

Regenerative Nd:glass amplifier seeded with a Nd:fiber laser

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Wavelength tuning and broad-bandwidth operation of a passively mode-locked Nd:glass amplifier is demonstrated at 1060 μm . The oscillator pulses are used to seed a bulk regenerative Nd:glass amplifier, and 300-fs transform-limited pulses with an energy of 10 μJ are obtained after 31 round trips at a repetition rate of 500 Hz.

Passively mode-locked rare-earth-doped fiber lasers are a well-established medium for the generation of ultrashort pulses,¹⁻³ allowing one to generate pulses with a bandwidth as large as the bandwidth of the gain medium.⁴ In particular, Nd-doped fiber oscillators are of special interest because the oscillator pulses may be used in bulk-medium or high-power Nd:glass amplifier systems.⁵⁻⁷ In these applications, Nd:phosphate glass with a peak emission wavelength at 1.053 μm is preferred owing to its good thermal properties and low nonlinear refractive index. However, high-quality Nd:phosphate or fluoride fibers (with a similar peak emission wavelength) do not exist yet, and typical low-loss lead-glass or silica fibers emit at $\sim 1.06 \mu\text{m}$. We show here that in a highly nonlinear Nd:glass amplifier and the generation of subpicosecond transform-limited pulses with microjoule energies.

We used a lead-glass fiber consisting of a Schott F2/F7 glass combination doped with ≈ 3000 parts in 10^6 of Nd^{3+} as the oscillator in our experiments. The peak emission wavelength is 1.060 μm , and the nonlinear refractive index ($n_2 = 10^{-19} \text{ m}^2/\text{W}$) and the positive group-velocity dispersion (GVD) ($\beta_2 = 70,000 \text{ fs}^2/\text{m}$) of this material are approximately three times higher than those in a silica glass. The fiber length was 23 cm, and the core diameter was 5 μm . The fiber was pumped with a mixture of 752- and 799-nm beams from a krypton laser with absorbed pump powers of as much as 180 mW. The absorption length was ≈ 10 cm. Intracavity dispersion adjustment was achieved by using a single Brewster-cut ZnS prism pair, which provided a

negative GVD of 57,000 fs^2/m . Passive amplitude modulation in the cavity was obtained with nonlinear-polarization evolution,^{2,4} where passive mode locking was initiated with an acousto-optic modulator, which was switched off once pulses were generated. With the proper polarization setting, the oscillator remained stable for hours and required only small adjustments on a day-to-day basis. The oscillator cavity was thus of similar design as that in Ref. 2. In addition, a variable aperture was translated in front of the output coupler for spectral windowing.

With a 20% output coupler, we obtained a cw lasing threshold of < 5 mW of absorbed pump power, a maximum lasing power of 20 mW, and a slope efficiency of 11%. With a 50% output coupler, the slope efficiency and the maximum lasing power were higher by a factor of 2. The maximum cw mode-locked power was 12 mW, where the pulse repetition rate was 100 MHz. A minimum pulse width of 150 fs with a time-bandwidth product of 0.5 for a sech^2 shape was produced with an overall cavity dispersion of approximately $-20,000 \text{ fs}^2$. However, pulse breakup (leading to higher-order mode locking or pulse bunching) was observed to occur for cw mode-locked powers as low as 3 mW. At an overall cavity dispersion of approximately $-40,000 \text{ fs}^2$, wavelength tuning was performable, where sech^2 -shaped pulses with a time-bandwidth product of 0.8 were obtained in the spectral range from 1.053 to 1.070 μm . A pulse spectrum at the lower end of the tuning range is shown in Fig. 1, which also demonstrates the complete elimination of a cw background. However, because the adjustment of the cavity parameters required to produce a large spectral shift was critical, for experimental convenience the amplifier seed pulses were produced by using a different approach. In this procedure, the pulses were generated with more positive values of GVD. Typically, as the cavity dispersion is increased to more positive values, the pulse bandwidth increases equally, resulting in increasingly strongly chirped pulse solutions.⁴ The pulse bandwidth may even exceed the bandwidth of

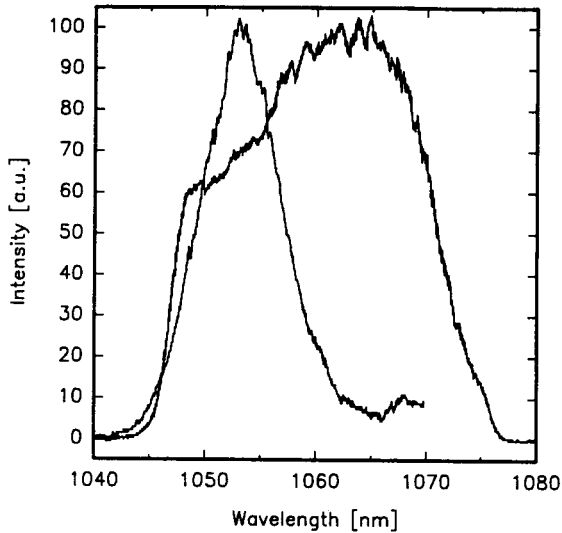


Fig. 1. Spectrally shifted and superbroad oscillator pulse spectrum.

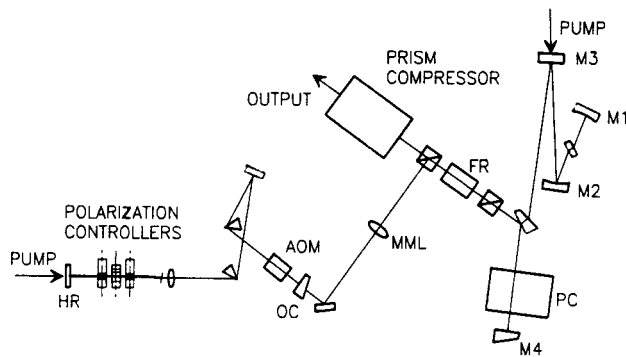


Fig. 2. Experimental arrangement of the oscillator (mirrors HR-OC) and amplifier (mirrors M1-M4) system. HR, high reflectors; AOM, acousto-optic modulator; OC, output coupler; MML, mode-matching lens; FR, Faraday rotator; PC, Pockels cell.

the gain medium for high-power pulses.⁴ Here we employed a GVD of $\approx 0 \text{ fs}^2$ in the cavity such that the generated pulse spectrum was sufficiently broad to cover the wavelength region of interest (see Fig. 1). The corresponding FWHM oscillator pulse width was 530 fs, which gave a time-bandwidth product of 3.4. The pulses could be compressed externally to within a factor of 3 of the bandwidth limit, and pulse compression down to the bandwidth limit required further spectral filtering.

An additional feature of these strongly chirped gain-guided pulse solutions is that their energy content can be significantly higher than is possible for pulses in the negative GVD regime, and pulse breakup was not observed even for the highest cw mode-locked powers. The reason may be understood from approximate analytical solutions of the mode-locked pulses in the cavity,^{4,8} where all cavity parameters are assumed to be evenly distributed along the fiber length. The corresponding length-averaged propagation equation has a chirped sech-pulse solution. The fiber system is well approximated by this type of equation, particularly for small prism separations, because the variation in

pulse width along the cavity also becomes small then.⁴ High-energy pulse solutions in the positive GVD regime result in strongly chirped pulses with small peak powers, whereas low-energy pulse solutions do not exist. On the other hand, in the negative GVD regime, high-energy pulse solutions are weakly chirped and have correspondingly high peak powers. In addition, low-energy pulse solutions with an even lower chirp also exist. In the presence of pulse perturbations and a saturation of the passive amplitude modulation in the cavity, high-energy pulses therefore tend to break up into pulse bunches or pulses at multiples of the cavity round-trip frequency.

The complete oscillator-amplifier system is shown in Fig. 2. Here, the bulk gain medium is a phosphate glass plate of 6-mm length and 1-mm thickness doped with 2 wt. % Nd. To ensure maximum long-term stability, the amplifier was cw pumped with only 0.7 W from the krypton laser, well below a possible pumping level of 1.6 W determined from thermal considerations. The pump beam under-filled the laser beam waist radius of $30 \mu\text{m}$ obtained by using two focusing mirrors with 150-mm radii of curvature. Amplification of single pulses from the

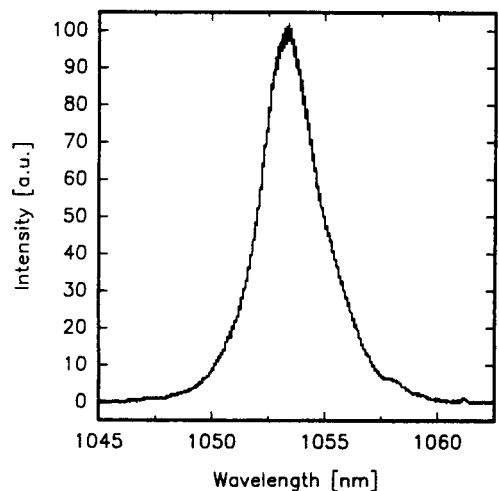
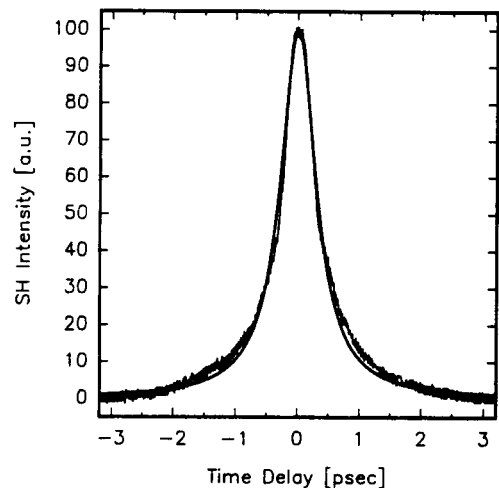


Fig. 3. Background-free autocorrelation of amplified pulses (top) and the corresponding pulse spectrum (bottom). Also shown is a Lorentzian fit to the autocorrelation trace (solid curve in top graph).

oscillator was ensured by insertion of a Pockels cell with a static $\lambda/4$ phase offset into the amplifier cavity. The prevention of feedback into the oscillator was critical and avoided by a polarizer-Faraday rotator arrangement, which also served to channel the amplified pulses out of the system. After amplification, the pulses were compressed to their minimal pulse width by a prism pair arrangement.

The oscillator pulse energy was 120 pJ. With mode matching and spectral losses taken into account, the final seed pulse energy into the amplifier was 10 pJ. The typical round-trip amplifier gain was 1.5. Saturation occurred after 36 round trips in the amplifier, where the pulse energy was 13 μJ and the typical uncompressed pulse width was 3 ps (assuming a sech^2 shape). At this point, the accumulated nonlinear phase delay for the 3-ps pulses in the amplifier was $\approx 1.6\pi$, which led to the onset of self-focusing and noncompressible spectral broadening of the amplified pulses. By limiting the number of round trips to 31 and the amplified pulse energy to 10 μJ , thus also operating the amplifier slightly away from saturation, nonlinear spectral broadening in the amplifier was sufficiently reduced. After compression, the resulting pulse energy was 8 μJ .

An autocorrelation trace of the compressed amplified pulse and the pulse spectrum are shown in Fig. 3. The amplified pulses had a Lorentzian shape with a FWHM width of 300 fs. The time-bandwidth product was 0.24, within 10% of the bandwidth limit of 0.22. To our knowledge, these are the shortest pulses yet produced from an all-glass oscillator-amplifier system at this energy level. Because the oscillator may also be pumped with a laser diode, the system may be upgraded to a diode-pumped all-solid-state version that produces subpicosecond pulses with energies up to the millijoule level.

In summary, we have demonstrated what is to our knowledge the first passive mode locking in a highly nonlinear lead-glass fiber. By using strongly chirped oscillator pulses, self-phase modulation in the oscillator was reduced and the energy content of the oscillator pulses was optimized. The oscillator pulses were of sufficient quality to allow seeding of a bulk Nd:glass amplifier system. We are currently investigating whether strongly chirped oscillator pulses may be used to reduce self-phase modulation in the amplifier further.

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