

1 **Microstructural interactions contribute to the hotspot in the**
2 **living cochlea**

3 Junpei Liu^{1,3#}, Yanru Bai^{1,3#}, Qianli Cheng², Shu Zheng^{1,3}, Stephen Elliott^{4*} and
4 Guangjian Ni^{1,2,3*}

5

6 ¹ Academy of Medical Engineering and Translational Medicine, Tianjin University,
7 Tianjin, 300072 China

8 ² Department of Biomedical Engineering, College of Precision Instruments and
9 Optoelectronics Engineering, Tianjin University, Tianjin, 300072 China

10 ³ Tianjin Key Laboratory of Brain Science and Neuroengineering, Tianjin, 300072
11 China

12 ⁴ Institute of Sound and Vibration Research, University of Southampton, Southampton,
13 SO17 1BJ UK

14 # contributed equally to this work

15 * Correspondence should be addressed to Stephen J Elliott: S.J.Elliott@soton.ac.uk and
16 Guangjian Ni: niguangjian@tju.edu.cn

17

18 **Highlights:**

- 19 ● 3D cochlea segmental models including micro-physiological structures were
20 developed.
- 21 ● The hotspot vibration is a local phenomenon in the cochlea.
- 22 ● The hotspot appears in the high- and low-frequency regions in the cochlea.

23 **Abstract**

24 The mechanism of the active cochlea relies on a complex interaction between
25 microstructures in the organ of Corti. A significant longitudinal vibration “hotspot” was

26 recently observed in the high-frequency region of the living gerbil cochlea between the
27 Deiters cells and the outer hair cells. A similar phenomenon was also found in guinea
28 pigs with a relatively smaller magnitude. The cause is unknown, but one hypothesis is
29 that this phenomenon is due to the structural constraints between different
30 microstructures. It is not easy to explain the mechanism of hotspots directly from
31 experimental observations. It may also be difficult to image or test if the hotspot will
32 occur in the low-frequency region in the cochlea. We built two three-dimensional finite
33 element models corresponding to the high- and low-frequency regions in the guinea pig
34 cochlea. Responses of the organ of Corti to passive acoustic and outer hair cell electrical
35 excitation were calculated. The two excitations were then superimposed to predict the
36 active response of the organ of Corti. The hotspot phenomenon in the experiment was
37 reproduced and analyzed in-depth about influencing factors. Our results indicate that
38 hotspots appear in the low-frequency region of the cochlea as well. We hypothesize that
39 the hotspot is a locally originated phenomenon in the cochlea, and the traveling wave
40 further enhances the response to low-frequency excitation. The movement of outer hair
41 cells inclined in the longitudinal direction is the leading cause of the hotspot.

42 **Keywords:** Hotspot, organ of Corti, finite element model, low-frequency

43

44 **1 Introduction**

45 The active amplification mechanism of the cochlea is related to the microscopic
46 movement in the organ of Corti (OC) (Robles and Ruggero, 2001; von Békésy, 1970).
47 At present, our understanding of this mechanism mainly relies on measurements in
48 animal experiments. Attention has been paid to the transverse movement of the basilar
49 membrane (BM), reticular lamina (RL), and tectorial membrane (TM), and differences
50 in the amplitude and phase were found (He et al., 2018; Ren et al., 2016). Recent
51 experiments have started to explore the areas of Deiters cells (DCs) and outer hair cells
52 (OHCs) (Cooper et al., 2018). They found that in the high-frequency region of the living
53 gerbil cochlea, the longitudinal response is significant and even greater than that of the
54 basilar membrane. This response is most evident near the connection between OHCs
55 and DCs, called “hotspot”. Similarly, Fallah et al. (2021) found that hotspot responses
56 also occur in the guinea pig, but the response magnitude was smaller than the gerbil.

57 Cooper et al. (2018) proposed that this phenomenon is driven by the movement of
58 OHCs, under the structural constraints of the organ of Corti. According to their
59 hypothesis, a similar response may also occur in the low-frequency region of the
60 cochlea, although this has not been observed experimentally yet.

61 This paper studied the hotspot using three-dimensional segmental finite element models
62 of the cochlea. Such models could reproduce experimentally observed results and test
63 different hypotheses. Our work showed that the hotspot could be simulated under the
64 following conditions:

65 (1) Including a three-dimensional structure that can simulate longitudinal
66 movement.

67 (2) Including the Phalangeal process (PhPs) to form a longitudinal structural
68 constraint.

69 (3) Including the physiological details of the organ of Corti to form a strong
70 constraint between microstructures.

71 (4) Ability to simulate the active response of the cochlea.

72 However, most of the existing cochlear models cannot meet the above conditions.
73 Traditional two-dimensional models cannot simulate the longitudinal movement of the
74 organ of Corti (Cai and Chadwick, 2003; Cai et al., 2004; Ni et al., 2016; Steele and
75 Puria, 2005). Beam models always need to simplify the geometry of the organ of Corti
76 (Nam, 2014; Nam and Fettiplace, 2010), but three-dimensional models could reflect
77 more detailed physiological structures (Zagadou et al., 2020). The “feedforward”
78 models proposed by Steele et al. (1993, 1999) and Geisler et al. (1995) reproduced
79 many of the structural features but did not focus on producing the longitudinal vibration
80 in the hotspot.

81 In this paper, we developed two three-dimensional segmented cochlear models,
82 including detailed micro-physiological structures in the organ of Corti, corresponding
83 to cochlear high- and low-frequency regions, respectively. These models included
84 orthotropic material properties of some microstructures, the OHCs longitudinal tilt, the
85 PhPs, and the longitudinal coupling between discontinuous structures. The
86 superposition of the OC responses due to acoustic and OHCs excitation was used for
87 calculating the active cochlear responses. The hotspot results simulated by the high-

88 frequency model are compared with the experiments to verify the effectiveness. Similar
89 results were obtained using the low-frequency model. Further, we analyzed the effect
90 of viewing angle on the results. We then changed part of the excitation conditions and
91 structure settings to illustrate the role and influence of some factors on the hotspot
92 phenomenon.

93 **2 Materials and methods**

94 **2.1 Model overview**

95 Two three-dimensional guinea pig cochlea segmental models were built in COMSOL
96 Multiphysics 5.6, including the detailed micro-physiological structures corresponding
97 to cochlear low- and high-frequency regions, as shown in Figure 1. The finite element
98 method was used to deal with the complexity of the geometric structures in the cochlea.
99 The models were built on the millimeter scale, and microstructures were on the
100 micrometer scale.

101 The high-frequency model was drawn based on geometry data from Salt laboratory¹
102 corresponding to the position where the characteristic frequency is about 16 kHz, and
103 the total thickness is 36 μm . The low-frequency model was drawn based on the existing
104 two-dimensional model (Ni et al., 2016), corresponding to the position where the
105 characteristic frequency is 0.8 kHz and the total thickness is 60 μm .

106 First, we constructed a high-frequency model to reproduce the hotspot phenomenon in
107 the experiments. The measured region by Cooper et al. (2018) corresponds to
108 characteristic frequencies from about 20 kHz to 40 kHz. According to the gerbil cochlea
109 frequency tonotopy (Muller, 1996), this frequency range corresponds to a position
110 range 10% to 23% of the total gerbil cochlea length away from the base. For the guinea
111 pig cochlea, 10% to 23% of the total length away from the base corresponds to a
112 characteristic frequency range of 14.3 kHz to 27 kHz (Greenwood, 1990; Ni et al., 2017;
113 Nuttall et al., 1999). Therefore, we built our high-frequency model with a characteristic
114 frequency of 16 kHz. Referring to the data of Salt laboratory and Fernandez (Fernandez,
115 1952), the scala vestibuli (SV) height was 463 μm , the scala media (SM) height was 77
116 μm , the scala tympani (ST) width was 318 μm , and the BM width was 110 μm in the

117 high-frequency model. The average length of OHCs in the 16 kHz model was 23 μm ,
118 consistent with estimations (Kelly, 1989).

119 Then we built the low-frequency model based on the 2D model by Ni et al. (2016). The
120 longitudinal continuity of microstructures in the cochlea was treated differently in the
121 model, as listed in Table 1. The scala fluid and part of the solid structures are
122 continuously distributed (Kikuchi et al., 1995). They were stretched with the same
123 length along the longitudinal direction as the overall model, 60 μm . A Thermoviscous-
124 Acoustics condition, used to solve linearized Navier–Stokes and Fourier heat equations,
125 was set for the fluids, but heat transmission was neglected, and only the fluid-flow
126 equations of momentum in the frequency domain were considered here, as

$$i\omega\rho_f\mathbf{u}_f = \nabla \cdot [-p_{va}\mathbf{I} + \mu(\nabla\mathbf{u}_f + (\nabla\mathbf{u}_f)^T) + (\mu_B - \frac{2}{3}\mu)(\nabla \cdot \mathbf{u}_f)\mathbf{I}] = 0, \quad (1)$$

127 where \mathbf{u}_f is the velocity field (the effects of gravity are neglected), ρ_f and p_{va} are the
128 fluid density and viscoacoustic fluid pressure. μ and μ_B are the dynamic and bulk
129 viscosity, respectively. \mathbf{I} represents the unity matrix, and i , ∇ , and ω are the imaginary
130 unit, differential operator, and angular frequency, respectively.

131 The pillar cells, hair cells, stereocilia, DCs, and Deiters rods were arranged at a specific
132 interval along the longitudinal direction (Raphael and Altschuler, 2003). The pillar and
133 hair cells were approximated as cylinders in the y - z plane with thickness of 3.2 μm and
134 8.4 μm in the longitudinal direction (Karavitaki and Mountain, 2007). The outer hair
135 cells were set to be inclined 10° in the longitudinal direction, referring to the average
136 measurement mice (Soons et al., 2015) because the guinea pig value is unknown yet.
137 The influence of different OHCs tilt angles on the results was discussed. The Deiters
138 cells were assigned the same longitudinal thickness with the outer hair cells, which were
139 close to measurement (Karavitaki and Mountain, 2007). The W or V-shaped hair
140 bundles at the top of the hair cells were simplified into the tallest row of stereocilia.
141 The stereocilia of OHCs were connected to the TM bottom, while the stereocilia of
142 IHCs were not (Lim, 1986). The stereocilia were all constructed with Timoshenko
143 beams and located in the middle layer of each segment along the longitudinal direction.
144 The diameters of the stereocilia, the PhPs, and the DC rods were set to be 0.2 μm , 1 μm ,
145 and 1 μm , respectively (Bohnke et al., 1999; Nam and Fettiplace, 2010). The gaps

146 between the discontinuous structures were filled with fluid, and discontinuous
 147 structures were entirely wrapped by fluid.

148 The PhPs were modeled with beam element, and one end was connected to the bottom
 149 of OHCs, and the top of Deiters rods, forming a Y-shaped structure. The other end of
 150 the PhPs was connected to the bottom of the reticular lamina. The average length of
 151 OHCs in the 0.8 kHz model is about 45 μm , consistent with estimations (Kelly, 1989).
 152 The experimental results show that the angle of OHCs and PhPs in the guinea pig
 153 cochlea is about 35° (Zetes et al., 2012). Based on the trigonometric relationship
 154 between the structures, the longitudinal spacing of PhPs is about 3 OHCs.

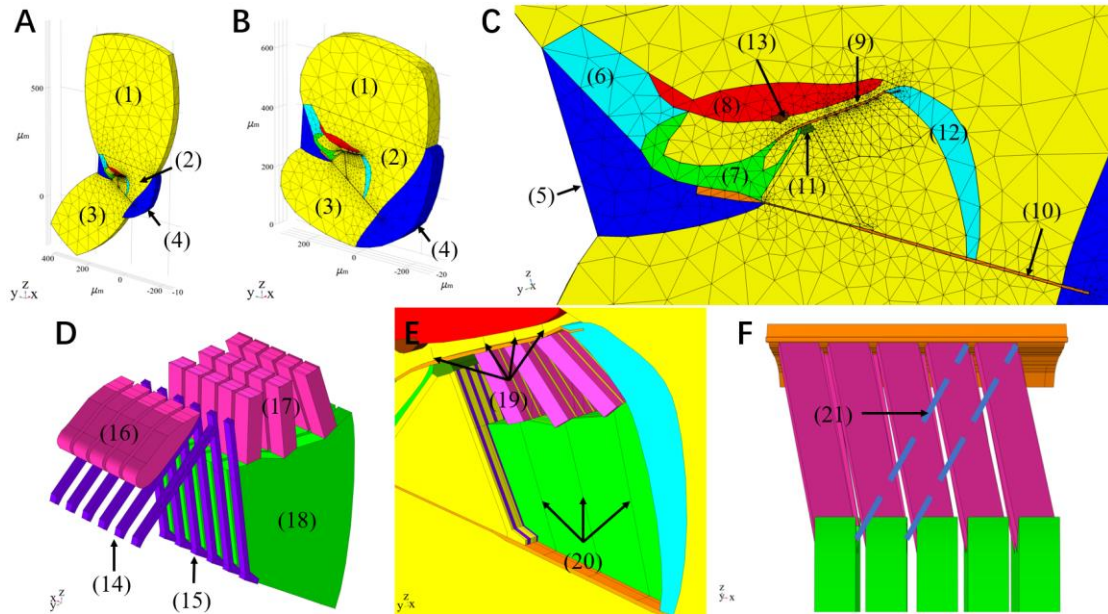
155

156

Table 1 Continuity in the models

Components (abbreviation)	Continuity	Components (abbreviation)	Continuity
Scala vestibuli (SV)	Yes	Hensen stripe	Yes
Scala media (SM)	Yes	Pillar cell head (PC)	Yes
Scala tympani (ST)	Yes	Outer pillar cell (OPC)	No
Spiral ligament	Yes	Inner pillar cell (IPC)	No
Spiral lamina (SLa)	Yes	Inner hair cell (IHC)	No
Spiral limbus	Yes	Outer hair cell (OHC)	No
Inner sulcus cells (ISC)	Yes	Stereocilia (St)	No
Tectorial membrane (TM)	Yes	Deiters cell (DC)	No
Reticular lamina (RL)	Yes	Deiters cell rod (DC rod)	No
Basilar membrane (BM)	Yes	Phalangeal processes (PhPs)	No
Hensen cell (HenC)	Yes		

157



158

159 Figure 1: Three-dimensional segmental models of the guinea pig cochlea. (A) The high-frequency model
 160 with a CF of 16 kHz. (B) The low-frequency model with a CF of 0.8 kHz. (C) Structure and mesh of the
 161 organ of Corti. (D) Discontinuous components in the organ of Corti. (E) Beam structures of some
 162 discontinuous components in the organ of Corti. (F) PhPs span 3 outer hair cells longitudinally. All
 163 structure names included in the model are numbered as follow: (1) Scala vestibuli, (2) Scala media, (3)
 164 Scala tympani, (4) Spiral ligament, (5) Spiral lamina, (6) Spiral limbus, (7) Inner sulcus cells, (8)
 165 Tectorial membrane, (9) Reticular lamina, (10) Basilar membrane, (11) Pillar cell head, (12) Hensen
 166 cells, (13) Hensen stripe, (14) Inter pillar cells, (15) Outer pillar cells, (16) Inter hair cells, (17) Outer
 167 hair cells, (18) Deiters cells, (19) Stereocilia, (20) Deiters rods, (21) Phalangeal processes. Yellow
 168 segments denote fluid elements, black and blue lines denote beam elements, and the rest denote solid
 169 elastic elements.

170 2.2 Boundary conditions

171 In this work, both models used the same boundary conditions. The two ends of the
 172 basilar membrane were connected with the spiral lamina and the spiral ligament. The
 173 boundary conditions are more complicated and depend on the adjacent tissue and fiber
 174 structure. Ni et al. (2013) showed that boundary conditions at both ends of the basilar
 175 membrane have little effect on the fluid coupling and coupled response. Therefore, we
 176 fixed the spiral ligament and spiral lamina, corresponding to the tightening of the basilar
 177 membrane on both ends, which is consistent with Steele and Puria (2005) and Ni et al.
 178 (2016).

179 The solid surface was set as a continuous periodic condition to simulate their movement

180 under a periodic arrangement. This boundary condition makes the displacement of the
 181 two sides of the boundary always equal, as,

$$u(x_d) = u(x_s), \quad (2)$$

182 where u is the displacement of solid, x_d and x_s are corresponding positions on both sides
 183 of the model. The effect of this boundary condition was discussed in Appendix I. The
 184 fluid was set to be no-stress boundary so that the total surface stress was zero, as,

$$[-p_t \mathbf{I} + \mu(\nabla \mathbf{u}_t + (\nabla \mathbf{u}_t)^T) - (\frac{2\mu}{3} - \mu_B)(\nabla \mathbf{u}_t) \mathbf{I}] \mathbf{n} = 0, \quad (3)$$

185 where p_t is the total acoustic pressure, \mathbf{u}_t is the total acoustic velocity, μ is the dynamic
 186 viscosity, μ_B is the bulk viscosity, \mathbf{I} is the second-order identity tensor, and \mathbf{n} is the
 187 normal direction. The no-stress boundary condition can simulate the longitudinal
 188 pressure release of the fluid when the organ of Corti moves. For example, when the
 189 organ of Corti moves, the volume of fluid in the SV and ST will change, which will
 190 change the pressure. If there were no such setting, this pressure change would restrict
 191 the movement of the organ of Corti. The effects of this boundary condition are
 192 discussed in Appendix II.

193 All contact surfaces between fluid and solid in the models were set as Thermoviscous
 194 Acoustic-Structure Boundary, which includes the coupling between the discontinuous
 195 structure and the fluid inside the organ of Corti. This coupling is described in the
 196 frequency domain as,

$$u_{t,\text{fluid}} = i\omega u_{\text{solid}} \quad (4)$$

197 where $u_{t,\text{fluid}}$ is the total fluid velocity, and u_{solid} is the solid displacement. This coupling
 198 ensures stress being continuous across the fluid-structure interface. Spatial continuity
 199 of displacement is enforced at the connection nodes between the beam and solid
 200 elements by,

$$\mathbf{u}_b = \mathbf{u}_s, \quad (5)$$

201 where \mathbf{u}_b and \mathbf{u}_s are the displacement of beam and solid, respectively. Since the beam
 202 elements in finite element models do not feature actual surfaces to interact with the

203 surrounding domain, fluid–structure interaction conditions do not apply to beams.

204 **2.3 Material properties**

205 Material properties of each structure are listed in Table 2 and Table 3. To adjust the
206 resonance frequency to be consistent with the defined characteristic frequency, the
207 stiffness of some components was adjusted to be consistent with measurements and
208 existed models (Cai and Chadwick, 2003; Steele and Puria, 2005; Zwislocki and
209 Cefaratti, 1989)

210 Orthotropic materials were used for TM, RL, and BM. Liu et al. (2008) showed that the
211 orthotropy ratio was 10 at the upper-middle turn of the cochlea and 68 at the base. They
212 pointed out that the value may vary along the length of the cochlea. The guinea pig
213 cochlea was 18.5 mm long, and the characteristic frequency at the base, f_B , was 44 kHz
214 (Fernandez, 1952). The characteristic frequency of the guinea pig cochlea exponentially
215 decreases from the base to the apex (Greenwood, 1990; Nuttall et al., 1999), as

$$CF(x) = f_B e^{-x/l}, \quad (6)$$

216 where x is the distance to the base, and l is the characteristic frequency distribution
217 scale, which was set to 3.8 mm in our work. The location with a characteristic frequency
218 of 0.8 kHz was then calculated to be about 15.2 mm away from the base, close to the
219 cochlea upper-middle turn. Meanwhile, the 16 kHz position is 3.8 mm away from the
220 base. Therefore, the orthotropy ratio was set to 10 for the low-frequency model and 40
221 for the high-frequency model.

222 The density of all components in the model was the same as water, 1000 kg/m^3 .
223 Poisson's ratio, ν , had a linear relationship with Young's modulus, E , as $\nu=1/2-E/6/K$,
224 where $K=1 \text{ GPa}$. The damping was included in the stiffness matrix as a loss factor of
225 0.1. The fluid was incompressible with a dynamic viscosity of 1 mPa s .

226

227

228

Table 2 Material properties of orthotropic materials in the model

Components	Parameter	Low-frequency model	High-frequency model
Tectorial membrane	Young's modulus [Pa]	$E_{XX}: 4e3$	$E_{XX}: 1.2e5$
		$E_{YY}: 4e4$	$E_{YY}: 4.8e6$
		$E_{ZZ}: 4e4$	$E_{ZZ}: 4.8e6$
	Shear modulus [Pa]	$G_{XY}: 2e3$	$G_{XY}: 6e4$
		$G_{YZ}: 2e4$	$G_{YZ}: 2.4e6$
		$G_{XZ}: 2e3$	$G_{XZ}: 6e4$
	Poisson's ratio	$V_{XY}: \frac{1}{10} \left(\frac{1}{2} - \frac{E_{YY}}{6K} \right)$	$V_{XY}: \frac{1}{40} \left(\frac{1}{2} - \frac{E_{YY}}{6K} \right)$
		$V_{YZ}: \frac{1}{10} \left(\frac{1}{2} - \frac{E_{YY}}{6K} \right)$	$V_{YZ}: \frac{1}{40} \left(\frac{1}{2} - \frac{E_{YY}}{6K} \right)$
		$V_{XZ}: \frac{1}{2} - \frac{E_{YY}}{6K}$	$V_{XZ}: \frac{1}{2} - \frac{E_{YY}}{6K}$
	Reticular lamina	Young's modulus [Pa]	$E_{XX}: 3e8$
$E_{YY}: 3e9$			$E_{YY}: 3.6e11$
$E_{ZZ}: 3e9$			$E_{ZZ}: 3.6e11$
Shear modulus [Pa]		$G_{XY}: 1e8$	$G_{XY}: 3e9$
		$G_{YZ}: 1e9$	$G_{YZ}: 1.2e11$
		$G_{XZ}: 1e8$	$G_{XZ}: 3e9$
Poisson's ratio		$V_{XY}: \frac{1}{10} \left(\frac{1}{2} - \frac{E_{YY}}{6K} \right)$	$V_{XY}: \frac{1}{40} \left(\frac{1}{2} - \frac{E_{YY}}{6K} \right)$
		$V_{YZ}: \frac{1}{10} \left(\frac{1}{2} - \frac{E_{YY}}{6K} \right)$	$V_{YZ}: \frac{1}{40} \left(\frac{1}{2} - \frac{E_{YY}}{6K} \right)$
		$V_{XZ}: \frac{1}{2} - \frac{E_{YY}}{6K}$	$V_{XZ}: \frac{1}{2} - \frac{E_{YY}}{6K}$
Basilar membrane		Young's modulus [Pa]	$E_{XX}: 6e5$
	$E_{YY}: 6e6$		$E_{YY}: 7.2e8$
	$E_{ZZ}: 6e6$		$E_{ZZ}: 7.2e8$
	Shear modulus [Pa]	$G_{XY}: 2e5$	$G_{XY}: 6e6$
		$G_{YZ}: 2e6$	$G_{YZ}: 2.4e8$
		$G_{XZ}: 2e5$	$G_{XZ}: 6e6$
	Poisson's ratio	$V_{XY}: \frac{1}{10} \left(\frac{1}{2} - \frac{E_{YY}}{6K} \right)$	$V_{XY}: \frac{1}{40} \left(\frac{1}{2} - \frac{E_{YY}}{6K} \right)$
		$V_{YZ}: \frac{1}{10} \left(\frac{1}{2} - \frac{E_{YY}}{6K} \right)$	$V_{YZ}: \frac{1}{40} \left(\frac{1}{2} - \frac{E_{YY}}{6K} \right)$
		$V_{XZ}: \frac{1}{2} - \frac{E_{YY}}{6K}$	$V_{XZ}: \frac{1}{2} - \frac{E_{YY}}{6K}$

Table 3 Material properties of isotropic materials in the model

Components	Low-frequency model	High-frequency model
	Young's modulus [Pa]	Young's modulus [Pa]
Spiral ligament	1e9	1.2e11
Spiral lamina	1e9	1.2e11
Spiral limbus	1e6	1.2e8
Inner sulcus cell	3e3	3.6e5
Hensen stripe	3e3	3.6e5
Hensen cell	3e3	3.6e5
Deters cell	3e3	3.6e5
Deiters cell rod	1e8	1.2e10
Pillar cell head	1e7	1.2e9
Outer pillar cell	1e8	1.2e10
Inner pillar cell	1e8	1.2e10
Inner hair cell	3e3	3.6e5
Outer hair cells	1e4	1.2e6
Stereocilia	1e5	1.2e7
Phalangeal processes	1e8	1.2e10

234 2.4 Mesh

235 The organ of Corti includes complex three-dimensional structures. The mesh of the
236 model was adjusted to ensure the quality of the elements, as shown in Figure 1. One-
237 dimensional beam elements were used for the stereocilia, phalangeal processes, and
238 Deiters rods. All other structures were meshed with tetrahedron elements. The organ of
239 Corti and the fluid area nearby were meshed densely, and the SV, SM, and ST areas
240 were meshed relatively loosely. The low-frequency model had 36,123 solid elements,
241 184 beam elements, and 39,106 fluid elements. The high-frequency model had 34,572
242 solid elements, 171 beam elements, and 38,292 fluid elements. The quadratic elements
243 were selected for solid and fluid. The axial displacement and twist are represented by
244 linear shape functions in the beam elements, while a cubic shape function represents
245 the bending.

246 **2.5 Stimulation of active response**

247 The active response was calculated by superimposing acoustic and OHCs excitations
248 to simulate the movement of the organ of Corti in the living cochlea. First, a sinusoidal
249 pressure difference was uniformly applied to the BM to simulate the excitation when
250 the sound propagates along the cochlea. Under the action of acoustic excitation, RL and
251 TM will undergo shearing motion, which determines the magnitude of the load at both
252 ends of the OHCs. The OHC force was calculated as follow (Geleoc et al., 1997;
253 Murakoshi et al., 2015)

$$F_{OHC}(x) = \frac{F_{max}}{1+e^{\alpha_1(x_1-x)}(1+e^{\alpha_2(x_2-x)})} \quad (7)$$

254 where F_{max} is the maximum load that can be generated at both ends of the OHC, set to
255 155 nN, x is the shear displacement of RL and TM, x_1 and x_2 are the displacements, at
256 which the setpoints of transition between states were set to 0.092 nm^{-1} and 0.038 nm^{-1} .
257 α_1 and α_2 are the displacement sensitivities of the transitions, set to 8.2 nm and 49 nm
258 (Geleoc et al., 1997).

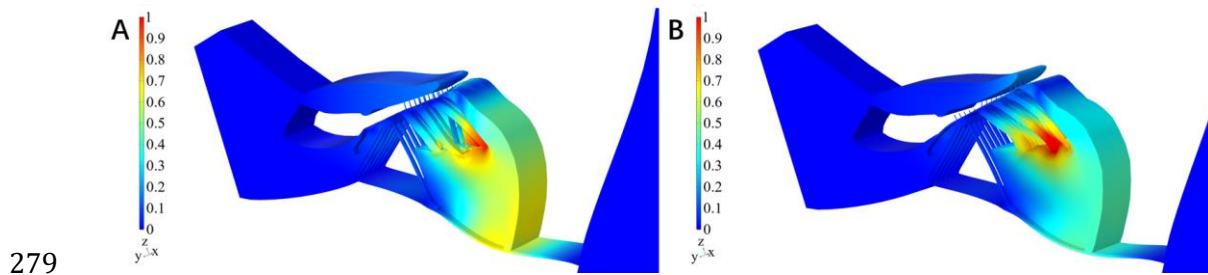
259 **3 Results**

260 **3.1 Hotspots in OHCs and DCs area**

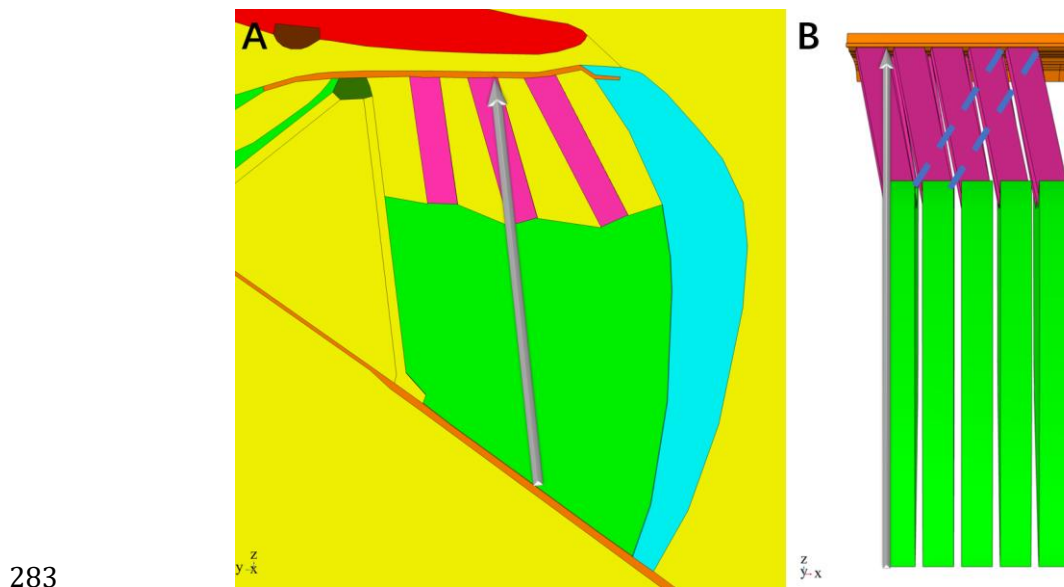
261 First, we calculated the active response of the organ of Corti based on the high- and
262 low-frequency model, as shown in Figure 2. When the BM moves towards the ST, the
263 shearing movement between the RL and TM causes OHCs to elongate. The location
264 with the most significant response is close to OHCs and DCs, as observed in the
265 experiments (Cooper et al., 2018).

266 As shown in Figure 3, a path was defined, similar to the definition in the experiment
267 (Cooper et al., 2018), to compare the model results with the experiment. This path starts
268 from the BM, passes through the DCs and OHCs area, and extends to the bottom of the
269 RL. The intersection between OHCs and Deiters cells that the path passes through
270 connects PhPs. The longitudinal displacement amplitude was calculated along the
271 defined path using the two models, as shown in Figure 4. It can be seen that the
272 longitudinal displacement amplitude of the two models reaches the maximum near the

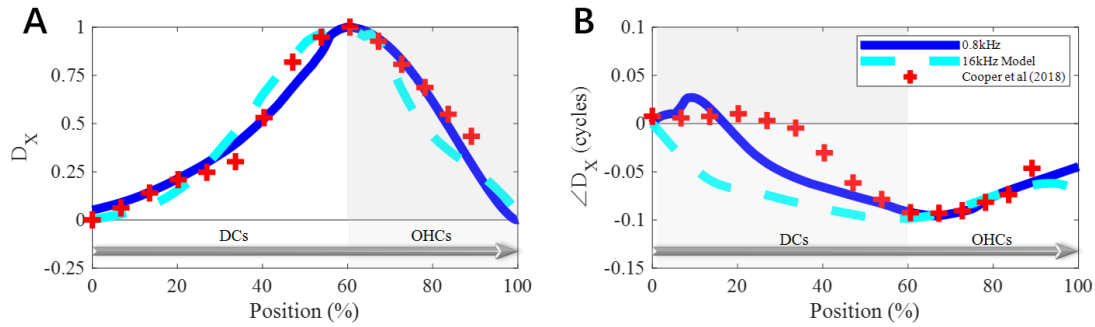
273 junction of DCs and OHCs, while the response close to BM and RL is small.
 274 Furthermore, the phase of DCs and OHCs is different from BM, consistent with the
 275 measured results in the experiment. Our model demonstrates how hotspot vibrations
 276 could be observed in the low-frequency region. **It can be seen that the response**
 277 **amplitude of the low-frequency model is greater than that of the high-frequency model**
 278 **when driven by the same stimuli.**



280 Figure 2: The active responses calculated based on (A) the high-frequency model and (B) the low-
 281 frequency model. The amplitudes were normalized with respect to the maximum value, and the
 282 deformation was magnified by 300 and 5 times for better visualization.



284 Figure 3: Defined path, marked with a gray arrow, for calculating longitudinal displacements of different
 285 components in the organ of Corti. (A) Transverse view. (B) Longitudinal view.



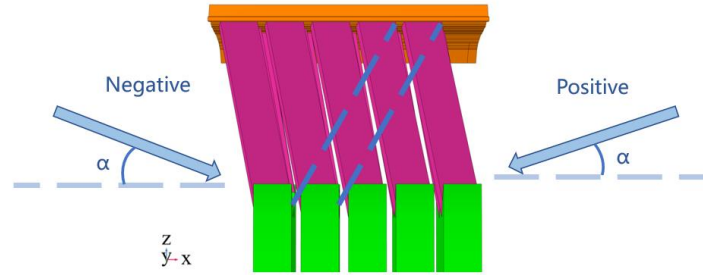
286

287 Figure 4: (A) The amplitude (A) and phase (B) of longitudinal displacement along the defined path. The
 288 amplitudes were processed with the min-max normalization method. The horizontal axis shows the
 289 percentage of the distance along the defined path.

290 3.2 The effect of viewing angle on the hotspot

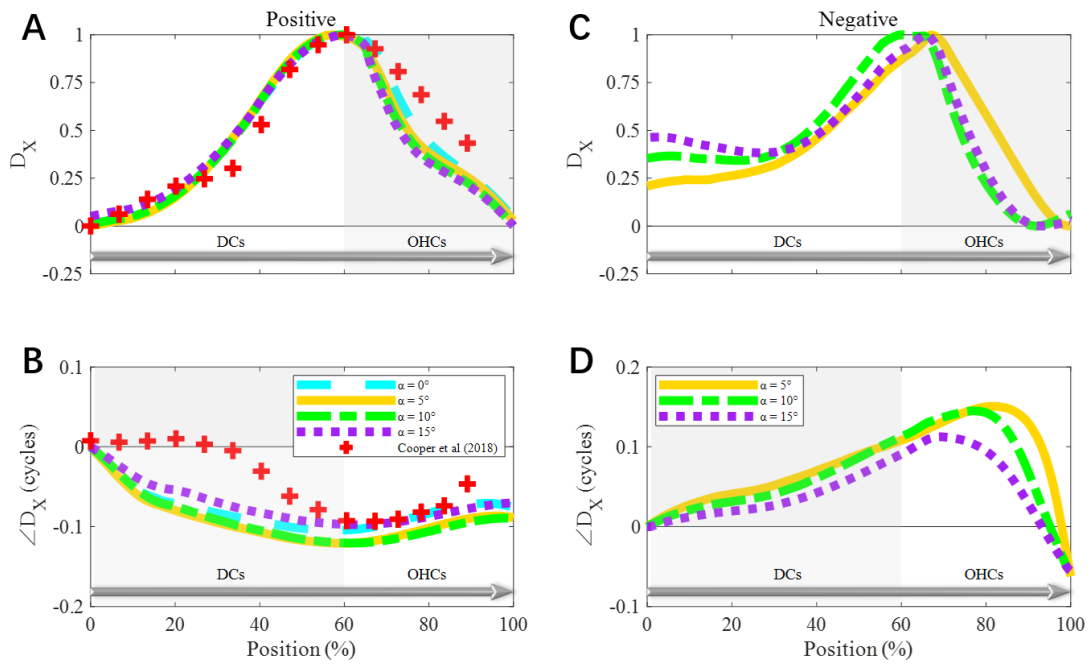
291 In the experimental study, the effect of different viewing angles on the results was
 292 predicted (Cooper et al., 2018). Based on the possible complex motion of the BM,
 293 Cooper et al. speculated: “Under the effect of the traveling wave, the phase of the
 294 hotspot will lead the BM when observing towards the apex and lag the BM when
 295 observing towards the base.” They then observed a similar phenomenon in their
 296 experiments.

297 Based on the high-frequency model, we also explored the influence of viewing angles
 298 on the hotspot. Referring to the method of Cooper et al. (2018), the viewing angle
 299 toward the cochlear apex was defined as “negative”, and toward the base as “positive”,
 300 as shown in Figure 5. Along with the two viewing angles, the calculated results of
 301 different deviation angles are shown in Figure 6. It can be seen that under the positive
 302 viewing angle, the results are in good agreement with the experimental results, and the
 303 hotspot phase lags to the BM. A similar phenomenon is also shown from the negative
 304 viewing angle, but the hotspot phase leads to the BM. Although the segmental model
 305 used in this study cannot include the effect of the traveling wave, the hotspot phase
 306 leading or lagging to the BM is still observed at different viewing angles. In this way,
 307 our results confirmed Cooper et al. predictions (4) and (5) (See supplementary
 308 information in Cooper et al. 2018). Since the deviation from different angles has little
 309 effect on the results, the result below focus on calculating the properties of the hotspot
 310 response using the positive viewing angle (specifically at $\alpha=0$).



311

312 Figure 5: Sketch of different viewing angles to the longitudinal direction.



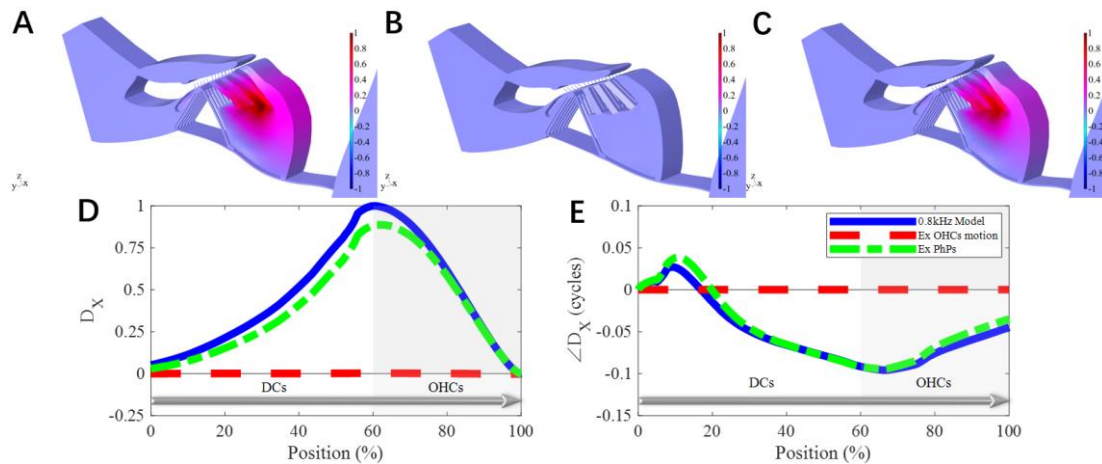
313

314 Figure 6: The positive (A, B) and negative (C, D) viewing angles, the amplitude (A, C), and phase (B,
 315 D) of longitudinal displacement along the defined path. The amplitudes were processed with the min-
 316 max normalization method. The phase results are calculated with reference to the position closest to the
 317 BM. The horizontal axis shows the percentage of the distance along the defined path.

318 3.3 Contributions of OHCs somatic motion and PhPs constraints to the hotspot

319 The experimental hypothesis is that the hotspot response is triggered by the activity of
 320 OHCs and is related to integrated structural constraints (Cooper et al., 2018). We
 321 recalculated the movement of the organ of Corti when PhPs or OHCs excitation was
 322 excluded, as shown in Figure 7. It can be seen that when the excitation of OHCs is
 323 stopped, the longitudinal deformation will disappear. When the PhPs are neglected,
 324 hotspot response amplitude is slightly decreased. It can be seen that the OHCs activity
 325 play an essential role in producing hotspot, and the existence of PhPs has further

326 promoted the occurrence of this phenomenon.



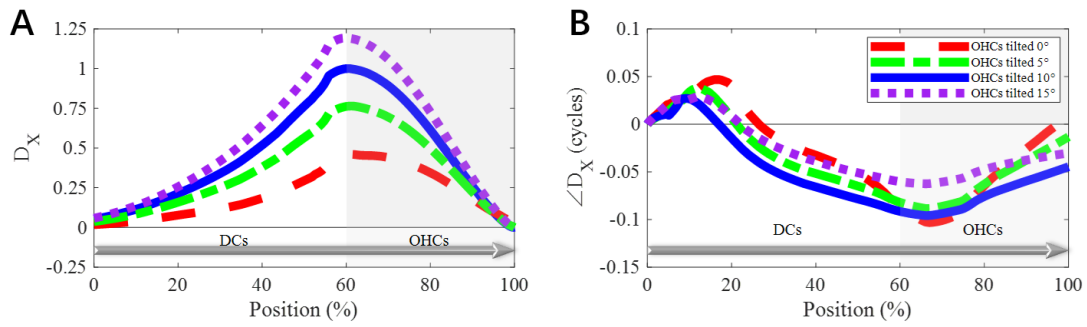
327

328 Figure 7: Deformation when (A) the model is fully active, (B) OHCs motility is excluded, and (C) PhPs
329 are eliminated. The longitudinal displacements in (A), (B), and (C) are normalized, and the deformation
330 is magnified 5 times (A, C) and 100 times (B) for better visualization. The amplitudes were processed
331 with the min-max normalization method. The (D) amplitude and (E) phase of DCs and OHCs
332 longitudinal displacement. The amplitudes were normalized with respect to the results of the 0.8 kHz
333 model. The horizontal axis shows the percentage of the distance along the defined path.

334 3.4 The effect of OHCs tilt angle on the hotspot

335 In our model, the OHCs are inclined 10° in the longitudinal direction. Existing studies
336 have shown that the inclination angle of OHCs in different species is different. For
337 example, the average inclination angle of gerbils is 5° , and that of chinchilla is 15°
338 (Yoon et al., 2011). It was also shown that even in the same species, the tilt angles at
339 different positions of the cochlea are different. For example, the tilt range in mice is
340 from 5° to 15° (Soons et al., 2015). Moreover, some results showed that OHCs and RL
341 occasionally tend to be perpendicular (Raphael et al., 1991; Soons et al., 2015).

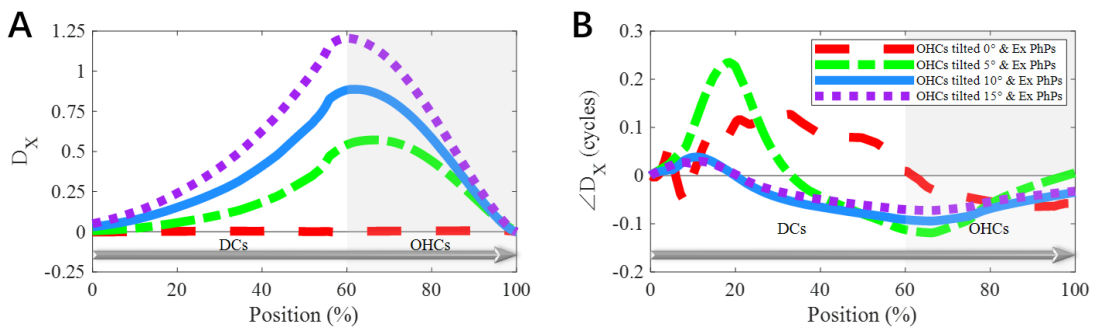
342 To explore the influence of different tilt angles on the hotspot response, we changed
343 the OHCs to be inclined 0° , 5° , 10° , and 15° longitudinally, as shown in Figure 8. The
344 greater the tilt angle of the OHCs along the longitudinal direction, the greater hotspot
345 amplitude. It is worth noting that when the OHCs are not tilted in the longitudinal
346 direction, the result also shows evident hotspot vibration. This may indicate that PhPs
347 played a more critical role in this phenomenon.



348

349 Figure 8: The amplitude (A) and phase (B) of DCs and OHCs longitudinal displacement when OHCs are
 350 inclined at different angles in the longitudinal direction. The amplitudes were normalized with respect to
 351 results when OHCs tilt 10°. The horizontal axis shows the percentage of the distance along the defined
 352 path.

353 We also explored the role of PhPs on hotspots when the OHCs inclined at different
 354 angles, as shown in Figure 9. If there were no PhPs, hotspot vibration will still occur
 355 when OHCs are tilted longitudinally, even if the tilt angle is slight. But when the OHCs
 356 are not inclined in the longitudinal direction, the hotspot will disappear without PhPs.

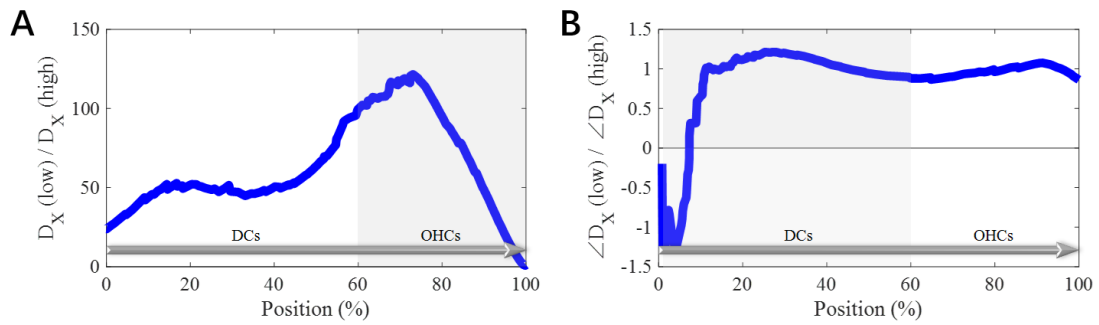


357

358 Figure 9: The amplitude (A) and (B) phase of DCs and OHCs longitudinal displacement when PhPs are
 359 excluded and OHCs inclined at different angles in the longitudinal direction. The amplitudes were
 360 normalized with respect to results when the OHCs tilted 10°. The horizontal axis shows the percentage
 361 of the distance along the defined path.

362 3.5 The effect of PhPs longitudinal span on the hotspot

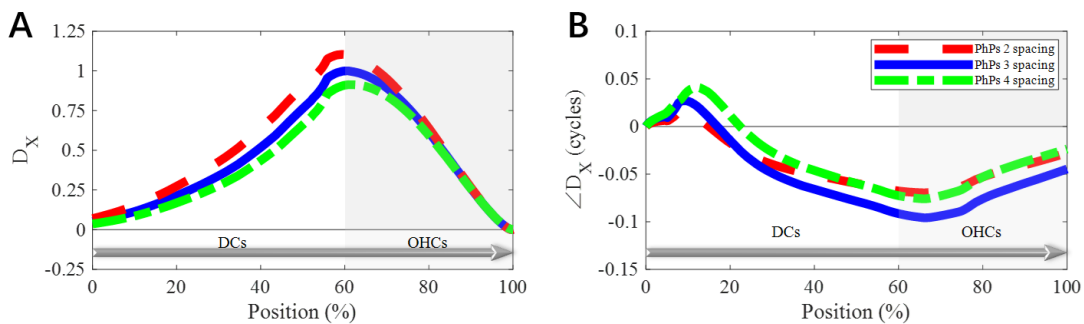
363 We first compared the hotspot responses of the high- and low-frequency models with
 364 the same PhPs span, 3 OHCs, as shown in Figure 10. It can be seen that the response
 365 amplitude of the low-frequency model is much greater than that of the high-frequency
 366 model.



367

368 Figure 10: Comparison of DCs and OHCs (A) longitudinal displacement and (B) phase calculated with
 369 the low- and high-frequency models. The horizontal axis shows the percentage of the distance along the
 370 defined path.

371 Existing studies have observed geometric parameters in different species and found
 372 some differences. For example, the longitudinal span of PhPs is 2 OHCs spacing in
 373 gerbils (Karavitaki and Mountain, 2007), 3 in mouse (Soons et al., 2015), and 4-5 in
 374 mole rat (Raphael et al., 1991). Moreover, the longitudinal spacing of OHCs in these
 375 species is close, with a distance of about $10\ \mu\text{m}$. Therefore, we used the guinea pig
 376 model to study the effect of different longitudinal spans of PhPs on the hotspot response,
 377 as shown in Figure 11. It can be seen that the hotspot response is more significant when
 378 the PhPs span is shorter.



379

380 Figure 11: The amplitude (A) and phase (B) of DCs and OHCs longitudinal displacement when PhPs
 381 span different spacing along the longitudinal direction. The amplitudes were normalized with respect to
 382 results when PhPs span 3 OHCs. The horizontal axis shows the percentage of the distance along the
 383 defined path.

384 4 Conclusion and discussion

385 Two three-dimensional models of the organ of Corti were developed, describing the
 386 high- and low- frequency regions in the cochlea, which are not a simple spatial

387 stretching but included several different continuity conditions based on the natural
388 physiological structure. Although the model constructed using beam elements could
389 reduce the amount of calculation, it cannot describe the local response of the organ of
390 Corti in detail. A three-dimensional model allows the simulation of the integrated
391 spatial coupling between solid and fluid. Compared with the two-dimensional model,
392 the three-dimensional model considers the longitudinal tilt of OHCs and the structure
393 of PhPs, which makes it possible to study the influence of these factors on the hotspot
394 phenomenon.

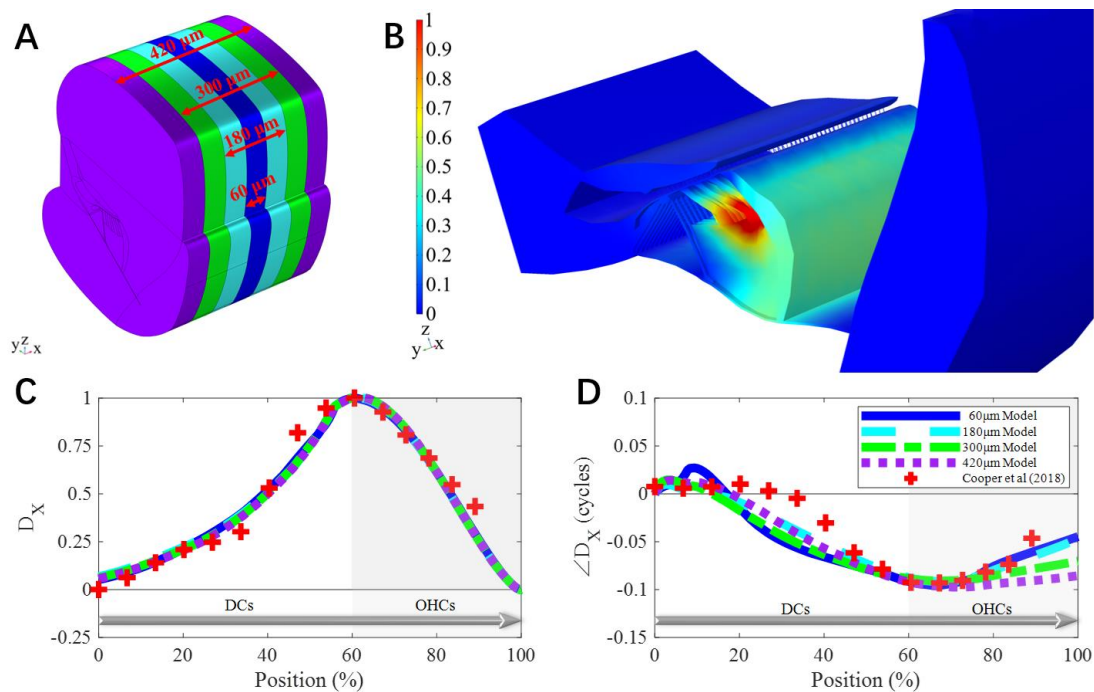
395 It should be noted that even without the traveling wave, our model still validated the
396 predictions (4) and (5) mentioned above and reproduced similar phenomena to
397 experiments, including the vibrational morphology of the hotspot and phase lead or lag
398 depending on the viewing angle. Therefore, we hypothesize that the hotspot is a locally
399 originated phenomenon in the cochlea, but the traveling wave further enhances the
400 response of the hotspot to low-frequency excitation.

401 When the OHCs activity was excluded, the longitudinal deformation of the OHCs and
402 DCs area was significantly reduced, confirming that the activity of OHCs induces the
403 hotspot vibration (Dewey et al., 2021). In addition, the results show that the longitudinal
404 structural constraints of PhPs also slightly contribute to the formation of the hotspot.
405 Our results confirm that the hotspot occurs in both high-frequency and low-frequency
406 regions.

407 In summary, the movement of OHCs triggers the hotspot and the PhPs structural
408 constraints promote this phenomenon, which supports the experimental hypothesis
409 (Cooper et al., 2018). The hotspot phenomenon occurs regardless of the tilt angle of the
410 OHCs, a larger tilt angle induces a larger amplitude. When OHCs are not inclined, the
411 structural constraints of PhPs become the main reason and a shorter PhPs span will
412 induce a larger hotspot amplitude.

413 **Appendix I: Effects of Periodic Condition**

414 Periodic conditions were assumed along the longitudinal solid side boundaries. To
 415 verify the effect of periodic conditions on the hotspot response, we extended the
 416 existing model longitudinally to 60 μm , 180 μm , 300 μm , and 420 μm , that is, the
 417 original model extended the same length along both sides of the longitudinal direction,
 418 as shown in Figure I.A, and recalculated the movement of the organ of Corti. It can be
 419 seen from Figure I.B that the movement of the organ of Corti has not changed after the
 420 model is extended. Figures I.C and D show no change in the hotspot response after the
 421 model is extended.



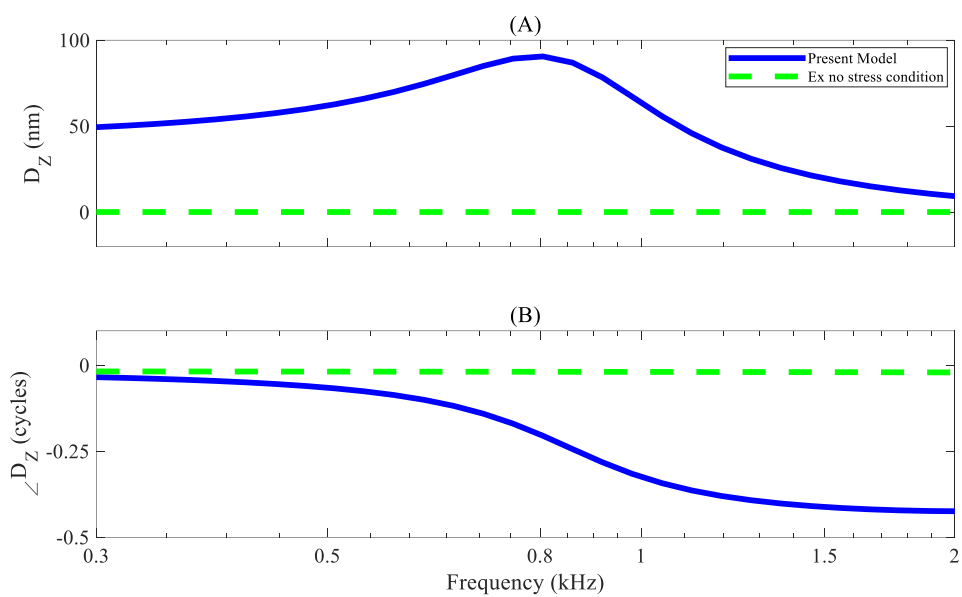
422

423 Figure I: (A) Models with different lengths in the longitudinal direction. The blue denotes 60 μm long
 424 (the original length), red 180 μm , green 300 μm , and purple 420 μm . (B) The active response of the organ
 425 of Corti when the model was extended to 420 μm . The amplitudes were processed with the min-max
 426 normalization method. The amplitude (C) and phase (D) of DCs and OHCs longitudinal displacement
 427 when the model is extended with different lengths. The amplitudes were normalized with respect to
 428 results when the model was 60 μm thick in the longitudinal direction. The horizontal axis shows the
 429 percentage of the distance along the defined path.

430

431 **Appendix II: Effects of no-stress condition**

432 The two sides of the fluid area along the longitudinal direction of the model were set as
433 no stress conditions. Under the existing model settings, loads of different frequencies
434 are applied to the bottom of the BM. The movement of the BM is shown in Figure II.
435 The result showed a steady upward trend from low to high frequency, reaching the
436 maximum value at 0.8 kHz, and rapidly decreasing. The model can simulate the
437 response trend in the cochlea. But when the no-stress condition is eliminated, this trend
438 does not appear.



439

440 Figure II: (A) Amplitude and (B) phase of the BM vertical displacement with and without no-stress
441 conditions.

442

443 **Author Contributions**

444 GN, JL, YB, and SJE contributed to the conception and design of the work, drafting
445 and revising the manuscript. JL, GN, YB, QC, and SZ participated in modeling work.
446 All authors agreed to submit the manuscript in its current state and agree to be
447 accountable for all aspects of the work.

448 **Acknowledgments**

449 The work was supported by grants from the National Natural Science Foundation of
450 China (81971698) and the Beijing-Tianjin-Hebei Basic Research Cooperation Project
451 (18JCZDJC45300).

452 ¹ Alec Salt's laboratory: <http://oto2.wustl.edu/cochlea/> (Last viewed June 4, 2016).

453 **References**

- 454 Bohnke, F., von Mikusch-Buchberg, J., Arnold, W., 1999. Active nonlinear mechanics
455 of the organ of Corti including the stereocilia-tectorial membrane complex. *Orl-Journal*
456 *for Oto-Rhino-Laryngology and Its Related Specialties* 61(5), 311-317.
457 <https://doi.org/10.1159/000027689>.
- 458 Cai, H.X., Chadwick, R., 2003. Radial structure of traveling waves in the inner ear.
459 *Siam Journal on Applied Mathematics* 63(4), 1105-1120, Pii s0036139901388957.
460 <https://doi.org/10.1137/s0036139901388957>.
- 461 Cai, H.X., Shoelson, B., Chadwick, R.S., 2004. Evidence of tectorial membrane radial
462 motion in a propagating mode of a complex cochlear model. *Proceedings of the*
463 *National Academy of Sciences of the United States of America* 101(16), 6243-6248.
464 <https://doi.org/10.1073/pnas.0401395101>.
- 465 Cooper, N.P., Vavakou, A., van der Heijden, M., 2018. Vibration hotspots reveal
466 longitudinal funneling of sound-evoked motion in the mammalian cochlea. *Nature*
467 *Communications* 9, 12, 3054. <https://doi.org/10.1038/s41467-018-05483-z>.
- 468 Dewey, J.B., Altoe, A., Shera, C.A., Applegate, B.E., Oghalai, J.S., 2021. Cochlear
469 outer hair cell electromotility enhances organ of Corti motion on a cycle-by-cycle basis
470 at high frequencies in vivo. *Proceedings of the National Academy of Sciences of the*
471 *United States of America* 118(43), e2025206118.
472 <https://doi.org/10.1073/pnas.2025206118/-/DCSupplemental>.
- 473 Fallah, E., Strimbu, C.E., Olson, E.S., 2021. Nonlinearity of intracochlear motion and
474 442 local cochlear microphonic: Comparison between guinea pig and gerbil. *Hearing*
475 *Research* 405, 108234. <https://doi.org/10.1016/j.heares.2021.108234>.
- 476 Fernandez, C., 1952. DIMENSIONS OF THE COCHLEA (GUINEA PIG). *Journal of*
477 *the Acoustical Society of America* 24(5), 519-523. <https://doi.org/10.1121/1.1906929>.

478 Geisler, C.D., Sang, C., 1995. A cochlear model using feed-forward outer-hair-cell
479 forces. *Hearing Research* 86(1-2), 132-146. [https://doi.org/10.1016/0378-](https://doi.org/10.1016/0378-5955(95)00064-b)
480 [5955\(95\)00064-b](https://doi.org/10.1016/0378-5955(95)00064-b).

481 Geleoc, G.S., Lennan, G.W., Richardson, G.P., Kros, C.J., 1997. A quantitative
482 comparison of mechano-electrical transduction in vestibular and auditory hair cells of
483 neonatal mice. *Proceedings. Biological sciences* 264(1381), 611-621.
484 <https://doi.org/10.1098/rspb.1997.0087>.

485 Greenwood, D.D., 1990. A cochlear frequency-position function for several species--
486 29 years later. *The Journal of the Acoustical Society of America* 87(6), 2592-2605.
487 <https://doi.org/10.1121/1.399052>.

488 He, W.X., Kemp, D., Ren, T.Y., 2018. Timing of the reticular lamina and basilar
489 membrane vibration in living gerbil cochleae. *Elife* 7, 17, e37625.
490 <https://doi.org/10.7554/eLife.37625>.

491 Karavitaki, K.D., Mountain, D.C., 2007. Imaging electrically evoked micromechanical
492 motion within the organ of corti of the excised gerbil cochlea. *Biophysical Journal* 92(9),
493 3294-3316. <https://doi.org/10.1529/biophysj.106.083634>.

494 Kelly, J.P., 1989. Cellular organization of the guinea pig's cochlea. *Acta oto-*
495 *laryngologica. Supplementum* 467, 97-112.

496 Kikuchi, T., Kimura, R.S., Paul, D.L., Adams, J.C., 1995. Gap junctions in the rat
497 cochlea: immunohistochemical and ultrastructural analysis. *Anatomy and embryology*
498 191(2), 101-118. <https://doi.org/10.1007/bf00186783>.

499 Lim, D.J., 1986. FUNCTIONAL STRUCTURE OF THE ORGAN OF CORTI - A
500 REVIEW. *Hearing Research* 22(1-3), 117-146. [https://doi.org/10.1016/0378-](https://doi.org/10.1016/0378-5955(86)90089-4)
501 [5955\(86\)90089-4](https://doi.org/10.1016/0378-5955(86)90089-4).

502 Liu, S., White, R.D., 2008. Orthotropic material properties of the gerbil basilar
503 membrane. *Journal of the Acoustical Society of America* 123(4), 2160-2171.
504 <https://doi.org/10.1121/1.2871682>.

505 Muller, M., 1996. The cochlear place-frequency map of the adult and developing
506 Mongolian gerbil. *Hearing Research* 94(1-2), 148-156. [https://doi.org/10.1016/0378-](https://doi.org/10.1016/0378-5955(95)00230-8)
507 [5955\(95\)00230-8](https://doi.org/10.1016/0378-5955(95)00230-8).

508 Murakoshi, M., Suzuki, S., Wada, H., 2015. All Three Rows of Outer Hair Cells Are
509 Required for Cochlear Amplification. *Biomed Research International* 2015, 12, 727434.
510 <https://doi.org/10.1155/2015/727434>.

511 Nam, J.-H., 2014. Microstructures in the Organ of Corti Help Outer Hair Cells Form
512 Traveling Waves along the Cochlear Coil. *Biophysical journal* 106(11), 2426-2433.
513 <https://doi.org/10.1016/j.bpj.2014.04.018>.

514 Nam, J.-H., Fettiplace, R., 2010. Force Transmission in the Organ of Corti
515 Micromachine. *Biophysical journal* 98(12), 2813-2821.
516 <https://doi.org/10.1016/j.bpj.2010.03.052>.

517 Ni, G., Elliott, S.J., 2013. Effect of basilar membrane radial velocity profile on fluid
518 coupling in the cochlea. *Journal of the Acoustical Society of America* 133(3), EL181-
519 EL187. <https://doi.org/10.1121/1.4789863>.

520 Ni, G., Elliott, S.J., Baumgart, J., 2016. Finite-element model of the active organ of
521 Corti. *Journal of the Royal Society Interface* 13(115), 20150913.
522 <https://doi.org/10.1098/rsif.2015.0913>.

523 Ni, G.J., Sun, L.Y., Elliott, S.J., 2017. A linearly tapered box model of the cochlea.
524 Journal of the Acoustical Society of America 141(3), 1793-1803.
525 <https://doi.org/10.1121/1.4977750>.

526 Nuttall, A.L., Guo, M.H., Ren, T.Y., 1999. The radial pattern of basilar membrane
527 motion evoked by electric stimulation of the cochlea. Hearing Research 131(1-2), 39-
528 46. [https://doi.org/10.1016/s0378-5955\(99\)00009-x](https://doi.org/10.1016/s0378-5955(99)00009-x).

529 Raphael, Y., Altschuler, R.A., 2003. Structure and innervation of the cochlea. Brain
530 Research Bulletin 60(5-6), 397-422. [https://doi.org/10.1016/s0361-9230\(03\)00047-9](https://doi.org/10.1016/s0361-9230(03)00047-9).

531 Raphael, Y., Lenoir, M., Wroblewski, R., Pujol, R., 1991. The sensory epithelium and
532 its innervation in the mole rat cochlea. The Journal of comparative neurology 314(2),
533 367-382. <https://doi.org/10.1002/cne.903140211>.

534 Ren, T.Y., He, W.X., Kemp, D., 2016. Reticular lamina and basilar membrane
535 vibrations in living mouse cochleae. Proceedings of the National Academy of Sciences
536 of the United States of America 113(35), 9910-9915.
537 <https://doi.org/10.1073/pnas.1607428113>.

538 Robles, L., Ruggero, M.A., 2001. Mechanics of the mammalian cochlea. Physiological
539 Reviews 81(3), 1305-1352.

540 Soons, J.A.M., Ricci, A.J., Steele, C.R., Puria, S., 2015. Cytoarchitecture of the Mouse
541 Organ of Corti from Base to Apex, Determined Using In Situ Two-Photon Imaging.
542 Jaro-Journal of the Association for Research in Otolaryngology 16(1), 47-66.
543 <https://doi.org/10.1007/s10162-014-0497-1>.

544 Steele, C.R., Baker, G., Tolomeo, J., Zetes, D., 1993. Electro-mechanical models of the
545 outer hair cell.

546 Steele, C.R., Lim, K.M., 1999. Cochlear model with three-dimensional fluid, inner
547 sulcus and feed-forward mechanism. Audiology and Neuro-Otology 4(3-4), 197-203.
548 <https://doi.org/10.1159/000013841>.

549 Steele, C.R., Puria, S., 2005. Force on inner hair cell cilia. International Journal of
550 Solids and Structures 42(21-22), 5887-5904.
551 <https://doi.org/10.1016/j.ijsolstr.2005.03.056>.

552 von Békésy, G., 1970. Travelling waves as frequency analysers in the cochlea. Nature
553 225(5239), 1207-1209. <https://doi.org/10.1038/2251207a0>.

554 Yoon, Y.J., Steele, C.R., Puria, S., 2011. Feed-Forward and Feed-Backward
555 Amplification Model from Cochlear Cytoarchitecture: An Interspecies Comparison.
556 Biophysical journal 100(1), 1-10. <https://doi.org/10.1016/j.bpj.2010.11.039>.

557 Zagadou, B.F., Barbone, P.E., Mountain, D.C., 2020. Significance of the Microfluidic
558 Flow Inside the Organ of Corti. Journal of Biomechanical Engineering-Transactions of
559 the Asme 142(8), 12, 081009. <https://doi.org/10.1115/1.4046637>.

560 Zetes, D.E., Tolomeo, J.A., Holley, M.C., 2012. Structure and Mechanics of Supporting
561 Cells in the Guinea Pig Organ of Corti. Plos One 7(11), e49338.
562 <https://doi.org/10.1371/journal.pone.0049338>.

563 Zwislocki, J.J., Cefaratti, L.K., 1989. Tectorial membrane II: Stiffness measurements
564 in vivo. Hearing Research 42(2), 211-227. [https://doi.org/https://doi.org/10.1016/0378-
565 5955\(89\)90146-9](https://doi.org/https://doi.org/10.1016/0378-5955(89)90146-9).

566