maximum likelihood estimates of  $(\beta_0, \beta_1)$  can not be found within the pre-specified 30 iterations. The case that only Type 4 band can not find the simulated coverage probability is due to the fact that the corrected critical value  $(c - |\hat{r}_p|)$  can not be found using parfit. In this case, a sentence "warning: comparcomp: perfect fit" was displayed.

From the results, some conclusions can be drawn. First, the simulated coverage probabilities of both bands are often larger than 95%. Second, when the sample size N = 50, both bands can be quite conservative with the simulated coverage probabilities being around 97%. When N = 200, the simulated coverage probabilities of WB bands are very close to 95% except few cases, whereas Type 4 bands may still be quite conservative or liberal. Third, the corrected critical value of Type 4 band may not be found for small sample size.

Also, it is motivated to compare the widths of the WB bands and Type 4 bands. Note that there are 128 design structures in our comparison, such as P1,N1,Q1 and P5,N2,Q8. For each design structure, we calculate 100 simulated critical values for each band. Therefore, we have totally 12,800 critical values for each band. Ignore the cases that one or both bands can not find the critical value. The left 10,476 cases are viewed as being valid. Then it is found that the proportion of the cases that the critical value of WB band is smaller than that of Type 4 band, out of the valid cases, is 68.36%.

Consequently, WB band seems to be better than Type 4 band generally,

Structure		scp wb	scp_t4	
the second s		Q1	0.9702	0.9652
		Q2	Na	Na
	the second	Q3	0.9730	0.9706
	N1	Q4	0.9539	0.9417
1 4 A		Q5	0.9720	0.9652
		Q6	Na	Na
	1	Q7	0.9729	0.9715
P1		Q8	0.9529	0.9409
		Q1	0.9510	0.9582
		Q2	0.9431	0.9412
	1.1	Q3	0.9529	0.9575
	N2	Q4	0.9568	0.9587
		Q5	0.9521	0.9570
		Q6	0.9238	0.9320
		Q7	0.9497	0.9569
		Q8	0.9511	0.9559
100		Q1	0.9728	0.9832
		Q2	Na	Na
	1 1 1 1	Q3	0_9684	0.9801
	N1	Q4	0.9575	0.9672
	1.1.2	Q5	0.9744	0.9807
		Q6	Na	Na
		Q7	0.9681	0.9805
P2		08	0.9612	0.9685
		Q1	0.9484	0.9615
	12.22	Q2	0.9446	0.9537
		Q3	0.9523	0.9648
	N2	Q4	0.9558	0.9673
		Q5	0.9510	0.9672
		Q6	0.9358	0.9536
	1.0.021	Q7	0.9533	0.9663
		Q8	0.9588	0.9683

Table 6.7: Simulated coverage probabilities for 95% confidence level

especially when the total sample size is large.

Structure		scp_wb	scp_t4	
9-11-11-11-11-11-11-11-11-11-11-11-11-11		Q1	0 9730	Na
		Q2	Na	Na
	1. 1. 1. 1. 1.	Q3	0.9696	Na
	N1	Q4	0.9879	Na
		Q5	0.9717	Na
		Q6	Na	Na
	100	Q7	0.9703	Na
P3		Q8	0.9878	Na
		Qĩ	0.9490	0.9666
	all second	Q2	0.9753	0.9782
		Q3	0.9470	Na
	N2	Q4	0.9565	0.9702
		Q5	0.9516	0.9666
	-	Q6 ·	0.9659	0.9735
	1- 1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-	Q7	0.9518	0.9695
		Q8	0.9620	0.9722
		Q1	0.9739	Na
		Q2	Na	Na
		Q3	0.9648	Na
	N1	Q4	0.9833	Na
		Q5	0.9736	Na
		Q6	Na	Na
		Q7	0.9638	Na
P4		Q8	0.9889	Na
		Q1	0.9492	0.9675
	1	Q2	0.9686	0.9803
		Q3	0.9582	Na
	N2	Q4	0.9515	0.9732
		Q5	0.9501	0.9698
		Q6	0.9630	0.9787
		Q7	0.9523	0.9703
		Q8	0.9551	0.9733

Table 6.8: Simulated coverage probabilities for 95% confidence level

150

Structure		scp_wb	scp_t4	
		Q1	0.9859	Na
	1.00	Q2	Na	Na
		Q3	0.9744	0.9343
	N1	Q4	Na	Na
		Q5	0.9628	Na
		Q6	0.9784	Na
10.00		Q7	0.9633	Na
P5		08	0.9665	Na
		Q1	0.9532	0.9369
		Q2	Na	Na
	1.124	Q3	0.9466	0:9245
	N2	Q4	0.9688	0.9588
		Q5	0.9489	0.9292
		QG	0.9550	0.9344
	1 - 2 - 2	Q7	0.9490	0.9305
		Q8	0.9504	0.9259
	Q1	0.9827	Na	
		Q2	Na	Na
		Q3	0.9677	0.9809
	N1	Q4	Na	Na
		Q5	0.9652	Na
		Q6	0.9743	Na
		Q7	0.9641	Na
P6		Q8	0.9705	Na
	Contraction of the second	Q1	0.9519	0.9689
		Q2	Na	Na
		Q3	0.9523	0.9718
	N2	Q4	0.9660	0.9798
	E LA POLI	Q5	0.9490	0.9702
		Q6	0.9536	0.9699
		Q7	0.9493	0.9688
		Q8	0.9502	0.9709

Table 6.9: Simulated coverage probabilities for 95% confidence level

Structure		scp_wb	scp_t4	
		Q1	0 9699	0.9646
1013		Q2	Na	Na
1	1. A.	Q3	0.9688	0.9651
	N1	Q4	0.9443	0.9341
		Q5	0.9678	0.9561
		Q6	0.8803	Na
		07	0.9751	0.9620
P7	1 - L	Q8	0.9574	0.9205
		Q1	0.9539	0.9548
		Q2	0.9129	0.8814
		Q3	0.9542	0.9542
	N2	Q4	0.9584	0.9557
		Q5	0.9569	Na
		Q6	0.9150	0.8630
	12000	Q7	0.9542	0.9540
100	1.1	Q8	0.9589	0.9492
		Q1	0.9693	0.9712
		Q2	Na	Na
		Q3	0.9683	0.9726
, <del>-</del>	N1	Q4	0.9464	0.9345
		Q5	0.9701	0.9662
		Q6	0.9027	Na
		Q7	0.9707	0.9739
P8		Q8	0.9566	0.9325
		. Q1	0.9551	0.9680
		02	0.9344	0.9309
100		Q3	0.9539	0.9702
1.6.1	N2	Q4	0.9579	0.9571
		Q5	0.9597	Na
1		Q6	0.9318	0.9256
1.1.1.1		Q7	0.9501	0.9652
	1.7.14	Q8	0.9569	0.9653

Table 6.10: Simulated coverage probabilities for 95% confidence level

152

Structure	Design poinits	Types
P1	x1=[0.35, 0.39, 0.48, 0.52, 0.57, 0.61]	Centred
Gentred	x2=[0.37, 0.41, 0.5, 0.53, 0.56, 0.58]	Centred
P2	x1=[0.85, 0.88, 0.92, 0.94, 0.98, 1]	Right-ended
One-comerad	x2=[0.03. 0.07. 0.11. 0.14. 0.16. 0.19]	Left-ended
P3	x1=[0.05, 0.08, 0.1, 0.92, 0.95, 0.98]	Two-ended
Two-comered	x2=[0.02, 0.04, 0.07, 0.91, 0.96, 0.99]	Two-ended
P4	x1=[0.2, 0.4, 0.7, 0.5, 0.8, 0.9]	Non-equally-spaced
Dispersed	x2=[0 15, 0.3, 0.45, 0.6, 0.75, 0.9]	Equally-spaced

Table 6.11: Design points for two predictor variables

Structure	Restricted intervals	Туре
R1	[0, 2] . [0, 2]	Long - Long
R2	10.5 1] . [0.5. 1]	Short - Short
R3	[0.5. 1] . [0. 2]	Short - Long

Table 6.12: Designs for restricted intervals of predictor variables

### 6.3.2 For two-dimensional case

For the two-dimensional case, we find the simulated coverage probabilities of the confidence bands constructed based on the simulation method of Liu, Jamshidian, Zhang and Donnelly (2005), and compare the results with the nominal confidence level.

The procedure is very similar to that in the one-dimensional case. The only difference is to change the number of predictor variables from 1 to 2 and the consequential changes to the regression coefficients, the restricted region, and the critical values.

Specifically, we choose four different designs P1,P2,P3,P4 in the predictor space, three pairs of restricted intervals R1,R2,R3, two levels of the total sample size N1,N2, and eight sets of the true regression coefficients Q1-Q8. Details are clearly shown in Tables 6.11-6.14.

Structure	Sample size	Total
111	[10, 10, 10, 10, 10, 10]	N = 60
N2	[16, 25, 29, 34, 46, 50]	N = 200

Table 6.13: Designs for total sample size

Structure	β0	β1	β2
Q1	-0.7	1.7	1.7
Q2	0.25	0.5	1
Q3	1.25	0.5	-1
Q4	1.5	-0.5	-0.5
Q5	-2.7	1.7	1.7
Q6	-1.75	0.5	1
Q7	-0.75	0.5	-1
O8	-0.5	-0.5	-0.5

Table 6.14: Designs for true regression coefficients

90% and 95% confidence levels are chosen in this simulation study. Note that this time when we construct confidence bands, the critical values come from the simulation-based method. We set the number of simulations equal to 5,000 for the calculation of the critical value, and the number of simulations equal to 10,000 for the calculation of the coverage probability. We consider this setting of the number of simulations as Type 1 setting. Alternatively, we may set 10,000 simulations for the critical value's calculation and 5,000 simulations for the coverage probability's calculation, which is considered as Type 2 setting. We have tried ten specific cases based on both settings, among which five are for the small sample size and the other five are for the large sample size. By comparing the resulting simulated coverage probabilities, it is found that the difference between the simulated coverage probabilities for the Type 1 and Type 2 settings is at the third decimal place for all ten chosen cases. So we reasonably believe that using either one may not influence our conclusions. Since it will take long time to do simulations for both settings, we just choose Type 1 setting here. Results are given in Tables 6.15-6.18.

From these results, it can be concluded that when N = 60 the confidence bands constructed based on the simulation method are much conservative with the simulated coverage probabilities generally larger than 93% for 90% confidence level and 97% for 95% level. When N = 200 the simulated coverage probabilities are pretty close to the nominal confidence levels, sometimes larger and sometimes smaller. Consequently, we reasonably believe this kind of confidence bands are good enough when N is large.

Structure combinations		scp		
		90%	95%	
		Q1	0.9404	0.9775
		02	0.9418	0.9798
		Q3	0.9395	0.9763
	N1	04	0.9428	0.9785
	1. A.	Q5	0.9454	0.9776
1. San 184	1	QS	0.9417	0.9780
1.5.5		Q7	0.9437	0.9785
P1. R1		Q8	0.9360	0.9804
		Q1	0.8945	0.9445
	5.54.1	Q2	0.9077	0.9525
		Q3	0.9033	0.9508
	N2	Q4	0.8956	0.9501
		Q5	0.9022	0.9554
		Q6	0.9021	0.9513
		Q7	0.8977	0.9485
	1. IS	Q8	0.8996	0.9476
	1981	Q1	0.9401	0.9766
1.1.1.1		Q2	0.9399	0.9763
		03	0.9455	0.9777
	N1	Q4	0.9460	0.9799
		Q5	0.9382	0.9757
		Q6	0.9409	0.9790
		Q7	0.9447	0.9794
P1, R2		QB	0.9420	0.9767
		Q1	0.8943	0.9456
		Q2	0.9057	0.9549
		Q3	0.9012	0.9456
- the	N2	Q4	0.9028	0.9525
	-	Q5	0.9138	0.9587
	19191	Q6	0.9034	0.9514
		Q7	0.8967	0.9519
	-	Q8	0.8934	0.9499
- 14.1		Q1	0.9349	0:9736
	1.5	Q2	0.9329	0.9737
		03	0.9305	0.9744
	N1	Q4	0.9332	0.9746
	A Trees	Q5	0.9275	0.9749
5 P		QG	0.9291	0.9752
P1. R3		07	0.9316	0.9748
		Q8	0.9341	0.9722
		Q1	0.9014	0.9543
		Q2	0.9050	0.9523
	1.5	Q3	0.8916	0.9490
	N2	Q4	0,9049	0.9553
		Q5	0.9005	0.9493
100		Q6	0.9026	0.9496
20.03	-	07	0.8890	0.9471
		Q8	0.8969	0.9468

'n

Table 6.15: Simulated coverage probabilities for two-dimensional case

156

Structure combinations		scp		
		90%	95%	
		Q1	0.9372	0.9801
	N1	02	0.9262	0.9694
		Q3	0.9559	0.9870
		Q4	0.9360	0.9771
		Q5	0.9268	0.9735
		Q6	0.9376	0:9791
		07	0.9158	0.9588
P2, R1		Q8	0.9390	0.9758
		Q1	0.8990	0.9535
		Q2	0.9065	0.9526
0.201		Q3	0.9046	0.9551
	N2	Q4	0.8889	0.9467
		QS	0.9068	0.9526
		Q6	0.8945	0.9500
1		07	0.8952	0.9502
		QB	0.8887	0.9465
		Q1	0.9374	0,9772
1		Q2	0.9294	0.9667
12113		Q3	0.9614	0.9895
	N1	Q4	0.9264	0.9708
		05	0.9197	0.9745
		QG	0.9378	0.9749
		07	0 9064	0.9622
P2 82		DR	0.9381	0.9754
	19-20-20	D1	0.8975	0.9439
		02	0.8976	0.9445
		03	0.9054	0.9550
	NI2	04	0.8962	0.9516
		05	0 8975	0.9466
1.1.1		06	0 8953	0.9464
		07	0.8998	0.9505
1.00		08	0 8899	0 9430
		01	0.9370	0.9758
		02	0.9207	0.9739
		03	0.9587	0 9888
1.1	MP	04	0 9268	0.9726
		05	n 9176	0 9664
		06	0.9393	0 9782
P2, R3		07	0.9131	0.9588
		08	0 9374	0 9738
		01	0.8968	0.9460
		02	0 8947	0.9413
		03	0.9010	0.9467
1.1.1.1	NO.	04	0.8958	0.9443
	145	05	0.8887	0 9479
		30	1 8005	0 9494
		07	0.0000	0.9515
		08	0.3021	0.00138
		100	0.0311	0.9430

Table 6.16: Simulated coverage probabilities for two-dimensional case

Structure combinations		scp		
		90%	95%	
in the second		Q1	0.9249	0.9687
		02	0.9447	0.9747
		Q3	0.9400	0.9739
	N1	Q4	0.9325	0.9779
		Q5	0.9200	0.9649
		Q6	0.9285	0.9746
		Q7	0.9421	0.9760
P3. R1		Q8	0.9454	0.9796
		Q1	0.9092	0.9521
- # <sup>-</sup>		Q2	0.8906	0.9464
		Q3	0.9042	0.9553
10100	N2	Q4	0.9045	0.9566
		Q5	0.9049	0.9560
1.1.1		QG	0.9004	0.9496
		Q7	0.8912	0.9474
1.1		Q8	0.8979	0.9465
		Q1	0.9067	0.9584
		02	0.9378	0.9731
		03	0.9393	0.9739
	N1	Q4	0.9365	0.9750
		Q5	0.9338	0.9775
		QG	0.9282	0.9704
		Q7	0.9414	0.9742
P3. R2		Q8	0.9391	0.9706
		Q1	0.9074	0.9627
		Q2	0.8929	0.9463
		Q3	0.9001	0.9505
1	N2	Q4	0.8969	0.9521
		QS	0.9029	0.9552
		Q6	0.8963	0.9540
		07	0,8956	0.9486
		QB	0.8971	0.9472
		Q1	0.9504	0.9813
		Q2	0.9442	0.9827
		03	0.9286	0.9763
	M	Q4	0.9229	0.9689
		Q5	0.9127	0.9670
P3, R3		06	0.9220	0.9688
		07	0.9428	0.9748
		QB	0.9471	0.9809
	antende de la composición de	Q1	0.9045	0.9540
		Q2	0.8918	0.9446
		Q3	0.8942	0.9475
	N2	Q4	0,8963	0.9503
12.4.3		Q5	0.8994	0.9494
		06	0.8997	0.9505
1000		07	0.8930	0.9468
and the second		OR I	0.9026	0.9521

Table 6.17: Simulated coverage probabilities for two-dimensional case

158

Structure combinations		scp		
		90%	95%	
		Q1	0.9350	0.9691
	Ň1	Q2	0.9407	0.9796
		Q3	0.9444	0.9746
		Q4	0.9389	0.9754
		Q5	0.9276	0.9702
		QG	0.9412	0.9734
		07	0.9457	0.9798
P4, R1	La constante de	QB	0.9467	0.9776
		Q1	0.8913	0.9482
		Q2	0.8874	0.9432
		Q3	0.8978	0.9499
8	N2	Q4	0:9031	0.9511
		Q5	0.9046	0.9487
a line new li		Q6	0.9046	0.9512
		07	0.9059	0.9514
		QB	0.8912	0.9443
		Q1	0.9191	0.9628
		Q2	0.9337	0.9728
		03	0.9431	0.9776
	N1	04	0.9363	0.9778
		05	0.9306	0.9707
1.4		QG	0.9378	0.9762
		07	0.9428	0.9737
P4 82		08	0.9415	0.9713
		01	0 9016	0.9459
		02	0 8977	0.9488
1		03	0.8990	0.9515
	N2	04	0.8943	0.9554
	142	05	0 9094	0.9508
		06	0 9007	0.9505
		07	0 8961	0.9495
1.1		08	0 8951	0.9458
		01	0.9451	0.9764
		02	0.9375	0.9757
	M4	03	0 9386	0.9718
		04	0 9342	0.9736
1		05	0 9246	0 9740
1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 - 1941 -		06	0.9352	0 9706
		07	0.9394	0.9740
P4, R3		08	0.9413	0.9740
	Chine Contraction	01	0.9030	0.9534
		02	0.9043	0.9533
	NO	03	0.8963	0 9551
		04	0.9035	0 9517
	142	05	0.9061	0.9516
		06	0.0001	0.00100
		07	0.80330	0.9478
		00	n 2000	0.0470
		00	0.0906	0.9521

Table 6.18: Simulated coverage probabilities for two-dimensional case

### 6.3.3 Conclusions

From the simulation results for both one-dimensional and two-dimensional cases, it is clear that the total sample size N plays a central role. When N is small, the confidence bands tends to be conservative. But for a sufficiently large N, the simulated coverage probabilities are often very close to the nominal confidence levels. This observation agrees with the large sample theory which is the base of the construction of simultaneous confidence bands for generalized linear models.

.

## Chapter 7

# Conclusions and future work

### 7.1 Conclusions

This thesis considers the construction of simultaneous confidence bands for a classical normal-error linear regression model and a general linear logistic regression model with a binary response variable. From the work in the last few chapters, some main conclusions can be drawn.

### 7.1.1 For linear regression

For linear regression, the confidence bands, centered by the estimated mean responses  $\mathbf{x}^{T}\hat{\boldsymbol{\beta}}$  and with the band width proportional to the standard error of  $\mathbf{x}^{T}\hat{\boldsymbol{\beta}}$ , are of interest. This type of confidence bands are of hyperbolic shape following Scheffé (1953)'s procedure, and are more popular than the bands of other shapes. Also, it is important to impose a constraint on each predictor variable so that the confidence bands constructed over the obtained restricted region are not unnecessarily wide when we deal with a real problem. Therefore, constructing exact confidence bands over different restricted regions becomes the central task. Two most frequently mentioned regions are the ellipsoidal region that centered at the point of the means of the predictor variables, and the rectangular region that is formed by imposing an interval constraint on each predictor variable.

Over an ellipsoidal region, this thesis summarizes three methods to construct both one-sided and two-sided exact simultaneous confidence bands for a linear regression model. These three methods are: the method following the idea of Bohrer (1973), the algebraical method, and the tubular neighborhood method. They start from the same point and are proven to have the equivalent computational formulae for calculation of critical values. Furthermore, it is found that the first method has a relatively simple computational formula for both simple and multiple linear regression cases. In addition, for some special cases, these three methods agree with some other well-known methods in statistical literatures. For instance, the first method of constructing one-sided and two-sided bands for a simple linear regression was considered by Bohrer and Francis (1972) and Wynn and Bloomfield (1971) respectively. The algebraical method of constructing two-sided bands for a multiple linear regression was considered by Casella and Strawderman (1980). Moreover, the idea of the tubular neighborhood method also appeared in Naiman (1986), Sun and Loader (1994).

To construct simultaneous confidence bands for a regression model over a rectangular region, several methods are available. Among these methods, Naiman (1986) produced a conservative confidence band for one-dimensional regression models, and his idea may be applied to the high dimensional cases but no explicit computational formula was given. The approximate method of Sun and Loader (1994) considered an approximation to the tube formula. The simulation-based method of Liu, Wynn and Hayter (2005) and Liu, Jamshidian, Zhang and Donnelly (2005) for polynomial regression and multiple linear regression respectively used Monte Carlo simulation. This thesis compares these methods in terms of critical values for simple linear regression, polynomial regression and bivariate linear regression respectively. From the simulation results, several conclusions can be drawn. The simulation-based method of Liu *et al.* (2005) can compute critical values almost as accurate as the exact method for a simple linear regression. It is better than the conservative method of Naiman (1986) and the approximate method of Sun

162

and Loader (1994) for polynomial and bivariate linear regressions. Naiman's method is quite good in the sense that it is a conservative method but its critical values are actually not too conservative. The approximate method, comparatively speaking, is bad but not seriously. These conclusions may be useful for someone who wants to construct simultaneous confidence bands for data analysis.

### 7.1.2 For logistic regression

For logistic regression, the base of constructing simultaneous confidence bands is the asymptotic normal distribution of the estimator. Hence, this thesis first illustrates a way of finding the asymptotic normality of the maximum likelihood estimator of the parameters of interest following the idea presented in Sen and Singer (1993).

Existing literatures on the construction of confidence bands for a logistic regression model are very limited. Methods of Brand, Pinnock and Jackson (1973) and Hauck (1983) construct confidence bands over the whole predictor space for simple and multiple regression cases respectively. Over a rectangular restricted region, we consider the Type 4 band of Sun, Loader and McCormick (2000) specially for the one-dimensional logistic regression. The method of Piegorsch and Casella (1988) for the construction of confidence bands for a multiple logistic regression is found not to be recommendable. This thesis considers two new methods following the ideas of Wynn and Bloomfield (1971) for simple regression and Liu, Jamshidian, Zhang and Donnelly (2005) for multiple regression. The confidence bands produced by these two methods are named WB band and Simulation-based band accordingly.

To assess the performance of these confidence bands, this thesis provides simulation studies for both one-dimensional and two-dimensional cases. From the simulated results, some useful conclusions can be drawn. The bands obtained based on large-size samples are better than those with small-size samples in the sense that the simulated coverage probabilities of the bands are clearly more closer to the nominal confidence levels for larger sample sizes. For one-dimensional case, WB band seems to be better than Type 4 band recommended by Sun, Loader and McCormick (2000), and it often performs very well when the sample size N is 200. For two-dimensional case, the Simulation-based bands are quite conservative when N = 60, and its simulated coverage probabilities are very close to the nominal confidence levels when N = 200.

### 7.2 Future work

This thesis considers constructing simultaneous confidence bands for only one regression model. The construction of confidence bands for two or more than two regression models may be of interest in the future work. Also, we only focus on the construction of confidence bands for a logistic regression with binary data in the thesis. We may consider constructing confidence bands for the ordinal logistic regression and the multinomial logistic regression. Moreover, we may think about other classes of regression models in the family of generalized linear models. Since all members of the generalized linear models share the large sample asymptotic property, the methods of constructing confidence bands should be similar.

# Appendix A

# Codes for computing the critical value and simulated coverage probability

This appendix provides the codes for computing the critical values using various methods for simple linear regression, polynomial regression and bivariate linear regression, and for computing the simulated coverage probabilities for the one-dimensional and two-dimensional linear logistic regressions. All codes in this appendix are written using MATLAB unless it is particularly specified.

## A.1 For computing the critical value for linear regression

# A.1.1 Obtaining c, using the exact method for simple linear regression

function c\_wb=wb\_cv(k0,nu,cl)

%%Output

```
%c_wb: the critical value of WB method
%%Input
%k0: the angle theta
%nu: the degree of freedom
%cl: the confidence level
tol=0.0001;
NO = 10000;
aa=1;bb=10;
faa=@(beta)fcdf((aa^2)/(2*(cos(beta))^2),2,nu);
int_faa=quad(faa,0,pi/2-k0/2);
HA=(2/pi)*(k0/2)*fcdf((aa^2)/2,2,nu)+(2/pi)*int_faa;
i=1;
while i<=NO
    c(i)=aa+(bb-aa)/2;
    f=@(beta)fcdf((c(i)^2)/(2*(cos(beta))^2),2,nu);
    int_f=quad(f,0,pi/2-k0/2);
    HI=(2/pi)*(k0/2)*fcdf((c(i)^2)/2,2,nu)+(2/pi)*int_f;
    if HI-cl==0 | (bb-aa)/2<tol
        c_wb=c(i);break
    end
    i=i+1;
    if HA*(HI-cl)<0
       aa=c(i-1);
       HA=HI;
    else
        bb=c(i-1);
    end
end
return
```

# A.1.2 Obtaining c, using the approximate method for simple linear regression

```
function c_app=app_cv(k0,nu,cl)
%%Output
%c_app: the critical value of the approximate method
%%Input
%k0,nu,cl: the same as before
tol=0.0001;
ND=10000;
aa=1;bb=10;
alpha_aa=(k0/pi)*(1+aa^2/nu)^(-nu/2)+2*(1-tcdf(aa,nu));
i=1;
while i<=NO
    c(i)=aa+(bb-aa)/2;
    alpha_I=(k0/pi)*(1+c(i)^2/nu)^(-nu/2)+2*(1-tcdf(c(i),nu));
    if alpha_I-(1-cl)==0 | (bb-aa)/2<tol
        c_app=c(i);break
    end
    i=i+1;
    if alpha_aa*(alpha_I-(1-cl))>0
        aa=c(i-1);
        alpha_aa=alpha_I;
    else
        bb=c(i-1);
    end
end
return
```

### A.1.3 Obtaining c, using the simulation-based method for simple linear regression

```
function [c_simu,se]=simu_cv(k0,nu,cl,nsim)
```

%%Output

%c\_simu: the critical value of the simulation-based method %se: the standard error %%Input %k0,nu,cl: the same as before %nsim: the number of simulations

```
%Generate sigma^/sigma
S=sqrt(sum(randn(nu,nsim).^2)./nu);
```

```
%Compute T
```

%Compute the quantile of the simulated values

```
T=sort(T);
r=nsim*cl;
c_simu=T(r);
```

```
%Compute the standard error of c
d=0.01;
K=(c_simu-T)/d;
g=sum((1/(d*sqrt(2*pi)))*exp(-0.5*(K.^2)))/length(T);
se=sqrt((cl*(1-cl))/(g^2*length(T)));
return
```

### A.1.4 Obtaining c, using Naiman's method for polynomial regression

```
function c_naiman=naiman_1d_cc(w,cl,p1,a,b);
```

%%Output

```
%c_naiman: the critical value of Naiman's method
%%Input
%w: the design points of the only predictor variable
%cl: the confidence level
%p1: the order of the polynomial regression plus 1
%a: the lower bound of the restricted interval
%b: the upper bound of the restricted interval
```

```
n=length(w);
nu=n-p1;
for j=1:p1
    X(:,j)=w'.^(j-1);
end
P=sqrtm(inv(X'*X));
p=fliplr(P);
```
```
for j=1:p1
    sqp(j,:)=conv(p(j,:),p(j,:));
end
sqmolp=sum(sqp);
x=a:(b-a)/1000:b;
for k=1:length(x)
    for j=1:(p1-1)
        xdp(j)=x(k)^{(p1-1-j)};
    end
    for j=1:((p1-1)*2+1)
        xsqmolp(j)=x(k)^{((p1-1)*2+1-j)};
    end
    for j=1:p1
        xp(j)=x(k)^{(p1-j)};
    end
    for j=1:(p1-1)*2
        xdsqmolp(j)=x(k)^{(p1-1)*2-j};
    end
    for j=1:p1
        dT(j)=(polyder(p(j,:))*xdp'*sqrt(sqmolp*xsqmolp')-
        p(j,:)*xp'*(1/(2*sqrt(sqmolp*xsqmolp')))*
        (polyder(sqmolp)*xdsqmolp'))/(sqmolp*xsqmolp');
    end
    moldT(k)=norm(dT);
end
for m=1:(length(x)-1)
    T(m) = (moldT(m) + moldT(m+1))/2;
end
k0=((b-a)/1000)*sum(T');
tol=0.0001;
```

```
ND=100000;
aa=1;bb=10;
t=0:(1/(aa*1000)):(1/aa);
for m=1:length(t)
    faa(m)=min((fcdf(2*((aa*t(m))^(-2)-1)/(p1-2),p1-2,2)*
    (k0/pi)+fcdf((((aa*t(m))^(-2)-1)/(p1-1),p1-1,1)),1)*
    fpdf(p1*t(m)^2,nu,p1)*2*p1*t(m);
end
for k=1:(length(t)-1)
    Func_aa(k) = (faa(k) + faa(k+1))/2;
end
alpha_aa=(1/(aa*1000))*sum(Func_aa');
i=1;
while i<=NO
    c(i)=aa+(bb-aa)/2;
    t_I=0:(1/(c(i)*1000)):(1/c(i));
    for m=1:length(t_I)
        f_I(m)=min((fcdf(2*((c(i)*t_I(m))^(-2)-1)/(p1-2),p1-2,2))
        *(k0/pi)+fcdf((((c(i)*t_I(m))^(-2)-1)/(p1-1),p1-1,1)),1)*
        fpdf(p1*t_I(m)^2,nu,p1)*2*p1*t_I(m);
    end
    for k=1:(length(t_I)-1)
        Func_I(k) = (f_I(k) + f_I(k+1))/2;
    end
    alpha_I=(1/(c(i)*1000))*sum(Func_I');
    if alpha_I-(1-cl)==0 | (bb-aa)/2<tol
        c_naiman=c(i);
        alpha=alpha_I; break
    end
   i=i+1;
    if alpha_aa*(alpha_I-(1-cl))>0
```

```
aa=c(i-1);
alpha_aa=alpha_I;
else
bb=c(i-1);
end
end
return
```

## A.1.5 Obtaining c, using the approximate method for polynomial regression

```
%%Output
c_{app}: the critical value of the approximate method
%%Input
%w,cl,p1,a,b: the same as before
n=length(w);
nu=n-p1;
for j=1:p1
    X(:,j)=w'.^(j-1);
end
q=X*inv(X'*X);
l=fliplr(q);
for j=1:n
    sql(j,:)=conv(l(j,:),l(j,:));
end
sqmoll=sum(sql);
x=a:(b-a)/1000:b;
for k=1:length(x)
```

function c\_app=approxi\_1d\_cc(w,cl,p1,a,b);

```
for j=1:(p1-1)
        xdl(j)=x(k)^{(p1-1-j)};
    end
    for j=1:((p1-1)*2+1)
        xsqmoll(j)=x(k)^((p1-1)*2+1-j);
    end
    for j=1:p1
        xl(j)=x(k)^{(p1-j)};
    end
    for j=1:(p1-1)*2
        xdsqmoll(j)=x(k)^{(p1-1)*2-j};
    end
    for j=1:n
        dT(j)=(polyder(l(j,:))*xdl'*sqrt(sqmoll*xsqmoll')-
        l(j,:)*xl'*(1/(2*sqrt(sqmoll*xsqmoll')))*
        (polyder(sqmoll)*xdsqmoll'))/(sqmoll*xsqmoll');
    end
    moldT(k)=norm(dT);
end
for m=1:(length(x)-1)
    T(m) = (moldT(m) + moldT(m+1))/2;
end
k0=((b-a)/1000)*sum(T');
tol=0.0001;
ND = 10000;
aa=1;bb=10;
alpha_aa=(k0/pi)*(1+aa^2/nu)^(-nu/2)+2*(1-tcdf(aa,nu));
i=1;
while i<=NO
    c(i)=aa+(bb-aa)/2;
```

```
alpha_I=(k0/pi)*(1+c(i)^2/nu)^(-nu/2)+2*(1-tcdf(c(i),nu));
if alpha_I-(1-cl)==0 | (bb-aa)/2<tol
        c_app=c(i);
        alpha=alpha_I;break
end
i=i+1;
if alpha_aa*(alpha_I-(1-cl))>0
        aa=c(i-1);
        alpha_aa=alpha_I;
else
        bb=c(i-1);
end
end
return
```

### A.1.6 Obtaining c, using the simulation-based method for polynomial regression

```
For quadratic regression
```

```
function [c_simu,se]=simu_quadratic_c(w,a,b,cl,nsim);
```

%%output

%c\_simu: the critical value of the simulation-based method %se: the standard error of c\_simu %%input %w,a,b,cl: the same as before %nsim: the number of simulations

```
n=length(w);
for m=1:3
    X(:,m)=w'.^(m-1);
```

```
end
q=inv(X'*X);
P=sqrtm(q);nu=n-3;
%Generate (beta^-beta)/sigma
V=P*randn(3,nsim);
%Generate sigma^/sigma
S=sqrt(sum(randn(nu,nsim).^2)./nu);
%Compute T
for m=1:nsim
   U=V(:,m)*V(:,m)';
    a1=U(2,1);
    a2=2*U(3,1)+U(2,2);
    a3=2*U(3,2)+U(2,3);
    a4=2*U(3,3);
   poly1=[a4 a3 a2 a1];
   b1=q(1,1);
   b2=q(2,1)+q(1,2);
   b3=q(3,1)+q(2,2)+q(1,3);
   b4=q(3,2)+q(2,3);
   b5=q(3,3);
   poly2=[b5 b4 b3 b2 b1];
    c1=U(1,1);
    c2=U(2,1)+U(1,2);
   c3=U(3,1)+U(2,2)+U(1,3);
   c4=U(3,2)+U(2,3);
   c5=U(3,3);
```

```
poly3=[c5 c4 c3 c2 c1];
    d1=q(2,1);
    d2=2*q(3,1)+q(2,2);
    d3=2*q(3,2)+q(2,3);
    d4=2*q(3,3);
    poly4=[d4 d3 d2 d1];
    g=conv(poly1,poly2)-conv(poly3,poly4);
    y=roots(g);
    for j=1:3
        A(j)=a^(j-1);
        B(j)=b^(j-1);
    end
    ha=abs(A*V(:,m))/sqrt(A*q*A');
    hb=abs(B*V(:,m))/sqrt(B*q*B');
    for j=1:(4*3-6)
        for k=1:3
            Y_j(k)=y(j)^{(k-1)};
        end
        if y(j)>a & y(j)<b
            h(j)=abs(Yj*V(:,m))/sqrt(Yj*q*Yj');
        else
            h(j)=0;
        end
    end
    H=[real(h) ha hb];
    H_max=max(H);
    Q(m) = H_max;
end
T=Q./S;
```

```
%Compute the quantile of the simulated values
T=sort(T);
r=nsim*cl;
c_simu=T(r);
```

```
%Compute the standard error
d=0.01;
K=(c_simu-T)/d;
g=sum((1/(d*sqrt(2*pi)))*exp(-0.5*(K.^2)))/length(T);
se=sqrt((cl*(1-cl))/(g^2*length(T)));
return
```

```
For cubic regression
```

```
function [c_simu,se]=simu_cubic_c(w,a,b,cl,nsim);
```

 $\ensuremath{\ens$ 

```
n=length(w);
for m=1:4
    X(:,m)=w'.^(m-1);
end
q=inv(X'*X);
P=sqrtm(q);
nu=n-4;
```

```
%Generate (beta^-beta)/sigma
V=P*randn(4,nsim);
```

%Generate sigma^/sigma

```
S=sqrt(sum(randn(nu,nsim).^2)./nu);
```

```
%compute T
for m=1:nsim
    U=V(:,m)*V(:,m)';
    a1=U(2,1);
    a2=2*U(3,1)+U(2,2);
    a3=3*U(4,1)+2*U(3,2)+U(2,3);
    a4=3*U(4,2)+2*U(3,3)+U(2,4);
    a5=3*U(4,3)+2*U(3,4);
    a6=3*U(4,4);
    poly1=[a6 a5 a4 a3 a2 a1];
```

```
b1=q(1,1);
b2=q(2,1)+q(1,2);
b3=q(3,1)+q(2,2)+q(1,3);
b4=q(4,1)+q(3,2)+q(2,3)+q(1,4);
b5=q(4,2)+q(3,3)+q(2,4);
b6=q(4,3)+q(3,4);
b7=q(4,4);
poly2=[b7 b6 b5 b4 b3 b2 b1];
```

```
c1=U(1,1);
c2=U(2,1)+U(1,2);
c3=U(3,1)+U(2,2)+U(1,3);
c4=U(4,1)+U(3,2)+U(2,3)+U(1,4);
c5=U(4,2)+U(3,3)+U(2,4);
c6=U(4,3)+U(3,4);
c7=U(4,4);
poly3=[c7 c6 c5 c4 c3 c2 c1];
```

```
d1=q(2,1);
    d2=2*q(3,1)+q(2,2);
    d3=3*q(4,1)+2*q(3,2)+q(2,3);
    d4=3*q(4,2)+2*q(3,3)+q(2,4);
    d5=3*q(4,3)+2*q(3,4);
    d6=3*q(4,4);
    poly4=[d6 d5 d4 d3 d2 d1];
    g=conv(poly1,poly2)-conv(poly3,poly4);
    y=roots(g);
    for j=1:4
        A(j)=a^(j-1);
        B(j)=b^(j-1);
    end
    ha=abs(A*V(:,m))/sqrt(A*q*A');
    hb=abs(B*V(:,m))/sqrt(B*q*B');
    for j=1:(4*4-6)
        for k=1:4
            Y_{j}(k)=y_{j}(k-1);
        end
        if y(j)>a & y(j)<b
            h(j)=abs(Yj*V(:,m))/sqrt(Yj*q*Yj');
        else
            h(j)=0;
        end
    end
    H=[real(h) ha hb];
    H_max=max(H);
    Q(m) = H_max;
end
```

T=Q./S;

```
%Compute the quantile of the simulated values
T=sort(T);
r=nsim*cl;
c_simu=T(r);
```

```
%Compute the standard error
d=0.01;
K=(c_simm-T)/d;
g=sum((1/(d*sqrt(2*pi)))*exp(-0.5*(K.^2)))/length(T);
se=sqrt((cl*(1-cl))/(g^2*length(T)));
return
```

#### For 4th order polynomial regression

```
function [c_simu,se]=simu_poly_c(w,a,b,cl,nsim);
%All outputs and inputs are the same as before
n=length(w);
for m=1:5
    X(:,m)=w'.^(m-1);
end
q=inv(X'*X);
P=sqrtm(q);
nu=n-5;
%Generate (beta^-beta)/sigma
V=P*randn(5,nsim);
%Generate sigma^/sigma
```

S=sqrt(sum(randn(nu,nsim).^2)./nu);

```
%compute T
for m=1:nsim
    U=V(:,m)*V(:,m)';
    a1=U(2,1);
    a2=2*U(3,1)+U(2,2);
    a3=3*U(4,1)+2*U(3,2)+U(2,3);
    a4=4*U(5,1)+3*U(4,2)+2*U(3,3)+U(2,4);
    a5=4*U(5,2)+3*U(4,3)+2*U(3,4)+U(2,5);
    a6=4*U(5,3)+3*U(4,4)+2*U(3,5);
    a7=4*U(5,4)+3*U(4,5);
    a8=4*U(5,5);
    poly1=[a8 a7 a6 a5 a4 a3 a2 a1];
```

```
b1=q(1,1);
b2=q(2,1)+q(1,2);
b3=q(3,1)+q(2,2)+q(1,3);
b4=q(4,1)+q(3,2)+q(2,3)+q(1,4);
b5=q(5,1)+q(4,2)+q(3,3)+q(2,4)+q(1,5);
b6=q(5,2)+q(4,3)+q(3,4)+q(2,5);
b7=q(5,3)+q(4,4)+q(3,5);
b8=q(5,4)+q(4,5);
b9=q(5,5);
poly2=[b9 b8 b7 b6 b5 b4 b3 b2 b1];
```

```
c1=U(1,1);
c2=U(2,1)+U(1,2);
c3=U(3,1)+U(2,2)+U(1,3);
c4=U(4,1)+U(3,2)+U(2,3)+U(1,4);
c5=U(5,1)+U(4,2)+U(3,3)+U(2,4)+U(1,5);
```

```
c6=U(5,2)+U(4,3)+U(3,4)+U(2,5);
c7=U(5,3)+U(4,4)+U(3,5);
c8=U(5,4)+U(4,5);
c9=U(5,5);
poly3=[c9 c8 c7 c6 c5 c4 c3 c2 c1];
```

```
d1=q(2,1);
d2=2*q(3,1)+q(2,2);
d3=3*q(4,1)+2*q(3,2)+q(2,3);
d4=4*q(5,1)+3*q(4,2)+2*q(3,3)+q(2,4);
d5=4*q(5,2)+3*q(4,3)+2*q(3,4)+q(2,5);
d6=4*q(5,3)+3*q(4,4)+2*q(3,5);
d7=4*q(5,4)+3*q(4,5);
d8=4*q(5,5);
poly4=[d8 d7 d6 d5 d4 d3 d2 d1];
```

else

```
h(j)=0;
end
end
H=[real(h) ha hb];
H_max=max(H);
Q(m)=H_max;
end
T=Q./S;
```

%Compute the quantile of the simulated values T=sort(T); r=nsim\*cl; c\_simu=T(r);

```
%Compute the standard error
d=0.01;
K=(c_simu-T)/d;
g=sum((1/(d*sqrt(2*pi)))*exp(-0.5*(K.^2)))/length(T);
se=sqrt((cl*(1-cl))/(g^2*length(T)));
return
```

## A.1.7 Obtaining c, using the approximate method for bivariate linear regression

function cc\_app=approxi\_2d\_cc(X,a,b,c,d,cl)

%%Output %cc\_app: the critical value of the approximate method %%Input %X: the design matrix %a,b: the lower and upper bounds of the restricted interval %c,d: the lower and upper bounds of the restricted interval

```
%cl: the confidence level
n=length(X(:,1)');
nu=n-3;
l=X*inv(X'*X);
for j=1:n
     sql(j,:)=[l(j,1)<sup>2</sup> l(j,2)<sup>2</sup> l(j,3)<sup>2</sup> 2*l(j,1)*l(j,2)
      2*l(j,1)*l(j,3) 2*l(j,2)*l(j,3)];
end
sqmoll=sum(sql);
dxl=l(:,2);
dyl=1(:,3);
dxsqmoll=[2*sqmoll(2) sqmoll(4) sqmoll(6)];
dysqmoll=[2*sqmoll(3) sqmoll(5) sqmoll(6)];
x=a:(b-a)/1000:b;
y=c:(d-c)/1000:d;
%Compute k0
for j=1:length(x)
     for k=1:length(y)
         xysqmoll=[1 x(j)^2 y(k)^2 x(j) y(k) x(j)*y(k)];
         xyl=[1 x(j) y(k)];
         xydxsqmoll=[x(j) 1 y(k)];
         xydysqmoll=[y(k) 1 x(j)];
         Tx=(dxl*sqrt(sqmoll*xysqmoll')-(l*xyl')*
         (1/(2*sqrt(sqmoll*xysqmoll')))*
         (dxsqmoll*xydxsqmoll'))/(sqmoll*xysqmoll');
         Ty=(dyl*sqrt(sqmoll*xysqmoll')-(l*xyl')*
         (1/(2*sqrt(sqmoll*xysqmoll')))*
         (dysqmoll*xydysqmoll'))/(sqmoll*xysqmoll');
         A = [Tx Ty];
```

```
f(k)=sqrt(det(A'*A));
    end
    for m=1:(length(y)-1)
        g(m) = (f(m)+f(m+1))/2;
    end
    k_int(j)=(d-c)/1000*sum(g');
end
for ii=1:(length(x)-1)
    K_int(ii)=(k_int(ii)+k_int(ii+1))/2;
end
k0=((b-a)/1000)*sum(K_int');
%Compute s0
for k=1:length(y)
    aysqmoll=[1 a^2 y(k)^2 a y(k) a*y(k)];
    ayl=[1 a y(k)];
    aydxsqmoll=[a 1 y(k)];
    aydysqmoll=[y(k) 1 a];
    Ty=(dyl*sqrt(sqmoll*aysqmoll')-(l*ayl')*
    (1/(2*sqrt(sqmoll*aysqmoll')))*
    (dysqmoll*aydysqmoll'))/(sqmoll*aysqmoll');
    f(k)=sqrt(det(Ty'*Ty));
end
for m=1:(length(y)-1)
    g(m) = (f(m)+f(m+1))/2;
end
ka_int=((d-c)/1000)*sum(g');
for k=1:length(y)
    bysqmoll=[1 b^2 y(k)^2 b y(k) b*y(k)];
    byl=[1 b y(k)];
```

```
bydxsqmoll=[b 1 y(k)];
    bydysqmoll=[y(k) 1 b];
    Ty=(dyl*sqrt(sqmoll*bysqmoll')-(l*byl')*
    (1/(2*sqrt(sqmoll*bysqmoll')))*
    (dysqmoll*bydysqmoll'))/(sqmoll*bysqmoll');
    f(k)=sqrt(det(Ty'*Ty));
end
for m=1:(length(y)-1)
    g(m) = (f(m)+f(m+1))/2;
end
kb_int=((d-c)/1000)*sum(g');
for j=1:length(x)
    xcsqmoll=[1 x(j)^2 c^2 x(j) c x(j)*c];
    xcl=[1 x(j) c];
    xcdxsqmoll=[x(j) 1 c];
    xcdysqmoll=[c 1 x(j)];
    Tx=(dxl*sqrt(sqmoll*xcsqmoll')-(l*xcl')*
    (1/(2*sqrt(sqmoll*xcsqmoll')))*
    (dxsqmoll*xcdxsqmoll'))/(sqmoll*xcsqmoll');
    f(j)=sqrt(det(Tx'*Tx));
end
for m=1:(length(x)-1)
    g(m) = (f(m)+f(m+1))/2;
end
kc_int=((b-a)/1000)*sum(g');
for j=1:length(x)
    xdsqmoll=[1 x(j)^2 d^2 x(j) d x(j)*d];
    xdl=[1 x(j) d];
    xddxsqmoll=[x(j) 1 d];
```

```
xddysqmoll=[d 1 x(j)];
    Tx=(dxl*sqrt(sqmoll*xdsqmoll')-(l*xdl')*
    (1/(2*sqrt(sqmoll*xdsqmoll')))*
    (dxsqmoll*xddxsqmoll'))/(sqmoll*xdsqmoll');
    f(j)=sqrt(det(Tx'*Tx));
end
for m=1:(length(x)-1)
    g(m) = (f(m)+f(m+1))/2;
end
kd_int=((b-a)/1000)*sum(g');
s0=ka_int+kb_int+kc_int+kd_int;
tol=0.0001;
NO=10000;
aa=1;bb=10;
alpha_aa=(k0/pi^(3/2))*(gamma((nu+1)/2)/gamma(nu/2))*(aa/sqrt(nu))*
(1+aa<sup>2</sup>/nu)<sup>(-(nu+1)</sup>/2)+(s0/(2*pi))*(1+aa<sup>2</sup>/nu)<sup>(-nu</sup>/2)+2*(1-tcdf(aa,nu));
i=1;
while i<=NO
    c(i)=aa+(bb-aa)/2;
    alpha_I=(k0/pi^(3/2))*(gamma((nu+1)/2)/gamma(nu/2))*(c(i)/sqrt(nu))*
    (1+c(i)^2/nu)^(-(nu+1)/2)+(s0/(2*pi))*(1+c(i)^2/nu)^(-nu/2)+
    2*(1-tcdf(c(i),nu));
    if alpha_I-(1-cl)==0 | (bb-aa)/2<tol
        cc_app=c(i);
        alpha=alpha_I; break
    end
    i=i+1;
    if alpha_aa*(alpha_I-(1-cl))>0
        aa=c(i-1);
        alpha_aa=alpha_I;
```

```
else
    bb=c(i-1);
    end
end
return
```

# A.2 For computing the simulated coverage probability for logistic regression

## A.2.1 Obtaining *scp*, using the WB method for simple logistic regression

function scp\_wb=wb\_scp(x,N,b,a1,a2,nsim)

%%Output

%scp\_wb: the simulated coverage probability of WB method %%Input %x: the design points of the only predictor variable %N: the vector of sub-sample sizes %b: the vector of true regression coefficients %a1: the lower bound of the restricted interval %a2: the upper bound of the restricted interval %c1: the confidence level %nsim: the number of simulations

```
n=length(x);.
for k=1:nsim
    for j=1:n
        p_i(j)=exp(b(1)+b(2)*x(j))./(1+exp(b(1)+b(2)*x(j)));
        z(j)=binornd(N(j),p_i(j),1,1);
        if z(j)==N(j) | z(j)==0
```

```
z(j)=binornd(N(j),p_i(j),1,1);
    end
end
y=z./N;
diff=1;
b_es=[0;0]; %initial guess of b_es
while diff>0.0001
    b_old=b_es;
    p=exp(b_es(1)+b_es(2)*x)./(1+exp(b_es(1)+b_es(2)*x));
    for i=1:length(x)
        J1(i)=N(i)*p(i)*(1-p(i));
        J2(i)=J1(i)*x(i);
        J3(i)=J2(i)*x(i);
    end
    s=[sum(y-p);sum((y-p).*x)];
    J=[sum(J1) sum(J2); sum(J2) sum(J3)];
    b_es=b_old+J\s;
    diff=sum(abs(b_es-b_old));
end
f_inv=inv(J);
P=sqrtm(f_inv);
vector_a=(P*[1;a1])';
vector_b=(P*[1;a2])';
theta_ast=acos((vector_a*vector_b')/(norm(vector_a)*
norm(vector_b)))./2;
tol=0.0001;
ND=10000;
aa=1;bb=10;
f=@(w)chi2cdf(aa.^2./(cos(w).^2),2);
g=quad(f,0,pi/2-theta_ast);
```

```
HA=(2/pi)*theta_ast*chi2cdf(aa^2,2)+(2/pi)*g;
i=1;
while i<=NO
    c(i)=aa+(bb-aa)/2;
    f1=@(y1)chi2cdf(c(i).^2./(cos(y1).^2),2);
    g1=quad(f1,0,pi/2-theta_ast);
    HI=(2/pi)*theta_ast*chi2cdf(c(i)^2,2)+(2/pi)*g1;
    if HI-0.95==0 | (bb-aa)/2<tol
        cc_wb=c(i);break
    end
    i=i+1;
    if HA*(HI-0.95)<0
       aa=c(i-1);
       HA=HI;
    else
        bb=c(i-1);
    end
end
v1=P(:,1)+P(:,2).*a1;
v2=P(:,1)+P(:,2).*a2;
M=inv(P)'*(b'-b_es);
if (M>=v1 & M<=v2) | (-M>=v1 & -M<=v2)
    Q=norm(M);
else
    Q1=abs(v1'*M)/norm(v1);
    Q2=abs(v2'*M)/norm(v2);
    Q=\max(Q1,Q2);
end
T=Q;
if T>cc_wb
    r(k)=0;
```

```
else
        r(k)=1;
    end
end
r_sum=sum(r');
scp_wb=r_sum/nsim;
return
```

## A.2.2 Obtaining *scp* of Type 4 band for simple logistic regression, using **parfit** on S-plus

```
library(locfit,first=T)
scpT4<-function(x,N,b,a1,a2,nsim)</pre>
{
  for(i in 1:nsim)
  ſ
    pr<-exp(b[1]+b[2]*x)/(1+exp(b[1]+b[2]*x))
    z<-c(0,0,0,0,0)
    y<-c(0,0,0,0,0)
    J1 < -c(0,0,0,0,0)
    J2<-c(0,0,0,0,0)
    J3 < -c(0,0,0,0,0)
    v<-c(0,0,0)
    v1<-c(0,0,0)
    cc<-c(0,0,0)
    for(i in 1:length(x))
    {
      z[i] <- rbinom(1,N[i],pr[i])</pre>
    }
    y<-z/N
    bb<-glm(y~x,family=binomial)</pre>
```

```
bes<-unlist(bb[1],use.names=F)</pre>
p<-exp(bes[1]+bes[2]*x)/(1+exp(bes[1]+bes[2]*x))</pre>
for(i in 1:length(x))
ſ
  J1[i]<-N[i]*p[i]*(1-p[i])
  J2[i]<-J1[i]*x[i]
  J3[i]<-J2[i]*x[i]
}
J0<-c(sum(J1),sum(J2),sum(J2),sum(J3))</pre>
J<-matrix(J0,nrow=2,byrow=T)</pre>
finv<-solve(J)</pre>
t<-data.frame(x,z,N)
fit<-scb(z~x,type=4,w=N,data=t,deg=1,family="binomial",</pre>
kern="parm",xlim=c(a1,a2))
xp<-unlist(fit[1],use.names=F)</pre>
ll<-unlist(fit[4],use.names=F)</pre>
ul<-unlist(fit[5],use.names=F)</pre>
for(i in c(1,10,20))
ſ
  cc[i]<-(ul[i]-ll[i])/(2*sqrt(c(1,xp[i])%*%finv%*%
  matrix(c(1,xp[i]),nrow=2)))
}
ccapp<-(cc[1]+cc[10]+cc[20])/3
R<-seq(0,by=0,length=nsim)
q<-0
while(q<=20)
{
  u<-a1+q*(a2-a1)/20
  G1<-c(1,u)%*%matrix(b-bes,nrow=2)
  G2<-sqrt(c(1,u)%*%finv%*%matrix(c(1,u),nrow=2))
  H < -abs(G1)/G2
```

```
if(H>ccapp)
{
    R[i]<-0
    break
    }
    R[i]<-1
    q<-q+1
    }
}
Rsum<-sum(R)
scpapp<-Rsum/nsim
return(scpapp)</pre>
```

### A.2.3 Obtaining *scp*, using the simulation-based method for bivariate logistic regression

function scp\_simu=simu\_scp(x1,x2,N,b,a1,a2,a3,a4,cl,nsim1,nsim2)

%%Output

7

%scp\_simu: the simulated coverage probability of the confidence % band constructed based on the simulation method %%Input %x1: the design points of the first predictor variable %x2: the design points of the second predictor variable %N: the vector of sub-sample sizes %b: the vector of true regression coefficients %a1: the lower bound of the first restricted interval %a2: the upper bound of the first restricted interval %a3: the lower bound of the second restricted interval %a4: the upper bound of the second restricted interval %a4: the upper bound of the second restricted interval %c1: the confidence level

```
%nsim1: the number of simulations for computing critical value
%nsim2: the number of simulations for computing coverage probability
for k=1:nsim2
    p_i=exp(b(1)+b(2)*x1+b(3)*x2)./(1+exp(b(1)+b(2)*x1+b(3)*x2));
   for j=1:length(x1)
        z(j)=binornd(N(j),p_i(j),1,1);
        if z(j) == 0 | z(j) == N(j)
           z(j)=binornd(N(j),p_i(j),1,1);
        end
    end
   y=z./N;
   diff=1;
   b_es=[0;0;0]; %initial guess of b_es
   while diff>0.0001
        b_old=b_es;
        pr=exp(b_es(1)+b_es(2)*x1+b_es(3)*x2)./
        (1+\exp(b_es(1)+b_es(2)*x1+b_es(3)*x2));
        for i=1:length(x1)
            J1(i)=N(i)*pr(i)*(1-pr(i));
            J2(i)=J1(i)*x1(i);
            J3(i)=J2(i)*x1(i);
            J4(i)=J1(i)*x2(i);
            J5(i)=J2(i)*x2(i);
            J6(i)=J4(i)*x2(i);
        end
        s=[sum(y-pr);sum((y-pr).*x1);sum((y-pr).*x2)];
        J=[sum(J1) sum(J2) sum(J4);sum(J2) sum(J3) sum(J5);
        sum(J4) sum(J5) sum(J6)];
        b_es=b_old+J\s;
        diff=sum(abs(b_es-b_old));
```

```
end
```

```
f_inv=inv(J);
P=sqrtm(f_inv);
v1=P(:,1)+P(:,2).*a1+P(:,3).*a3;
v2=P(:,1)+P(:,2).*a1+P(:,3).*a4;
v3=P(:,1)+P(:,2).*a2+P(:,3).*a3;
v4=P(:,1)+P(:,2).*a2+P(:,3).*a4:
for i=1:nsim1
   M=randn(3,1);
    if (M>=v1 & M<=v4) | (-M>=v1 & -M<=v4)
        Q=norm(M);
    else
        B1=[v1 v2];
        B2=[v1 v3];
        B3=[v2 v4];
        B4=[v3 v4];
        [Q1,R1]=qr(B1,0);
        [Q2, R2] = qr(B2, 0);
        [Q3,R3]=qr(B3,0);
        [Q4, R4] = qr(B4, 0);
        D1=dot(Q1(:,1),M)*Q1(:,1)+dot(Q1(:,2),M)*Q1(:,2);
        D2=dot(Q2(:,1),M)*Q2(:,1)+dot(Q2(:,2),M)*Q2(:,2);
        D3=dot(Q3(:,1),M)*Q3(:,1)+dot(Q3(:,2),M)*Q3(:,2);
        D4=dot(Q4(:,1),M)*Q4(:,1)+dot(Q4(:,2),M)*Q4(:,2);
        if (D1>=v1 & D1<=v2) | (-D1>=v1 & -D1<=v2)
            Q11=abs(D1'*M)/norm(D1);
        else
            Q11=max(abs(v1'*M)/norm(v1),abs(v2'*M)/norm(v2));
        end
        if (D2>=v1 & D2<=v3) | (-D2>=v1 & -D2<=v3)
            Q12=abs(D2'*M)/norm(D2);
```

```
else
              Q12=max(abs(v1'*M)/norm(v1),abs(v3'*M)/norm(v3));
          end
          if (D3>=v2 & D3<=v4) | (-D3>=v2 & -D3<=v4)
              Q13=abs(D3'*M)/norm(D3);
          else
              Q13=max(abs(v2'*M)/norm(v2),abs(v4'*M)/norm(v4));
          end
          if (D4>=v3 & D4<=v4) | (-D4>=v3 & -D4<=v4)
              Q14=abs(D4'*M)/norm(D4);
          else
              Q14=max(abs(v3'*M)/norm(v3),abs(v4'*M)/norm(v4));
          end
          Qarray=[Q11 Q12 Q13 Q14];
          Q=max(Qarray);
      end
      T(i)=Q;
  end
  T=sort(T);
  r=nsim1*cl;
  cc_simu=T(r);
MM=inv(P)'*(b'-b_es);
  if (MM>=v1 & MM<=v4) | (-MM>=v1 & -MM<=v4)
      QQ=norm(MM);
  else
      DD1=dot(Q1(:,1),MM)*Q1(:,1)+dot(Q1(:,2),MM)*Q1(:,2);
      DD2=dot(Q2(:,1),MM)*Q2(:,1)+dot(Q2(:,2),MM)*Q2(:,2);
      DD3=dot(Q3(:,1),MM)*Q3(:,1)+dot(Q3(:,2),MM)*Q3(:,2);
      DD4=dot(Q4(:,1),MM)*Q4(:,1)+dot(Q4(:,2),MM)*Q4(:,2);
      if (DD1>=v1 & DD1<=v2) | (-DD1>=v1 & -DD1<=v2)
```

```
QQ11=abs(DD1'*MM)/norm(DD1);
        else
            QQ11=max(abs(v1'*MM)/norm(v1),abs(v2'*MM)/norm(v2));
        end
        if (DD2>=v1 & DD2<=v3) | (-DD2>=v1 & -DD2<=v3)
            QQ12=abs(DD2'*MM)/norm(DD2);
        else
            QQ12=max(abs(v1'*MM)/norm(v1),abs(v3'*MM)/norm(v3));
        end
        if (DD3>=v2 & DD3<=v4) | (-DD3>=v2 & -DD3<=v4)
            QQ13=abs(DD3'*MM)/norm(DD3);
        else
            QQ13=max(abs(v2'*MM)/norm(v2),abs(v4'*MM)/norm(v4));
        end
        if (DD4>=v3 & DD4<=v4) | (-DD4>=v3 & -DD4<=v4)
            QQ14=abs(DD4'*MM)/norm(DD4);
        else
            QQ14=max(abs(v3'*MM)/norm(v3),abs(v4'*MM)/norm(v4));
        end
        QQarray=[QQ11 QQ12 QQ13 QQ14];
        QQ=max(QQarray);
    end
    TT=QQ;
    if TT>cc_simu
        rr(k)=0;
    else
        rr(k)=1;
    end
rr_sum=sum(rr');
scp_simu=rr_sum/nsim2; return
```

end

### References

- Al-Saidy, O.M., Piegorsch, W.W., West, R.W. et al. (2002). "Confidence bands for low-dose risk estimation with quantal response data," *Biometrics*, 59, 1056-1062.
- Agresti, A., and Coull, B.A. (1998). "Approximate is better than 'exact' for interval estimation of binomial proportions," *American Statistician*, 52, 119-126.
- Blyth, C.R., and Still, H.A. (1983). "Binomial confidence intervals," Journal of the American Statistical Association, 78, 108-116.
- Bohrer, R. (1967). "On sharpening Scheffé bounds," Journal of the Royal Statistical Society (B), 29, 110-114.
- 5. Bohrer, R. and Francis, G.K. (1972). "Sharp one-sided confidence bands for linear regression over intervals," *Biometrika*, **59**, 99-107.
- Bohrer, R. (1973). "A multivariate t probability integral," *Biometrika*, 60, 647-654.
- Bowden, D.C. (1970). "Simultaneous confidence bands for linear regression models," Journal of the American Statistical Association, 65, 413-421.
- Brand, R.J., Pinnock, D.E., and Jackson, K.L. (1973). "Large sample confidence bands for the logistic response curve and its inverse," *American Statistician*, 27, 157-160.

- Brown, L.D., Cai, T.T., and DasGupta, A. (2000). "Interval estimation in exponential families," Technical report, available at www-stat.wharton.upenn.edu/~tcai/.
- Brown, L.D., Cai, T.T., and DasGupta, A. (2001). "Interval estimation for a binomial proportion," *Statistical Science*, 16, 101-133.
- Brown, L.D., Cai, T.T., and DasGupta, A. (2002). "Confidence intervals for a binomial proportion and asymptotic expansions," *Annals of Statistics*, 30, 160-201.
- Casella, G. and Strawderman, W.E. (1980). "Confidence bands for linear-regression with restricted predictor variables," *Journal of the American Statistical Association*, 75, 862-868.
- Chen, H. (1990). "The accuracy of approximate intervals for a binomial parameter," Journal of the American Statistical Association, 85, 514-518.
- Clopper, C.J., and Pearson, E.S. (1934). "The use of confidence or fiducial limits illustrated in the case of the binomial," *Biometrika*, 26, 404-413.
- 15. Collett, D. (2002). "Modelling Binary Data," 2nd ed, Chapman & Hall/CRC.
- Dobson, A.J. (2001). "An Introduction to Generalized Linear Models," 2nd ed, Chapman & Hall/CRC.
- Gafarian, A.V. (1964). "Confidence bands in straight line regression," Journal of the American Statistical Association, 59, 182-213.
- Ghosh, B.K. (1979). "A comparison of some approximate confidence intervals for the binomial parameter," *Journal of the American Statistical* Association, 74, 894-900.

- Graybill, F.A. and Bowden, D.C. (1967). "Linear segment confidence bands for simple linear regression models," *Journal of the American Statistical Association*, 62, 403-408.
- Halperin, M. and Gurian, J. (1968). "Confidence bands in linear regression with constraints on independent variables," *Journal of the American Statistical Association*, 63, 1020-1027.
- Halperin, M., Rastogi, S.C., Ho, I., and Yang, Y.Y. (1967). "Shorter confidence bands in linear regression," *Journal of the American Statistical Association*, 62, 1050-1067.
- 22. Hauck, W.W. (1983). "A note on confidence bands for the logistic response curve," *American Statistician*, **37**, 158-160.
- Hayter, A.J., Liu, W., and Wynn, H.P. (2005). "Easy-to-construct confidence bands for comparing two simple linear regression lines," *Manuscript*, Georgia Tech, USA.
- 24. Hsu, J.C. (1996). "Multiple Comparisons Theory and Methods," Chapman & Hall.
- Johansen, S. and Johnstone, I. (1990). "Hotelling's theorem on the volume of tubes: some illustrations in simultaneous inference and data analysis," *Annals of Statistics*, 18, 652-684.
- Knafl, G., Sacks, J., and Ylvisaker, D. (1985). "Confidence bands for regression-functions," *Journal of the American Statistical Association*, 80, 683-691.
- Kosorok, M.R. and Qu, R. (1999). "Exact simultaneous confidence bands for a collection of univariate polynomials in regression analysis," *Statistics in Medicine*, 18, 613-620.
- 28. Liu, W., Jamshidian, M., Zhang, Y., and Bretz, F. (2004). "Constant width simultaneous confidence bands in multiple linear regression

with predictor variables constrained in intervals," *Journal of Statistical Computation & Simulation*, **00**, 1-12.

- Liu, W., Jamshidian, M., Zhang, Y., and Donnelly, J. (2005). "Exact simultaneous confidence bands in multiple linear regression with predictor variables constrained in intervals," *Journal of Computational* and Graphical Statistics, 14(2), 459-484.
- 30. Liu, W., Wynn, H.P., and Hayter, A.J. (2005). "Statistical inferences for polynomial regression models."
- 31. Loader, C. (2004). "The Volume-of-Tube formula: Computational methods and statistical applications."
- 32. Montgomery, D.C., Peck, E.A., and Vining, G.G. (2006). "Introduction to Linear Regression Analysis," 4th ed, Wiley.
- Naiman, D.Q. (1983). "Comparing Scheffé-type to constant-width confidence bounds in regression," *Journal of the American Statistical* Association, 78, 906-912.
- Naiman, D.Q. (1986). "Conservative confidence bands in curvilinear regression," Annals of Statistics, 14, 896-906.
- Naiman, D.Q. (1987). "Simultaneous confidence-bounds in multipleregression using predictor variable constraints," *Journal of the American Statistical Association*, 82, 214-219.
- Naiman, D.Q. (1990). "Volumes of tubular neighborhoods of spherical polyhedra and statistical inference," Annals of Statistics, 18, 685-716.
- 37. Piegorsch, W.W. and Casella, G. (1988). "Confidence bands for logistic regression with restricted predictor variables," *Biometrics*, 44, 739-750.
- Scheffé, H. (1953). "A method for judging all contrasts in analysis of variance," *Biometrika*, 40, 87-104.

- Seppanen, E. and Uusipaikka, E. (1992). "Confidence bands for linearregression over restricted regions," *Scandinavia Journal of Statistics*, 19, 73-81.
- 40. Snee, R.D. (1977). "Validation of regression models: methods and examples," *Technometrics*, **19**, 415-428.
- 41. Sun, J.Y. and Loader, C.R. (1994). "Simultaneous confidence bands for linear regression and smoothing," *Annals of Statistics*, **22**, 1328-1346.
- 42. Sun, J.Y., Loader, C.R., and McCormick, W.P. (2000). "Confidence bands in generalized linear models," *Annals of Statistics*, **28**, 429-460.
- Sun, J.Y., Raz, J., and Faraway, J.J. (1999). "Confidence bands for growth and response curves," *Statistica Sinica*, 9, 679-698.
- Uusipaikka, E. (1983). "Exact confidence bands for linear-regression over intervals," Journal of the American Statistical Association, 78, 638-644.
- 45. Weisberg, S. (2005). "Applied Linear Regression," 3rd ed, Wiley.
- Wilson, E.B. (1927). "Probable inference, the law of succession, and statistical inference," *Journal of the American Statistical Association*, 22, 209-212.
- Working, H. and Hotelling, H. (1929). "Applications of the theory of error to the interpretation of trends," *Journal of the American Statistical Association*, 24, 73-85.
- Wynn, H.P. and Bloomfield, P. (1971). "Simultaneous confidence bands in regression analysis," *Journal of the Royal Statistical Society* (B), 33, 202-217.
- Wynn, H.P. (1975). "Integrals for one-sided confidence bounds: A general result," *Biometrika*, 62, 393-396.

- 50. Wynn, H.P. (1984). "An exact confidence band for one-dimensional polynomial regression," *Biometrika*, **71**, 375-379.
- 51. Yeh, B. (1996). "Bootstrap percentile confidence bands based on the concept of curve depth," *Communications in Statistics Simulation and computation*, **25**, 905-922.
- 52. Zheng, X.D., and Loh, W.Y. (1995). "Bootstrapping binomial confidenceintervals," *Journal of Statistical Planning and Inference*, **43**, 355-380.
- 53. Zheng, X.D. (1998). "Better saddlepoint confidence intervals via bootstrap calibration," *American Mathematical Society*, **126**, 3669-3679.