

# Fabrication and Characterization of Low-Loss Optical Fibers Containing Rare-Earth Ions

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**Abstract**—Low-loss fibers containing rare-earths have been produced with high absorption levels in the visible and near infrared regions. Although containing relatively large quantities of rare-earth impurity dopants, the fibers possess low-loss windows where the attenuation is similar to that observed in undoped fibers. This attribute makes the fibers attractive for use in long distributed sensors, as well as low-threshold fiber lasers. Fiber characteristics relevant to these two applications are uniformity of dopant incorporation, absorption and fluorescence spectra, and fluorescence lifetime. These measurements are presented, together with their respective temperature dependences. The fiber fabrication method is described and results given for  $\text{Nd}^{3+}$ ,  $\text{Er}^{3+}$ , and  $\text{Tb}^{3+}$ -doped fibers.

## I. INTRODUCTION

AS LIGHTWAVE technology matures and conventional fibers become commonplace, attention is being increasingly directed to the fabrication of special fibers dedicated to particular functions. For example, the fiber guiding structure can be readily modified to provide polarization-holding properties, or a given dispersion characteristic. In addition to variations in waveguide structure, however, it is evident that modifying the materials from which the fibers are constructed can yield large improvements in the performance of optical fiber sensors (for a review see ref. [1]), or of transmission components such as isolators [2]. In this respect, glasses containing rare-earth ions are of particular interest, since their use is well known in both active (laser) and passive bulk-optical devices.

The introduction of  $\text{Tb}^{3+}$  or  $\text{Ho}^{3+}$  ions into a glass matrix is known to increase the Verdet constant of the glass [3], thus potentially improving the sensitivity of the fiber in magnetometers [4] and current measuring devices [5]. Similarly, it is thought that the nonlinear optical properties of a fiber may be increased by the incorporation of  $\text{Yb}^{3+}$  [6].

Short lengths of heavily-doped neodymium glass have already been employed as single-point temperature sensors, exploiting either the change in absorption spectrum

[7] or the fluorescence decay time [8]. The extension of these techniques to distributed temperature sensing over long lengths of fiber requires much smaller rare-earth concentrations, as well as very low intrinsic fiber losses.

Multimode fibers containing relatively large concentrations of neodymium also have been reported, fabricated from either compound glasses [9] or silica [10]. Lasers employing short lengths of these fibers have shown multimode stimulated emission at or near a wavelength of  $1.06 \mu\text{m}$ . Similarly, erbium glass lasers [11] which operate at a wavelength within the popular third window for optical communications ( $\sim 1.55 \mu\text{m}$ ), also are known and would make a particularly attractive fiber device.

With the recent emphasis on single-mode transmission and fiber devices, it is worthwhile reexamining this early laser work with a view to constructing single-mode fiber lasers and amplifiers in configurations that require much longer lengths of active fiber, for example, ring-resonator lasers and long, distributed wideband amplifiers. At their operating wavelength, such devices demand the very low losses inherent in telecommunications grade fiber, as well as the close proximity of large impurity absorption bands for the purpose of pumping to an excited state. This requirement and the need to end-pump long single-mode active fiber devices has led us to explore the fabrication of low-loss fibers containing much lower concentrations of rare-earths than previously considered.

In this paper we describe a technique for fabricating silica based multi- and single-mode fibers doped with low levels ( $< 0.25 \text{ wt/o}$ ) of rare-earth ions. The dopant incorporation can be achieved without significantly compromising the inherently low losses of the fiber. As examples, the characteristics of fibers containing  $\text{Nd}^{3+}$ ,  $\text{Er}^{3+}$ , and  $\text{Tb}^{3+}$  are presented and their suitability for fiber sensors assessed. The use of these fibers in various laser configurations is described in an accompanying paper [12].

## II. FABRICATION

To ensure low losses in rare-earth doped fibers, it is advantageous to exploit existing vapor-phase techniques (e.g., the MCVD process) and high-purity precursor materials. The rare-earth halides are ideal starting materials, as they are readily available in high ( $> 99.99$  percent) purity. However, since they are hygroscopic and have high melting points ( $> 500^\circ\text{C}$ ), a number of modifications must

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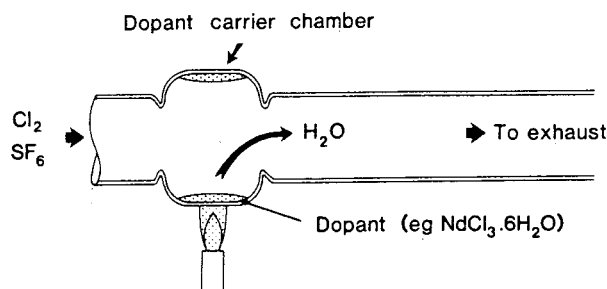


Fig. 1. Substrate tube incorporating dopant carrier chamber, showing drying technique for rare-earth chlorides.

be made to the MCVD process in order to incorporate the dopants without affecting the fiber loss. It should be noted that the technique we have developed is not limited to the rare-earth elements, but may be applied to the incorporation of any dopant from a precursor material which is a solid at or near room temperature, for example, the transition metals.

Fabrication can be considered in four stages:

#### A. Preconditioning and Drying of Rare-Earth Chloride

A standard MCVD substrate tube (O.D. 25 mm, 1.5-mm wall) is modified by the addition of a dopant carrier chamber upstream from the deposition tube, as shown in Fig. 1. The deposition tube is mounted in a preform lathe and the required solid dopant precursor material, e.g.,  $\text{NdCl}_3 \cdot 6\text{H}_2\text{O}$  (99.9 percent pure, melting point =  $758^\circ\text{C}$ ), is introduced into the carrier chamber. The carrier chamber is then gently heated by a temperature-controlled burner to about  $100^\circ\text{C}$  above the melting point of the dopant while flowing a drying gas, either  $\text{Cl}_2$  or  $\text{SF}_6$ , at a rate of 1 l/min. The dopant melts and, on cooling, forms a fused, anhydrous layer on the inside of the carrier chamber.

This refining stage is designed to both fully dehydrate the dopant crystals and to prevent free particulates from passing down the tube during subsequent deposition stages. However, fibers fabricated using only this single drying stage showed unacceptably high  $\text{OH}^-$ -absorption losses due to residual water of crystallization in the fused dopant. Consequently, a second drying stage was introduced during the core deposition, as will be described later.

#### B. Cladding Deposition

Initially, any rare-earth material carried downstream during the refining stage is removed from the walls of the deposition tube by gas-phase etching using  $\text{SF}_6$  [13] ( $1600^\circ\text{C}$ , 0.8 l/min). A conventional MCVD cladding glass is then deposited to give a cladding/core diameter ratio of greater than 7:1. Typically a  $\text{SiO}_2$ - $\text{P}_2\text{O}_5$ -F-matched clad is used, but preforms also have been fabricated using  $\text{SiO}_2$ - $\text{B}_2\text{O}_3$  and undoped  $\text{SiO}_2$ .

#### C. Core Deposition

Here a number of further modifications to the standard MCVD technique are made to ensure rare-earth incorpo-

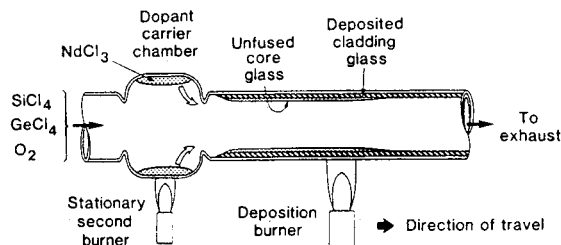


Fig. 2. Core-deposition stage for production of fibers doped with rare-earths.

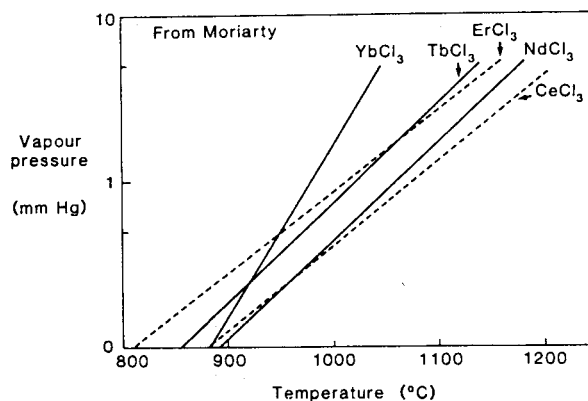


Fig. 3. Dependence of vapor pressure on temperature for typical rare-earth chlorides.

ration and reduce  $\text{OH}^-$  contamination. These will be described with reference to Fig. 2.

The dopant carrier chamber is preheated to a controlled temperature above  $1000^\circ\text{C}$  by a stationary burner to increase the vapor pressure of the fused rare-earth chloride. The required temperature is determined by the vapor-pressure characteristics of the material and the required dopant level in the finished fiber. Vapor pressure curves for some typical rare-earth chlorides are given in Fig. 3 [14]. It can be seen that a temperature of around  $1000^\circ\text{C}$  is sufficient to give a vapor pressure of about 1 Torr. If necessary, an increase in the vapor pressure could be obtained by using the appropriate iodide or bromide salts.

During core deposition, the reactants (typically  $\text{GeCl}_4$  and  $\text{SiCl}_4$ ) are mixed with oxygen and passed through the heated dopant chamber, where controlled amounts of rare-earth halide are entrained in the gas flow. Since the chamber temperature is insufficient to oxidize the reactants, they are oxidized as normal in the downstream hot zone to produce deposited core layers containing low levels of rare-earths. However, the temperature of the MCVD hot zone is chosen such that it is not high enough to fuse the deposited core glass layers. This enables further drying of the materials to be performed.

Analysis of the dopant concentration in the fiber core shows higher dopant levels with increasing carrier chamber temperature, as predicted by the vapor pressure curves. A wide range of dopant concentration levels can thus be obtained by careful control of the temperature.

#### D. Core Drying and Fusion

After deposition, the porous core layer is further dried by heating to  $900^\circ\text{C}$  for 30 min with a traversing burner,

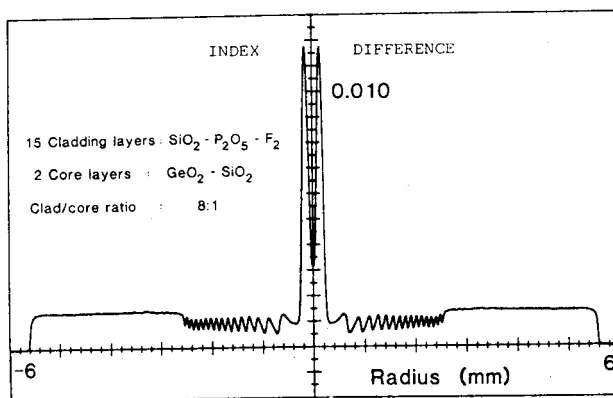


Fig. 4. Refractive-index profile of rare-earth doped preform. Deposited cladding is  $\text{SiO}_2\text{-P}_2\text{O}_5\text{-F}_2$ . Core is  $\text{GeO}_2\text{-SiO}_2$  containing  $\sim 450$  ppm  $\text{Tb}^{3+}$ .

while flowing chlorine gas through the tube (1 l/min). The technique is similar to that used for the dehydration of VAD preforms [15]. The unsintered layer is then fused to form a glassy layer, with the addition of helium, if required, to prevent bubble formation [16]. Preform collapse and fiber drawing are conventional.

### E. Fabrication Results

A wide range of single and multimode fibers containing rare-earths have been fabricated including highly birefringent "Bow-tie" fibers [13]. Core index differences of between 0.2 and 1.2 percent and dopant incorporation levels between 0.2 and 900 ppm have been achieved. These results indicate the versatility of the technique and its applicability to many types of fiber design.

The level of rare-earth incorporation is insufficient to significantly affect the core refractive index [10]. Consequently, the refractive-index profile is due solely to the conventional MCVD dopants and can be varied accordingly. The profile of a  $\text{Tb}^{3+}$ -doped preform is shown in Fig. 4 and is virtually identical to that obtained without rare-earth doping.

The fabrication technique also can be applied to core compositions other than the  $\text{GeO}_2\text{-SiO}_2$  glass used here, for instance the  $\text{P}_2\text{O}_5\text{-SiO}_2$  [17] and  $\text{Al}_2\text{O}_3\text{-SiO}_2$  [18] glass systems. Moreover, the technique may be used to introduce impurity dopants into the deposited cladding glass.

## III. CHARACTERISTICS OF FIBERS CONTAINING RARE-EARTH IONS

Dopants which have been successfully incorporated into fibers include  $\text{Nd}^{3+}$ ,  $\text{Er}^{3+}$ ,  $\text{Tb}^{3+}$ , and  $\text{Eu}^{3+}$  ions. In the results presented below, the dopant concentrations were confirmed by comparing the measured absorption spectra of the drawn fibers with previously published data for rare-earth ions in high-silica bulk glasses [19]. The results that follow are biased toward  $\text{Nd}^{3+}$ -doped fibers, since this material is better characterized in the literature.

### A. Absorption Spectra

Measurement of the absorption spectra of rare-earth doped fibers poses a number of problems owing to the

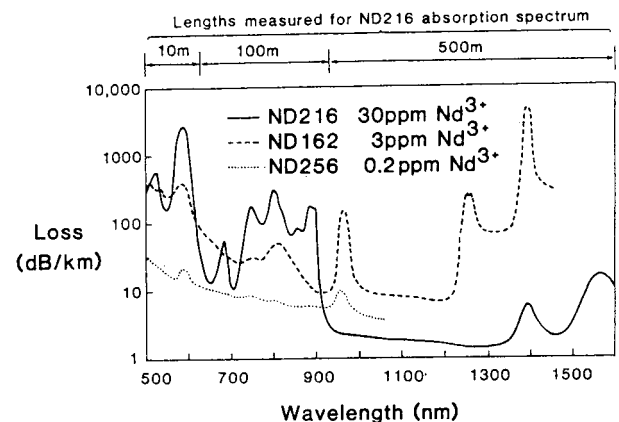


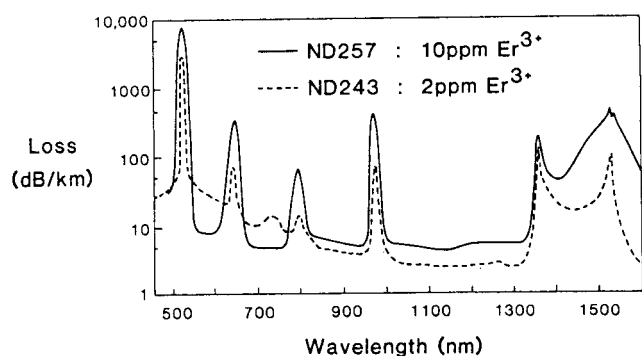
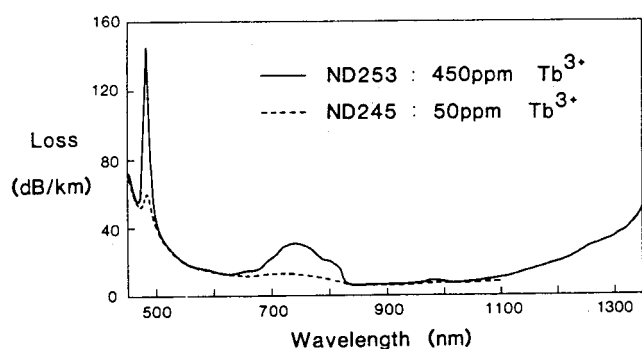
Fig. 5. Absorption spectra of fibers containing various concentrations of  $\text{Nd}^{3+}$  ions (as marked), showing windows of very low loss. For comparison, fiber attenuation without second drying stage (ND 162) exhibits large  $\text{OH}^-$  absorption band at 1390 nm. The lengths marked at the top of the diagram indicate the fiber lengths used to obtain the absorption spectrum of ND216.

difficulty of measuring losses which vary by several orders of magnitude across the spectrum. A multiple cut-back technique in combination with attenuation equipment optimized for dynamic range was used to overcome these difficulties. A white-light source and a scanning double monochromator provided the fiber input, while the output power was measured using either a Si or, for longer wavelengths, a liquid  $\text{N}_2$  cooled Ge photodiode. The double monochromator reduced the stray light in the system and allowed an attenuation in excess of 48 dB to be measured in single-mode fibers with a 2-nm spectral resolution (c.f. 35 dB in most instruments).

Various fiber lengths were measured, depending upon the regions of the spectrum under test and the results re-scaled and combined to give absorption spectra with extremely high dynamic ranges. For example, the absorption spectrum of the  $\text{Nd}^{3+}$ -doped fiber number ND216 illustrated in Fig. 5 was determined using lengths of 10, 100, and 500 m, as indicated on the graph, and shows a measurement range of 3000 dB/km.

A possible source of error in the measurement is the presence of excited state fluorescence, a proportion of which is received by the detector. The effect reduces the apparent loss within the absorption bands. However, it can be calculated that the fluorescence has a negligible effect on measurement accuracy and this was confirmed by using blocking filters.

The absorption spectra for three fibers containing different levels of  $\text{Nd}^{3+}$  dopant are shown in Fig. 5. Strong characteristic  $\text{Nd}^{3+}$  absorptions in the visible and near infrared regions can be clearly seen, together with a low-loss window ( $< 2$  dB/km for fiber ND216) between 950 and 1350 nm. Significantly, this includes the  $\text{Nd}^{3+}$  laser wavelength around  $1.60 \mu\text{m}$ , where the loss is only 1.8 dB/km. These loss levels are not dissimilar to those observed in telecommunications-grade fibers. The small loss penalty is believed to be due to increased scatter in the glass as a result of the presence of large impurity ions, rather than to absorption band tails.

Fig. 6. Absorption spectra of fibers containing 2 and 10-ppm  $\text{Er}^{3+}$  ions.Fig. 7. Absorption spectra of fibers containing 50- and 450-ppm  $\text{Tb}^{3+}$  ions.

The efficiency of the techniques used to dry both the precursor and deposited materials is demonstrated by comparing the  $\text{OH}^-$ -absorption bands at 1390 nm for fibers ND162 and ND216 (Fig. 5.) No attempt was made to dry either the precursor or deposited materials for fiber ND162, resulting in an  $\text{OH}^-$ -impurity level of  $\sim 65$  ppm. For fiber ND216, however, the two-stage drying technique results in a considerably reduced  $\text{OH}^-$ -absorption peak of only 5 dB/km at 1390 nm, which corresponds to an  $\text{OH}^-$ -impurity level of  $\sim 80$  ppb.

The absorption spectra for two fibers containing different levels of  $\text{Er}^{3+}$  ions are shown in Fig. 6. Strong  $\text{Er}^{3+}$ -absorption bands can be clearly seen at 520, 980, and 1536 nm with, again, regions of low loss close to the absorption peaks. This is particularly marked in fiber ND257 where, despite the extremely high loss ( $\sim 9000$  dB/km) in the absorption band at 520 nm, the loss falls to a remarkable 25 dB/km at 540 nm, a mere 20 nm away.

The absorption spectra for two fibers containing  $\text{Tb}^{3+}$  ions are shown in Fig. 7. Although containing relatively high dopant concentrations, the fibers show only a few, low-intensity peaks compared to the  $\text{Nd}^{3+}$ - and  $\text{Er}^{3+}$ -doped fibers described previously. The effect is typical of  $\text{Tb}^{3+}$  ions in glass and is due to the low absorption cross section of the  $\text{Tb}^{3+}$  ion within the wavelength range of measurement. Note that the loss increase beyond  $1 \mu\text{m}$  for both fibers are bend edges, as the fibers were designed for use at wavelengths below 600 nm, where the  $\text{Tb}^{3+}$  ion is known to fluoresce (see below).

The temperature dependence of the absorption spectra (Fig. 8) is important for both fiber sensors and lasers. The

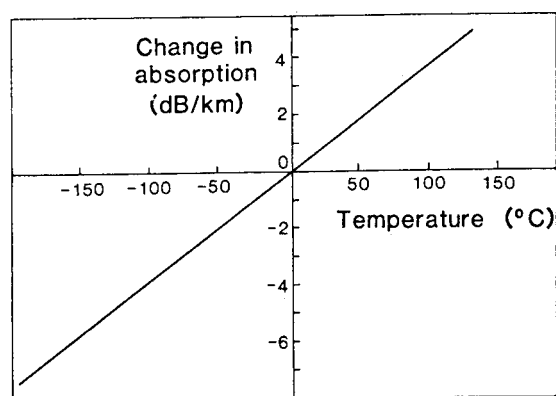
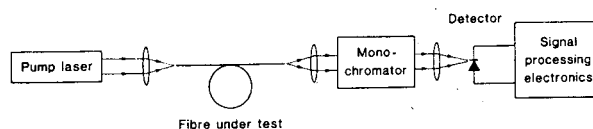
Fig. 8. Temperature variations of absorption at 600 nm in a fiber doped with  $\sim 0.2$ -ppm  $\text{Nd}^{3+}$ .

Fig. 9. Schematic of equipment for measurement of fluorescence characteristics. Signal-processing equipment consists of a phase-sensitive detector for fluorescence spectra or a computer-controlled digital averager for fluorescence lifetime measurements.

TABLE I  
SPECIFICATIONS OF PUMP LASERS USED IN MEASUREMENTS OF FIBER  
FLUORESCENCE CHARACTERISTICS

Dopant	Pump Laser Type	Pump Wavelength (nm)	Pump Output Power (mW)
$\text{Nd}^{3+}$	Semiconductor	780	1
$\text{Er}^{3+}$	Argon-ion	514	200
$\text{Tb}^{3+}$	Argon-ion	488	50

fiber used was multimode (40- $\mu\text{m}$  core, 125- $\mu\text{m}$  cladding) and contained 0.2-ppm  $\text{Nd}^{3+}$ . The absorption spectrum at 25°C was given in Fig. 5 (fiber ND256.) Over the range from  $-196^\circ\text{C}$  (liquid nitrogen) to  $+125^\circ\text{C}$ , the fiber loss at 600 nm (i.e., the tail of the 590-nm absorption band) shows a linear dependence with temperature, which is promising for use as a temperature sensor.

### B. Fluorescence Spectra

The fluorescence spectra of the fibers was measured using the equipment shown schematically in Fig. 9. The laser used as the pump source depends upon the fiber under investigation, since for efficient excitation it is necessary to match the pump wavelength to an impurity absorption band. The wavelengths and output powers of the lasers used for each rare-earth are shown in Table I. The detector was either a Si or a liquid  $\text{N}_2$  cooled Ge photodiode, depending on the wavelength of interest. The signal was processed with a phase-sensitive detector.

Referring to Fig. 10, the  $\text{Nd}^{3+}$  fiber shows fluorescence bands centered on wavelengths of 940, 1088, and 1370

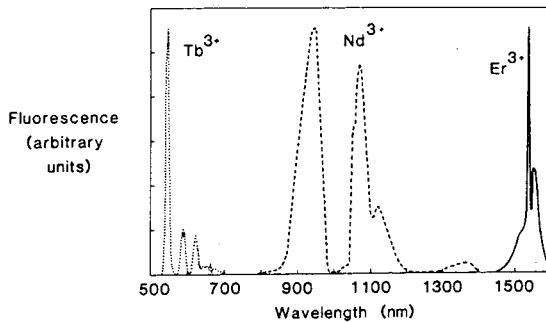


Fig. 10. Fluorescence spectra of  $\text{Nd}^{3+}$ -,  $\text{Er}^{3+}$ -, and  $\text{Tb}^{3+}$ -doped fibers.

nm, corresponding to emissions from the  $^4I_{3/2}$  state to the  $^4I_{13/2}$ ,  $^4I_{11/2}$ , and  $^4I_{9/2}$  levels. Note that the fluorescence peaks are shifted to slightly longer wavelengths than normal in glass as a result of the silica host [10], [20]. The broad fluorescence band centered at  $1.088 \mu\text{m}$  has enabled the development of a neodymium fiber laser with an extremely wide tuning range of  $80 \mu\text{m}$  [12].

As expected in a three-level system, the fluorescence of the  $\text{Er}^{3+}$ -doped fiber coincides with an absorption band at the fluorescence wavelength. The fluorescence measured corresponds to a transition from the  $^4I_{3/2}$  level to the  $^4I_{15/2}$  ground level and again, the extensive width of this band has led to the development of a broadly tunable CW laser, in this case tunable between  $1.529$  and  $1.553 \mu\text{m}$  [12].

The fluorescence spectrum of the  $\text{Tb}^{3+}$ -doped fiber contains visible fluorescence bands at  $545$ ,  $590$ , and  $625 \text{ nm}$ . These correspond to transitions from the  $^5D_4$  level to the  $^7F_5$ ,  $^7F_4$  and  $^7F_3$  levels, respectively. A further weak fluorescence band centered around  $670 \text{ nm}$  also can be seen and is believed to be a combination of the fluorescence due to  $^5D_4$  to  $^7F_2$ ,  $^7F_1$  and  $^7F_0$  transitions.

### C. Fluorescence Lifetimes

A knowledge of the fluorescence decay time is required to permit calculations of fiber laser saturation intensities and lasing thresholds. In addition, the temperature dependence of the fluorescence lifetime is of interest for sensor applications. The fluorescence decay characteristics were investigated with the equipment shown schematically in Fig. 9, with a laser again chosen to match the absorption bands of the fiber under test. The signal-processing electronics now consist of a computer-controlled digital averager triggered by the laser pump.

The fluorescence lifetime of the  $\text{Nd}^{3+}$ -doped fibers was measured using a frequency-doubled  $Q$ -switched Nd-YAG laser (wavelength  $532 \text{ nm}$ , pulse width  $90 \text{ ns}$ ) as the pump source. A  $1/e$  fluorescence decay time of  $470 \mu\text{s}$  at both  $940$  and  $1088 \text{ nm}$  was measured, which is in good agreement with previously published results [20]. For the  $\text{Er}^{3+}$ -doped fibers, a  $1/e$  decay time of  $14 \text{ ms}$  was obtained using a mechanically-chopped argon-ion laser beam operating at  $514 \text{ nm}$  as the pump. This is again in good agreement with previously results [11].

A more detailed analysis of the fluorescence decay was

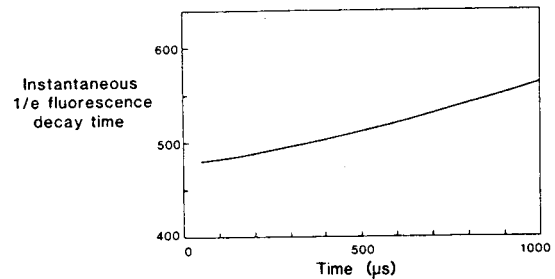


Fig. 11. Variation in instantaneous  $1/e$  fluorescence decay time for a  $\text{Nd}^{3+}$ -doped fiber plotted against time-after-excitation.

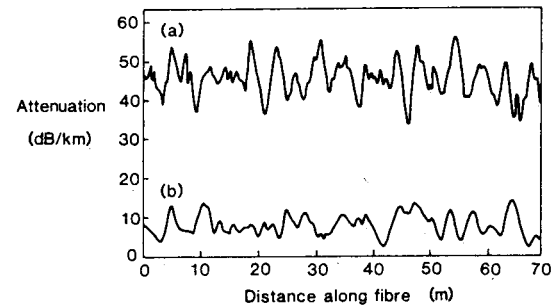


Fig. 12. Local attenuation of fibers measured using an OTDR technique, showing average uniformity over length. (a)  $\text{Nd}^{3+}$ -doped fiber. (b) Undoped reference fiber.

made for the  $\text{Nd}^{3+}$ -doped fibers. A curve fitting routine was used to obtain the instantaneous  $1/e$  decay time and Fig. 11 shows this value plotted against time after the excitation pulse. It may be seen that the instantaneous value of the fluorescence lifetime increases with time, a phenomenon which has been previously noted [21] and which is due to the statistical distribution of the  $\text{Nd}^{3+}$  ion in the glass matrix.

Initial measurements of the temperature dependence of the fluorescence decay in  $\text{Nd}^{3+}$ -doped fibers show a decrease of approximately 2 percent in the  $1/e$  fluorescence lifetime over the temperature range  $0$  to  $100^\circ\text{C}$ . This is accompanied by a 10-percent decrease in the fluorescence output level due to a reduction in the quantum efficiency of the fluorescence process [22].

### D. Consistency of Dopant Incorporation with Length

The use of rare-earth doped fibers as distributed sensors [1] or fiber lasers [12] requires a uniform dopant incorporation along the fiber length. The wavelength-tunable backscatter technique [23] was used to obtain length resolution of the dopant absorption bands and the result obtained at  $620 \text{ nm}$  for a  $\text{Nd}^{3+}$ -doped single-mode fiber is shown in Fig. 12, together with a reference result for an undoped fiber.

No variation in the average absorption level, and hence amount of dopant incorporated, is visible along the  $80\text{-m}$  length of the doped fiber, thus confirming the high degree of control in the fabricated process. The noise levels visible on both traces are due to well-known measurement limitations [24] and are not associated with rapid dopant fluctuations.

## IV. DISCUSSION

The application of the rare-earth doped fibers described here has already been demonstrated. Lasing action has been reported at a wavelength of  $1.088\ \mu\text{m}$  in  $\text{Nd}^{3+}$ -doped fibers [25] and at  $1.536\ \mu\text{m}$  in  $\text{Er}^{3+}$ -doped fibers [12]. The very low thresholds reported are due in part to the extremely low losses of the fibers, which further emphasizes the importance of the techniques developed to remove  $\text{OH}^-$ -impurity ions.

The possibility of using rare-earth doped fiber as the sensing element in a distributed temperature sensor has been mentioned earlier. Calculations for a distributed sensor based on the temperature variation of the  $\text{Nd}^{3+}$ -absorption bands indicate that an accuracy of  $3^\circ\text{C}$  with a resolution of 5 m could be easily obtained over a 200-m length of fiber, using a backscatter technique similar to that described in [26]. Further improvements may be obtained by the use of a dopant with a greater change in absorption with temperature.

## V. CONCLUSIONS

A simple, reproducible fiber fabrication technique has been developed which allows the incorporation of uniformly low levels of rare-earth ions as impurity dopants in the core of many types of optical fibers. The technique is not limited to the rare-earth elements, but could be applied to any dopant with a solid precursor material, for instance the transition metals.

Fibers have been fabricated containing various rare earths with dopant levels of between 0.2 and 990 ppm (0.25 wt/o). Remarkably, all exhibit windows in which losses are comparable with conventional fibers, despite the close proximity of very high-loss dopant absorption bands. The low fiber losses combined with the consistency of dopant incorporation along the fiber length make the fibers suitable for use in distributed sensor applications.

It is clear that rare earth-doped fibers of the type described here will find many applications in laser and non-linear devices, signal processing, and switching. An early indicator of the potential is the ease with which low-threshold single-mode fiber lasers can be constructed using either  $\text{Nd}^{3+}$ - or  $\text{Er}^{3+}$ -doped fibers.

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