# Data-Driven Building Energy Modelling – Generalisation Potential of Energy Signatures Through Interpretable Machine Learning

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### Abstract

Building energy modeling based on data-driven techniques has been demonstrated to be effective in a variety of situations. However, the question about its limits in terms of generalization is still open. The ability of a machine-learning model to adapt to previously unseen data and function satisfactorily is known as generalization. Apart from that, while machine-learning techniques are incredibly effective, interpretability is required for a "human-in-the-loop" approach to be successful. This study develops and tests a flexible regression-based approach applied to monitored energy data on a Passive House building. The formulation employs dummy (binary) variables as a piecewise linearization method, with the procedures for producing them explicitly stated to ensure interpretability. The results are described using statistical indicators and a graphic technique that allows for comparison across levels in the building systems. Finally, suggestions are provided for further steps toward generalization in datadriven techniques for energy in buildings.

## 1. Introduction

Data-driven building energy modeling methods that use machine-learning techniques have been shown to be useful in a variety of applications (Hong et al., 2020), from design (Westermann & Evins, 2019) to operation (Manfren et al., 2020). As a result, they have the potential to become a key tool for accelerating the ongoing process of building stock decarbonisation (Norton et al., 2021; Tronchin, & Knight, 2016) as well as an integral part of innovative services and technologies (Farina et al., 1998; Manfren et al., 2021a). However, the question of whether data-driven approaches can be generalized is still being debated. The ability of a machine-learning model to adapt to previously unknown data and perform reasonably well, given specified performance criteria, is referred to as generalization. A simple example of generalization is a model trained on building energy consumption data over a period of time and then used to estimate energy consumption during a successive period of time. This is the counterfactual approach used in Measurement and Verification (M&V) protocols, which uses statistical indicators as model acceptability criteria during the calibration phase. A more ambitious form of generalization would be that of using data-driven methods on energy modeling problems involving sets of building with homogeneous characteristics. Using datadriven methods on energy modeling problems involving different sets of buildings with relatively similar characteristics would be a more ambitious type of generalisation.

In this research, we use regression models trained and tested on building energy signatures as a tool for addressing the generalization problem. In fact, methods based on energy signature (ISO, 2013) (i.e., energy divided by the number of operating hours in the time interval of the analysis, corresponding to an average power) are scalable (temporally and spatially) (Manfren et al., 2021b; Tronchin, 2021; Tronchin et al., 2018), can work with unstructured data (using clustering) (Pistore et al., 2019; Westermann et al., 2020) and provide results that are weather normalized (Fazeli et al., 2016). Additionally, energy signatures can be scaled according to the building's size (Pistore et al., 2019; Tronchin et al., 2016), to produce a performance comparison that is independent of the size. Further, regression-based approaches are considered interpretable machine learning techniques (ISO, 2020) because it is possible to predict how the model output will change in response to a change in input data or algorithmic parameters (i.e., the rationale behind model output and the algorithmic logic can be easily understood in human terms) (Fabbri et al., 2014 and 2021). In this study, we employ this technique to analyze monitored data from a Passive House building in the Province of Forlì-Cesena in northern Italy, with the goal of improving formulations at the state of the art while also considering generalization and interpretability issues (Tronchin, 2005 and 2021).

### 2. Methods

The regression model proposed in this research is a reformulation of the variable-based degree-days regression, originally proposed by Kissock et al. (2003) in their Inverse Modeling Toolkit (IMT), which has been included in ASHRAE 14:2014 (ASHRAE, 2014) and has been evolving steadily with different algorithmic formulations. Essentially, interpretable regression-based methods can be based on general piecewise linearization methods (Lin et al., 2013) and use dummy (binary variables) to handle non-linearities. Model formulation and calibration criteria are reported hereafter (Tronchin et al., 2021a and 2021b).

#### 2.1 Model Formulation

Separate sub-models (heating, base load and cooling), indicated in Table 1, are combined into a single model (which is the sum of the individual sub-models) by introducing additional variables (dummy, 0-1 binary variables) to the original datasets using rules, indicated in Table 2. The binary variables multiply the original variables and act as interaction terms. Two types of models are tested, type 1 and type 2. In the first case, the independent variable is outdoor air temperature, while, in the second case, the independent variables are outdoor air temperature and total solar radiation on horizontal surface. The dependent variables are the energy signatures calculated from the monitored data described in Section 3.

The rules provided hereafter in Table 2 can be applied both manually and in an automated way to the

dataset, for example, using ranges of balance-point temperature (change-points) for heating and cooling (Manfren et al., 2019).

Table 1 – Regression model formulation

| Mode      | Demand                                      | Sub-models  |                    |
|-----------|---|---|--------------------|
| Type<br>1 | Heating                                     | $q_h = a_0(X_h) + a_1(X_h\theta_e) + \varepsilon_h$   | (1)                |
|           | Base<br>load                                | $q_b = b_0(X_b) + b_1(X_b\theta_e) + \varepsilon_b$   | (2)                |
|           | Cooling                                     | $q_h = c_0(X_c) + c_1(X_c\theta_e) + \varepsilon_c$   | (3)                |
| Type<br>2 | Heating                                     | $q_h = a_0(X_h) + a_1(X_h\theta_e) + a_2(X_hI_{sol}) + \varepsilon_h$   | ) (4)              |
|           | Base<br>load                                | $q_b = b_0(X_b) + b_1(X_b\theta_e) + b_2(X_bI_{sol}) + \varepsilon_b$   | (5)                |
|           | Cooling q                                   | $c_h = c_0(X_c) + c_1(X_c\theta_e) + c_2(X_cI_{sol}) + c_2(X_cI_{sol})$ | ε <sub>c</sub> (6) |
| Table 2   | – Rules for d                               | ummy variable creation  |                    |
| Pula      | Descriptior                                 |   | Vari-<br>ables     |
| 1         | correspondi                                 | y demand is greater than 0 for the<br>ng sub-model (e.g., heating, cool-<br>load), then the dummy variable is   | Xh,<br>Xb,<br>Xc   |
| 2         | balance poi<br>heating base                 | oor air temperature is lower than<br>int temperature for heating (i.e.,<br>e temperature), the dummy varia-<br>ng is equal to 1.  | Xh                 |
| 3         | balance poi<br>cooling base                 | or air temperature is greater than<br>int temperature for cooling (i.e.,<br>e temperature), the dummy varia-<br>ng is equal to 1.   | Xc                 |
| 4         | ing, cooling<br>be coherent<br>for building | my variables (that partition heat-<br>g and base load demands) should<br>with the schedules of operation<br>g services (i.e., months of heating<br>system operation).   | Xh,<br>Xb,<br>Xc   |
| 5         | sumed to be                                 | y variables for base load are as-<br>1 in all the months (i.e., electricity<br>er demand are always present).   | Xb                 |

#### 2.2 Model Calibration Criteria

Following the indications proposed by state-of-theart Measurement and Verification (M&V) protocols, such as ASHRAE 14:2014 (ASHRAE, 2014), Efficiency Value Organization (EVO) IPMVP (EVO, 2003), and Federal Energy Management Program (FEMP) (FEMP, 2008), the thresholds of acceptability for regression models as calibrated with monthly data are reported in Table 3.

Table 3 – Model calibration criteria

| Data interval | Metric   | ASHRAE<br>Guidelines 14 | IPMVP | FEMP |  |
|---------------|----------|-------------------------|-------|------|--|
| Monthly       | NMBE     | ±5                      | ±20   | ±5   |  |
|               | Cv(RMSE) | 15                      | -     | 15   |  |

## 3. Case Study

The case study is Passive House building, located in the northern Italian province of Forlì-Cesena; the essential building data are reported in Table 4.

The building was monitored for three years and electric and thermal demand data were split by end use, as indicated in Table 5.

The modeling workflow pursued to test the models reported in Table 1 incrementally is set out in the following steps:

- 1. Initial training, year 1, 2.
- 2. Testing, year 3 (model created in step 1).
- 3. Retraining, year 1, 2 and 3.

The results obtained are reported hereafter in Section 4.

| Group       | Туре              | Unit                 | Design |
|-------------|-------------------|----------------------|--------|
| Geometry    | Gross volume      | m <sup>3</sup>       | 1557   |
|             | Net volume        | m <sup>3</sup>       | 1231   |
|             | Heat loss surface | m <sup>2</sup>       | 847    |
|             | area              | 111-                 | 047    |
|             | Net floor area    | m <sup>2</sup>       | 444    |
|             | Glazed area/total |                      |        |
|             | wall area ratio   | %                    | 22.5   |
|             | percentage        |                      |        |
|             | Surface/volume    | 1/m                  | 0.54   |
|             | ratio             | 1/111                | 0.54   |
| Envelope    | U value external  | W/(m <sup>2</sup> K) | 0.18   |
|             | walls             | vv/(iii ix)          | 0.10   |
|             | U value roof      | $W/(m^2K)$           | 0.17   |
|             | U value transpar- | $W/(m^2K)$           | 0.83   |
|             | ent components    | <b>vv</b> /(iii K)   | 0.00   |
| HVAC and    | Ground-source     |                      |        |
| DHW         | heat pump         |                      | 8.4    |
|             | (GSHP) -          | kW                   |        |
|             | Brine/Water Heat  |                      |        |
|             | Pump (B0/W35)*    |                      |        |
|             | Borehole heat ex- |                      |        |
|             | changer (2 dou-   | m                    | 100    |
|             | ble U boreholes)  |                      |        |
| On-site en- | Building Inte-    |                      |        |
| ergy pro-   | grated Photo-     |                      |        |
| duction     | Voltaic (BIPV) -  | kWp                  | 9.2    |
|             | Polycrystalline   |                      |        |
|             | silicon           |                      |        |
|             | Solar thermal -   |                      |        |
|             | Glazed flat plate | m <sup>2</sup>       | 4.32   |
|             | collector         |                      |        |
|             | Domestic hot      | m <sup>3</sup>       | 0.74   |
|             | water storage     |                      | 0.7 1  |

\* EN 14511 test condition in heating mode, brine at 0 °C and water 35 °C with supply-return temperature difference  $\Delta t$  = 10 °C.

#### Table 5 – Dataset used for modeling

| Data                | Enduse                  | Interval | Monitoring<br>period |
|---------------------|-------------------------|----------|----------------------|
| Electric            | Total                   | Monthly  | 3 years              |
|                     | HVAC, DHW               | Monthly  | 3 years              |
|                     | Appliances and lighting | Monthly  | 3 years              |
| Thermal en-<br>ergy | Heating                 | Monthly  | 3 years              |
|                     | Cooling                 | Monthly  | 3 years              |

## 4. Results and Discussion

In this section, the results of the model training and testing process are reported, indicating both numerical results represented by statistical indicators (Table 3) and visualization of energy signatures for the different models fitted.

## 4.1 Numerical Results of Regression Models

The results obtained are split with respect to the two types of models considered, namely type 1 and type 2.

#### 4.1.1 Model Type 1

It can be clearly seen that model type 1, after 2 years, obtains values for the indicators *NMBE* and Cv(RMSE) that make them acceptable as calibrated (Table 3), with the exception of electricity demand for HVAC and DHW and thermal demand for cooling. In these cases, the values are higher than 15 % for Cv(RMSE) but lower than 20 %.

Table 6 – Model type 1 – Initial training (year 1 and 2)

| Data     | End-use      | EN(M) | EN(P) | $R^2$ | NMBE  | Cv(RMSE) |
|----------|--------------|-------|-------|-------|-------|----------|
|          |              | kWh   | kWh   | %     | %     | %        |
| Electric | Total        | 23812 | 23510 | 84.77 | -1.27 | 12.59    |
|          | HVAC,<br>DHW | 8611  | 8499  | 91.05 | -1.30 | 17.99    |
|          | Appliances   | 15201 | 15202 | 70.27 | 0.01  | 10.12    |
| Thermal  | Heating      | 17761 | 17757 | 98.05 | -0.03 | 8.87     |
|          | Cooling      | 5054  | 5004  | 93.50 | -0.99 | 16.45    |

The model trained for the period indicated in Table 6 (first 2 years) is then tested for the third year of monitoring. In this case, we can see how, for model type 1, the statistical indicators in the testing phase are larger (i.e., the model performance is lower in terms of goodness of fit.

Table 7 - Model type 1 - Testing (year 3)

| Data     | End-use      | EN(M) | EN(P) | $\mathbb{R}^2$ | NMBE   | Cv(RMSE) |
|----------|--------------|-------|-------|----------------|--------|----------|
| _        |              | kWh   | kWh   | %              | %      | %        |
| Electric | Total        | 11318 | 10167 | 65.37          | -10.17 | 20.15    |
|          | HVAC,<br>DHW | 3659  | 3181  | 90.78          | -13.07 | 20.76    |
|          | Appliances   | 7659  | 7013  | 26.83          | -8.44  | 22.13    |
| Thermal  | Heating      | 6029  | 5460  | 85.28          | -9.53  | 21.17    |
|          | Cooling      | 1784  | 1841  | 63.23          | 3.19   | 20.21    |

Finally, models are retrained with the entire 3-year dataset, obtaining results that are slightly better compared to the ones presented in Table 6, but not largely different.

Table 8 - Model type 1 - Retraining (year 1, 2 and 3)

| Data     | End-use      | EN(M) | EN(P) | $R^2$ | NMBE  | Cv(RMSE) |
|----------|--------------|-------|-------|-------|-------|----------|
|          |              | kWh   | kWh   | %     | %     | %        |
| Electric | Total        | 35130 | 34819 | 84.41 | -0.88 | 12.12    |
|          | HVAC,<br>DHW | 12270 | 12139 | 91.23 | -1.07 | 17.35    |
|          | Appliances   | 22860 | 22868 | 67.34 | 0.04  | 10.56    |
| Thermal  | Heating      | 23790 | 23795 | 95.91 | 0.02  | 12.42    |
|          | Cooling      | 6838  | 6735  | 90.91 | -1.51 | 17.77    |

#### 4.1.2 Model Type 2

The same workflow presented for model type 1 in Section 4.1.1 is repeated here for model type 2. The results are reported in Tables 9, 10 and 11, respectively. In this case, we can see a moderate improvement for the model training (Table 9) and retraining (Table 11), but a much better performance of the models in the testing phase (Table 10). In general, model type 2 performs better than type 1.

| Data       | End-use        | EN(M)     | ) EN(P)   | $R^2$          | NMBE   | Cv(RMSE) |
|------------|----------------|-----------|-----------|----------------|--------|----------|
|            |                | kWh       | kWh       | %              | %      | %        |
| Electric   | Total          | 23812     | 23518     | 88.36          | -1.23  | 11.05    |
| _          | HVAC,<br>DHW   | 8611      | 8534      | 91.74          | -0.90  | 17.16    |
|            | Appliances     | 15201     | 15204     | 82.19          | 0.02   | 7.84     |
| Thermal    | Heating        | 17761     | 17759     | 98.95          | -0.01  | 6.50     |
|            | Cooling        | 5054      | 5229      | 93.54          | 3.46   | 18.34    |
| Table 10 – | Model type 2 - | - Testing | g (year 3 | 3)             |        |          |
| Data       | End-use        | EN(M)     | ) EN(P)   | $\mathbb{R}^2$ | NMBE   | Cv(RMSE) |
|            |                | kWh       | kWh       | %              | %      | %        |
| Electric   | Total          | 11318     | 10551     | 85.96          | -6.78  | 12.53    |
| _          | HVAC,<br>DHW   | 3659      | 3248      | 91.75          | -11.24 | 18.80    |
|            | Appliances     | 7659      | 7329      | 66.66          | -4.30  | 12.04    |
| Thermal    | Heating        | 6029      | 5828      | 94.13          | -3.59  | 13.52    |
|            | Cooling        | 1784      | 1964      | 85.58          | 10.10  | 16.66    |
| Table 11 – | Model type 2 - | - Retrair | ning (yea | ar 1, 2        | and 3) |          |
| Data       | End-use        | EN(M)     | ) EN(P)   | $\mathbb{R}^2$ | NMBE   | Cv(RMSE) |
|            |                | kWh       | kWh       | %              | %      | %        |
| Electric   | Total          | 35130     | 34847     | 89.75          | -0.81  | 10.16    |
| -          | HVAC,<br>DHW   | 12270     | 12200     | 92.41          | -0.57  | 16.56    |
|            | Appliances     | 22860     | 22870     | 84.05          | 0.05   | 7.60     |
| Thermal    | Heating        | 23790     | 23798     | 98.32          | 0.03   | 7.96     |
| _          | Cooling        | 6838      | 7002      | 91.61          | 2.39   | 17.04    |

Table 9 - Model type 2 - Initial training (year 1 and 2)

#### 4.2 Energy Signature Visualization

In this section, energy signatures are visualized for both electric and thermal data and divided by end use. Section 4.2.1 focuses on electricity data, while Section 4.2.2 focuses on thermal data.

#### 4.2.1 Energy Signatures – Electricity

The energy signature shapes shown in Fig. 1 for total electricity, Fig. 2 for electricity for HVAC and DHW, Fig. 3 for appliances and lighting, are substantially similar to a 5p or nearly 4p model according to the classification proposed by ASHRAE14:2014. The charts are used to compare models type 1 and 2 at multiple levels in the building

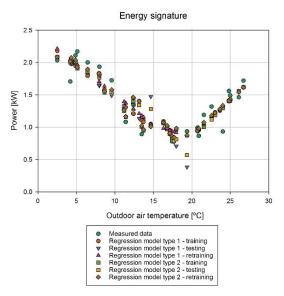


Fig. 1 – Energy signatures, measured data and regression models types 1 and 2 – Total electricity

The spread of data around the trend line is quite limited in Fig. 1 (total electricity) and Fig. 2 (electricity for HVAC and DHW), while it is more pronounced for Fig. 3 (appliances and lighting). In the latter, there is a lower temperature dependence (steepness of the trend line), compared to the other cases. However, the dependence is actually on daylight hours, which are correlated to temperature (lower temperatures correspond to winter condition where daylight hours are less and electric consumption for lighting is higher) and on the actual operation pattern, whose variability also determines the larger spread of values.

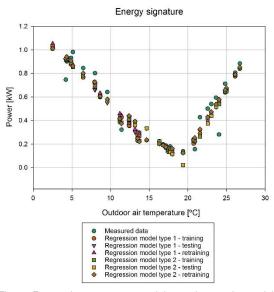


Fig. 2 – Energy signatures, measured data and regression models types 1 and 2 – Electricity for HVAC and DHW

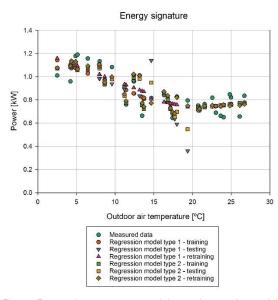


Fig. 3 – Energy signatures, measured data and regression models types 1 and 2 – Electricity for appliances and lighting

4.2.2 Energy Signatures – Thermal Energy

The energy signature shapes shown in Fig. 4 for thermal demand for heating and in Fig. 5 for thermal demand for cooling are essentially similar to a 3p model according to the classification proposed by ASHRAE14:2014. There are clearly some months when the technical systems do not produce either heating or cooling. Finally, it is possible to identify graphically, in an approximated way, the balancepoint temperature for heating and cooling, around 14 °C and 19 °C, respectively.

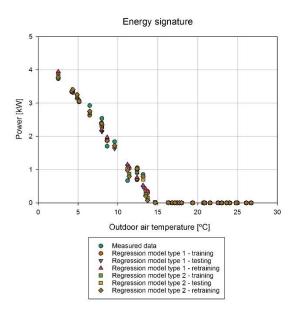


Fig. 4 – Energy signatures, measured data and regression models types 1 and 2 – Thermal energy for heating

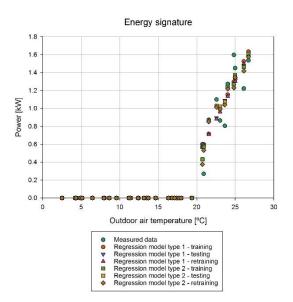


Fig. 5 – Energy signatures, measured data and regression models types 1 and 2 – Thermal energy for cooling

## 5. Conclusion

Machine learning-based building energy modeling techniques have proved to be effective in a range of applications. However, problems such as generalization and interpretability must be considered in order to enable the widespread adoption of these techniques. A piecewise linear regression model (interpretable) was proposed to analyze monitored data from a Passive House building, located in the northern Italian province of Forlì-Cesena. The building was monitored for three years, and this technique requires at least two years of monthly interval data to be used effectively. Nonetheless, the formulation provided is quite simple and flexible; the visualization of energy signatures can also help understanding the actual spread of data around the trend line, which represent outdoor air temperature dependence.

Further efforts involving the categorization of building data according to archetypes could be considered to address the generalization issue effectively. Finally, interpretability is extremely relevant because of the necessity to promote a "human-in-the loop" approach when using machine learning tools and the transparent link between regression model formulation and other analytical techniques at the state-of-the-art could represent an interesting research area from the perspective of future studies (Tronchin et al., 2020a and 2020b).

## Nomenclature

| Symbol                | Quantity  | Unit  |
|-----------------------|---|-------|
| a0,b0,c0              | regression coefficients, intercept  | kW    |
| a1,b1,c1              | regression coefficients, temperature dependence term  | kW/K  |
| a2,b2,c2              | regression coefficients, solar radia-<br>tion dependence term   | m²    |
| Cv(RMSE)              | coefficient of variation of RMSE  | -     |
| EN(M)                 | measured energy   | kWh   |
| EN(P)                 | predicted energy  | kWh   |
| Isol                  | total solar radiation on horizontal<br>surface (direct and diffuse) average<br>hourly value on monthly base | kW/m² |
| NMBE                  | normalized mean bias error (ex-<br>pressed in percentage)   | -     |
| <i>q</i> <sup>h</sup> | energy signature heating  | kW    |
| qь                    | energy signature base load  | kW    |

| qc    | energy signature cooling                            | kW |
|-------|---|----|
| $R^2$ | determination coefficient (expressed in percentage) | -  |
| Xh    | dummy variable (binary 0-1) heating                 | -  |
| $X_b$ | dummy variable (binary 0-1) base<br>load            | -  |
| Xc    | dummy variable (binary 0-1) cooling                 | -  |
| θε    | outdoor air temperature                             | ٥C |
| Eh    | error term heating                                  | kW |
| Eb    | error term base load                                | kW |
| Ec    | error term cooling                                  | kW |

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