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Vertical Integration of KTN on SOI Wafer

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Abstract:

Optical modulators play an important role in communication systems, and silicon has been a focal point in this field thanks to its compatibility with CMOS fabrication. However, silicon's lack of inherent electro-optic behavior makes it suboptimal for modulation purposes. Conversely, potassium tantalate niobate (KTN) materials boast an improved electro-optic coefficient, presenting a path for improving modulation efficiency. However, limited research exists on KTN materials due to the difficulties associated with their fabrication.

Here, a fabrication methodology is described for wafer-scale vertical integration of KTN material onto silicon-on-insulator (SOI) wafers. The resulting devices exhibit a propagation loss of 3.3dB mm^{-1} and a transition loss within the range of 0.46 to 0.76dB , which are in agreement with simulations. This method tackles the fabrication challenges and showcases the potential of utilising KTN as the integration material on silicon platform for future optical modulators.

1. Introduction

Optical modulators play an essential role in telecommunications due to the increasing usage of photonic devices in the industry, particularly in fiber-optics and data centre communications. The increasing needs for high-bandwidth transmission have propelled silicon-based optical modulator technology to a point where further performance improvements have become increasingly difficult to find, with driver-integrated devices reaching 224Gbps PAM-4 with the efficiency down to sub pJ/bit [1]. Due to the lack of a strong electro-optic effect in silicon, modulators have relied heavily on the plasma dispersion effect, primarily using carrier depletion. This has resulted in a large feature size, greater insertion loss, and limited modulation efficiency. This has motivated research on integrating other materials onto the silicon waveguide platform to realise optical modulation. Perovskite materials offer comparatively large electro-optic effects without the need for extrinsic dopings. This will avoid the absorption loss due to interactions with silicon dopants and provide increased modulation efficiency, allowing the required phase shift to be achieved at a shorter distance or with reduced drive power.

Silicon (Si) serves as the cornerstone material within the semiconductor industry due to its abundance and electronic characteristics. In the photonics field, its stable native cladding, silicon dioxide (SiO_2) with a high refractive index contrast facilitates high light confinement, enabling miniaturizing of devices [2]. Additionally, photonic components integrated onto a silicon-based platform allow the use of the same manufacturing processes as the CMOS technology, yielding better economics and wafers with fewer defects.

In recent years there has been research aiming to overcome the limitations of the plasma dispersion effect by integrating thin film lithium niobate (LN) and barium titanate (BTO) onto the silicon platform [3, 4]. Thin film LN modulators have demonstrated high-speed performance with efficiencies comparable with carrier-depletion-based devices while maintaining low propagation loss and a linear transfer function [5, 6]. BTO-based modulators have measured a Pockels coefficient orders of magnitude greater than LN-based devices and in some cases, enhanced efficiency over MOSCAP-based silicon devices, reaching as low as 0.2V cm [7–9]. Among perovskite materials, KTN, characterized by its chemical composition $\text{KTa}_{1-x}\text{Nb}_x\text{O}_3$ emerges as an alternative. In comparison to other studied perovskites such as KH_2PO_4 and BaTiO_3 , KTN stands out with the highest electro-optic coefficient of around 10^4pm V^{-1} (around two orders

47 higher than the current research-focused material - lithium niobate (LiNbO_2) [10, 11]). [12, 13]
 48 demonstrated an EO modulator using buried KTN waveguides with $< 0.05 \text{ dB mm}^{-1}$ propagation
 49 loss, and projected a 5 V mm modulation efficiency through electrode and waveguide optimization.
 50 Further improvements on EO modulation of KTN can be achieved by exploiting electric-field
 51 enhanced permittivity [14], incorporating nanodisordered regions [15], and adopting a proposed
 52 modulation maximisation model in [16].

53 This paper provides a first demonstration of passive KTN waveguides integrated into a
 54 silicon photonic platform monolithically. We demonstrate passive KTN waveguide losses at
 55 3.3 dB mm^{-1} , which compare well to initial demonstrations of BTO waveguides with suboptimal
 56 loss at 4 dB mm^{-1} [17]. Coupling structures to pass the light to and from silicon waveguides are
 57 also shown with a loss around $0.46 - 0.76 \text{ dB}$. This integration approach holds promise due to
 58 its capability to capitalise on the large electro-optics effect with promise of miniaturised device
 59 size and enhanced modulation efficiency, harness silicon fabrication technology, and seamless
 60 integration with other silicon-based devices.

61 2. Design and Fabrication

62 2.1. Design Concept

63 The design consists of a KTN waveguide on top of a silicon strip waveguide platform separated
 64 by a thin silicon dioxide layer. The silicon waveguide is tapered down to a tip, which forces the
 65 mode to be coupled to the KTN waveguide. The same structure performs the reverse function.
 66 Cutback loss test structures are used for characterising the propagation losses of KTN and silicon
 67 waveguides and their transition loss. A passive imbalanced Mach-Zehnder interferometer (MZI)
 68 structure consisting of a multi-mode interferometer (MMI)-based splitter and combiner, silicon
 69 waveguide bends, and two waveguide arms incorporating transition structures along with KTN
 70 waveguides is also present on the chip.

71 2.2. Si-KTN Waveguide Transition Modelling

72 Lumerical EME was used to model a single transition from silicon to KTN with a total length of
 73 $160 \mu\text{m}$. The target structure, depicted in Figure 1, features a KTN waveguide with a width and
 74 thickness of $1.5 \mu\text{m}$ and 360 nm respectively, an oxide thickness of 100 nm , and a silicon thickness
 75 of 220 nm . The silicon waveguides have a tip width of 150 nm tapered from a width of 450 nm
 76 over a distance of $150 \mu\text{m}$. The simulated transition loss at a wavelength of 1550 nm is 0.114 dB .

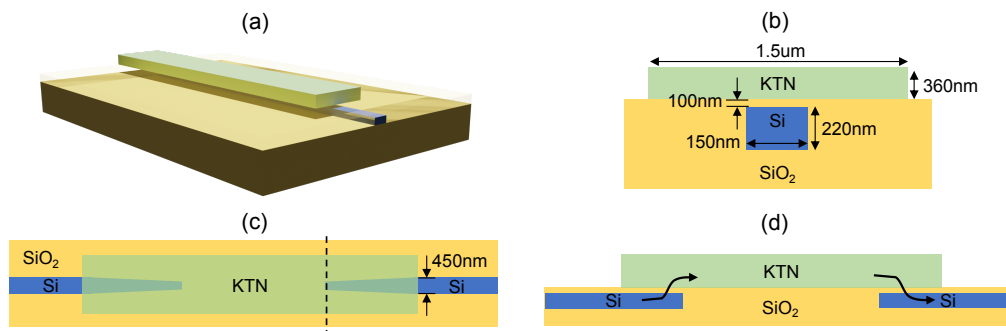


Fig. 1. (a) 3D schematics of the Si-KTN tapering section. (b) 2D cross-section (b) 2D top and (c) 2D yz-plane view of the target design transition structure.

77 2.3. Fabrication

78 Device fabrication was performed within the cleanroom facilities at the University of Southampton.
79 It started with 200mm SOI wafers with a 220nm silicon overlayer and a 2 μ m buried oxide (BOX)
80 layer. Grating couplers were etched 70nm into the silicon surface using a 248nm deep ultraviolet
81 (DUV) scanner lithography and inductively coupled plasma (ICP) etching. Strip waveguides
82 were defined by selectively etching the silicon layer completely through to the BOX layer. A
83 1 μ m silicon dioxide layer was deposited onto the wafer surface using plasma enhanced chemical
84 vapour deposition (PECVD). This layer was then planarised and thinned to leave a 100nm
85 silicon dioxide layer on top of the waveguide using chemical mechanical polishing (CMP). DUV
86 lithography was then used to produce a liftoff mask on the wafer to define regions where KTN
87 was required. A 360nm KTN layer was then deposited through RF sputtering at 200mm wafer
88 scale from a KTN target.

89 Initial recipe parameters were developed from previously reported work [18]. The sputtering
90 parameters were 200W RF power, pressure at 3mT, 100 sccm Ar flow, and 1 sccm O₂ flow. A
91 30nm silicon dioxide capping layer was deposited on top by RF sputtering with parameters of
92 90W RF power, pressure at 10mT, and 50 sscm Ar flow. After liftoff, DUV lithography and
93 ion-beam etching was used to define waveguides within the KTN regions with smooth sidewalls.
94 Microscopic and focused ion beam-scanning electron microscope (FIB-SEM) images of the
95 fabricated chips can be seen in Fig.2. Finally, the wafer was diced into chips and cleaned, ready
96 for testing.

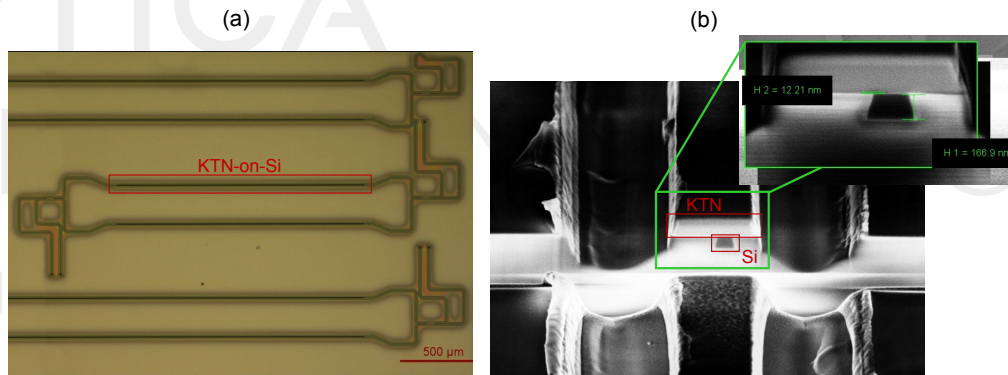


Fig. 2. (a) Microscopic view of MZI test structures. (b) An overview and close-up FIB-SEM images of the tapering section. It shows that the silicon is offset by 12.21nm, and the oxide layer between the two materials is polished away.

97 3. Result and Discussion

98 3.1. Passive Characterisation

99 Devices were characterised by passing light at a wavelength of 1550nm through and measuring
100 the power transmission level. Grating couplers were defined on each waveguide's input and output
101 sides to facilitate light coupling between optical fibers and the silicon chip. The propagation loss
102 within the KTN waveguides and the transition loss of the KTN-to-Si interfaces were investigated.
103 As depicted in Figure 3(a)(b), the propagation loss is approximately 0.45dB mm⁻¹ for silicon
104 (Si) and 3.3dB mm⁻¹ for KTN. The transition of a mode propagating within a silicon waveguide
105 to and from KTN induces a loss ranging from 0.46 to 0.76dB per transition, as illustrated in
106 Fig.3(c). The higher loss than anticipated from simulation can be attributed to over-polishing and
107 fabrication errors.

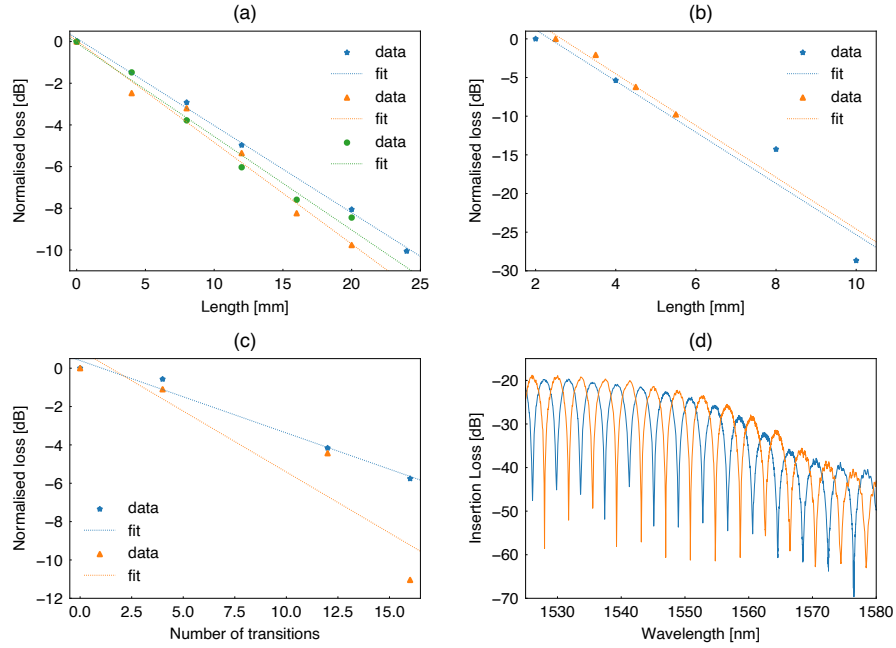


Fig. 3. Experimental results of passive characterisation of different waveguide structures across multiple chips. Normalised loss to the shortest length of (a) Si and (b) KTN. (c) Normalised loss to the smallest number of Si-KTN transitions. (d) Transmission spectrum of imbalanced MZI with KTN integrated into both arms.

108 Examination of Fig.2(c) reveals a lateral offset of the silicon within the transition region as
 109 as well as overpolishing during the CMP process, resulting in complete removal of the 100nm oxide
 110 between the KTN and silicon layer, and a thinning of the silicon layer to 170nm. Additionally,
 111 the absence of top cladding on the chips makes the structures susceptible to loss from particles
 112 gathering on the surface during the preparation, dicing, and measurement stages.

113 The impact of the imperfections was examined by simulating a reference device using
 114 parameters of those observed in the fabricated devices, followed by simulating deviations in the
 115 device parameters from this reference. The baseline simulation featured a silicon waveguide with
 116 a width of 450nm and height of 170nm. The silicon taper region spans 150 μ m, with a starting
 117 width of 450nm leading to a tip width of 202nm. A KTN waveguide, with a width of 1.5 μ m, and
 118 a height of 360nm, was defined directly on top of the silicon waveguide without the 100nm oxide
 119 layer.

120 From Fig. 4, it can be seen that the baseline loss is within the range of the measured
 121 experimental loss (grey shading), showing that our simulated and experimental results largely
 122 agree. The impact of the variation of the different design parameters can also be observed.
 123 Compared to the initially targeted thickness of 220nm, the fabricated thickness of 170nm results
 124 in an increase in loss of 0.26dB. The graph shows that decreasing the thickness and width of the
 125 KTN material, as well as decreasing the width of the silicon tip, leads to an increase in optical
 126 output. The graph indicates an almost linear relationship between the KTN thickness, silicon tip
 127 width, and the loss, having a similar gradient of approximately -0.0012dB/nm. Lateral offsets
 128 between the positions of the KTN waveguide and the silicon waveguide have minimal impact
 129 on the power output, indicating the structure is resilient to such misalignments. These insights
 130 offer a preliminary guide for optimizing the geometry of Si-KTN waveguides, providing valuable

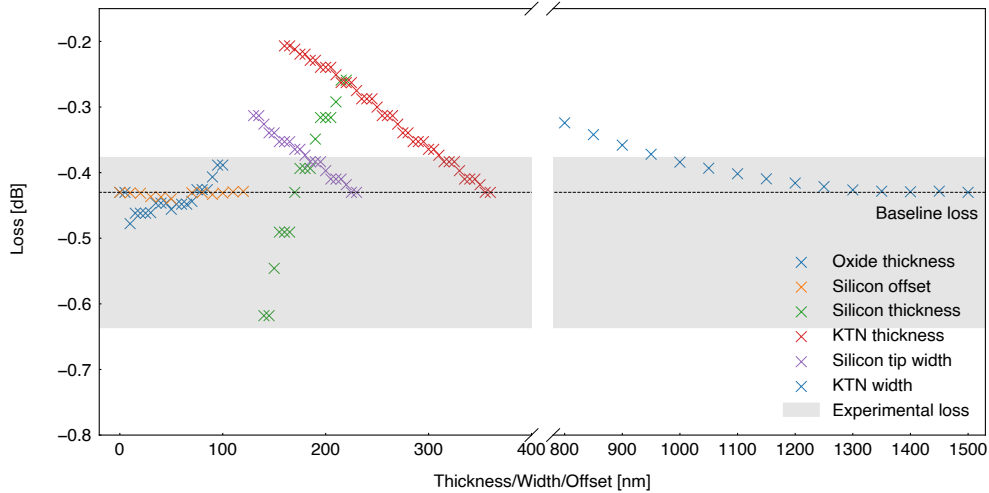


Fig. 4. Analysis of Si-KTN transition loss with various geometrical parameter variation around the baseline fabricated structure.

131 direction to reduce the loss.

132 The transmission spectrum of an imbalanced MZI with integrated KTN waveguides on both
 133 arms is illustrated in Figure 3(e). The extinction ratio (ER) exceeds 20dB, while the minimum
 134 insertion loss (IL_{\min}) is approximately 20dB. The high ER of the MZI, coupled with a large
 135 electro-optic coefficient of KTN, allows for a reduction in the required modulator driving voltage,
 136 thereby enhancing the overall modulation efficiency.

137 4. Conclusion

138 This study provided a first insight into the feasibility of wafer-scale integration of KTN waveguides
 139 onto a silicon photonics platform and lays the initial groundwork for realising high-speed and
 140 efficient optical modulators. Despite passive KTN waveguides exhibiting a loss around an order
 141 of magnitude higher than their passive silicon counterparts, they remain comparable to the
 142 doped silicon waveguides required to form a modulator. Furthermore, the high electro-optic
 143 coefficients surpass those of most other materials, meaning that the propagation length required
 144 can be short and, therefore, lower the overall loss. As an initial step in Si-KTN integration, the
 145 propagation loss of 3.7dB mm^{-1} in KTN is similar to that reported in BTO at 4dB mm^{-1} without
 146 optimisation [17]. Previous research [19] has demonstrated a considerable loss reduction in BTO
 147 to around 0.6dB mm^{-1} with loss source identification. Such research conducted on KTN can
 148 yield reductions in losses in a similar manner to that reported in BTO. In addition, the Si-KTN
 149 integration reported in this work has yet to undergo geometry and fabrication optimisation.

150 Despite KTN's potential as an alternative modulator material, certain challenges persist.
 151 Improving fabrication quality and tackling issues related to the high dielectric constant remain a
 152 priority. The latter poses challenges, such as the need for higher driving currents and increased
 153 time constants [4,20]. Nonetheless, with ongoing progress in fabrication technology, we anticipate
 154 a rising interest in exploring Si-KTN-based modulators.

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157 **Disclosures.** The authors declare no conflicts of interest.

158 **Data Availability Statement.** Data underlying the results presented in this paper are available in Ref. [21].

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